ASX ANNOUNCEMENT

17 April 2024

Mineral Resource upgrade paves way for Northern Silica Project PFS

- **Significant 17% increase in Indicated Resource and establishment of maiden 49.5 Mt Measured Mineral Resource for Diatreme's flagship Northern Silica Project (NSP) in Far North Queensland**
- **Results provide strong Resource foundation for upcoming Pre-Feasibility Study (PFS) and maiden Ore Reserve**
- **Bulk sample testing and further specialist metallurgical testwork currently underway at external laboratories**
- **NSP on track for development amid increasing demand for critical mineral key to solar energy industry.**

Emerging silica sands developer, Diatreme Resources Limited (ASX:DRX) announced today a significant upgrade to the estimated Si2 Mineral Resource at the Company's Northern Silica Project (NSP) in Far North Queensland, highlighting the critical mineral project's potential amid an accelerating solar energy boom.

In the last two months Diatreme has advanced the NSP significantly, with results from the 2023 infill drilling program delivered in late February 2024, through to Particle Size Distribution results arriving in late March 2024, and a deposit scale bulk density program completed in early April 2024. Each phase was designed to enhance the precision of Resource modelling and to enhance project confidence.

The latest data has shown an increase in both the estimated Mineral Resource categories, with the inclusion of a maiden Measured Resource of 49.5 Mt, as well as increasing the size of the Indicated Resource to 120.5 Mt (up 17% from the previous estimate). Diatreme's total low iron, high purity silica sand resource base exceeds 402 Mt, an extremely strategic and highly valuable resource that is well positioned to supply the fast-growing solar PV market.

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Diatreme's CEO, Neil McIntyre commented: *"It is pleasing to report a further enhancement in the quality of the resource estimate for our flagship NSP, with the establishment of its first Measured category Mineral Resource and significant increase in its Indicated category Mineral Resource.*

"The enhanced resource allows us to advance our PFS with greater confidence, providing a deeper understanding of the extraordinary potential for commercialisation contained within the Si2 dune complex at the NSP.

"We look forward to delivering the project's PFS by mid-2024, together with a maiden Ore Reserve, as we ramp up development of this asset vital to the clean energy revolution, both in Australia and internationally."

The resource upgrade follows moves by the Australian Government to promote the domestic manufacturing of solar panels under its $1 billion "Solar Sunshot" program. Low iron, high purity silica sand is a key ingredient in the solar PV manufacturing process (solar glass), which is currently dominated by China.

The NSP is also located near Cape Flattery, an area identified as a potential critical minerals hub for silica sand by the Queensland Government in its 2023 "Critical Minerals Strategy."

NEXT STEPS

The PFS will represent a critical milestone in the NSP's development, building upon insights gained during the June 2023 Scoping Study and furthering understanding of both technical and financial viability. The PFS will evaluate the optionality of methods and technologies best suited for extracting and processing the Si2 deposit's silica sand, ensuring that the selected approaches align with Diatreme's core values. Additionally, the study will involve logistical planning to streamline the transport of materials through the Port of Cape Flattery using an underpinning commercial rationale and development strategy. Further in-depth market analysis will be undertaken to ascertain the projected demand and pricing dynamics for high-purity silica sand.

By establishing a thorough and rigorous framework through the PFS, the study aims to not only verify its economic viability but also optimise mining and processing operations, ultimately ensuring the NSP will be a low-cost producer of low iron, high purity silica sand. This strategic focus is designed to maximize the resource's value while minimising operational costs, thus setting a solid foundation for the decision-making process regarding the full-scale development of the mining operation.

Samples from within the Si2 resource area which were sent for Bulk Sample test work and metallurgical characterisation in Q1 2024 have been undergoing processing at specialist laboratories and are now nearing completion. This round of test work is aimed to further confirm current known processing methods as well as investigate new processing methods and technologies now available. Metallurgical test work completed to-date confirms the silica sand resource is readily amenable to upgrading by conventional washing and screening methods to a low iron, high purity silica sand for photovoltaic applications (solar panel glass).

Deposit	JORC Resource Category	Silica Sand (Mt)	SiO_2 (%)	Fe_2O_3 (%)	TiO_2 (%)	Al_2O_3 (%)	LOI (%)
Si2	Measured	49.5	99.33	0.11	0.13	0.11	0.12
	Indicated	120.5	99.32	0.10	0.14	0.10	0.14
	Inferred	65	99.20	0.12	0.17	0.12	0.17
Total		**235**	**99.29**	**0.11**	**0.15**	**0.11**	**0.14**

Table 1: Mineral Resource Estimate for Si2

RESULTS OVERVIEW

The results of the Mineral Resource update at Si2 in summary are as follows:

- Increase from 103Mt to 120.5 Mt in the Indicated category Mineral Resource – up 17%.
- Establishment for the first time of a 49.5 Mt Measured category Mineral Resource.
- Diatreme now has 170 Mt of Measured + Indicated Mineral Resource, of suitable confidence to support mine planning. This provides the foundation for a PFS and Ore Reserve estimation.
- Overall tonnage remains at 235 Mt at the Si2 deposit.
- The results of the recent bulk density testwork have confirmed that the previously assumed density of 1.6 t/m3 is appropriate.
- Particle size distribution confirmed the deposit contains a relatively homogenous distribution of silica sand, suitable for downstream processing into target markets.

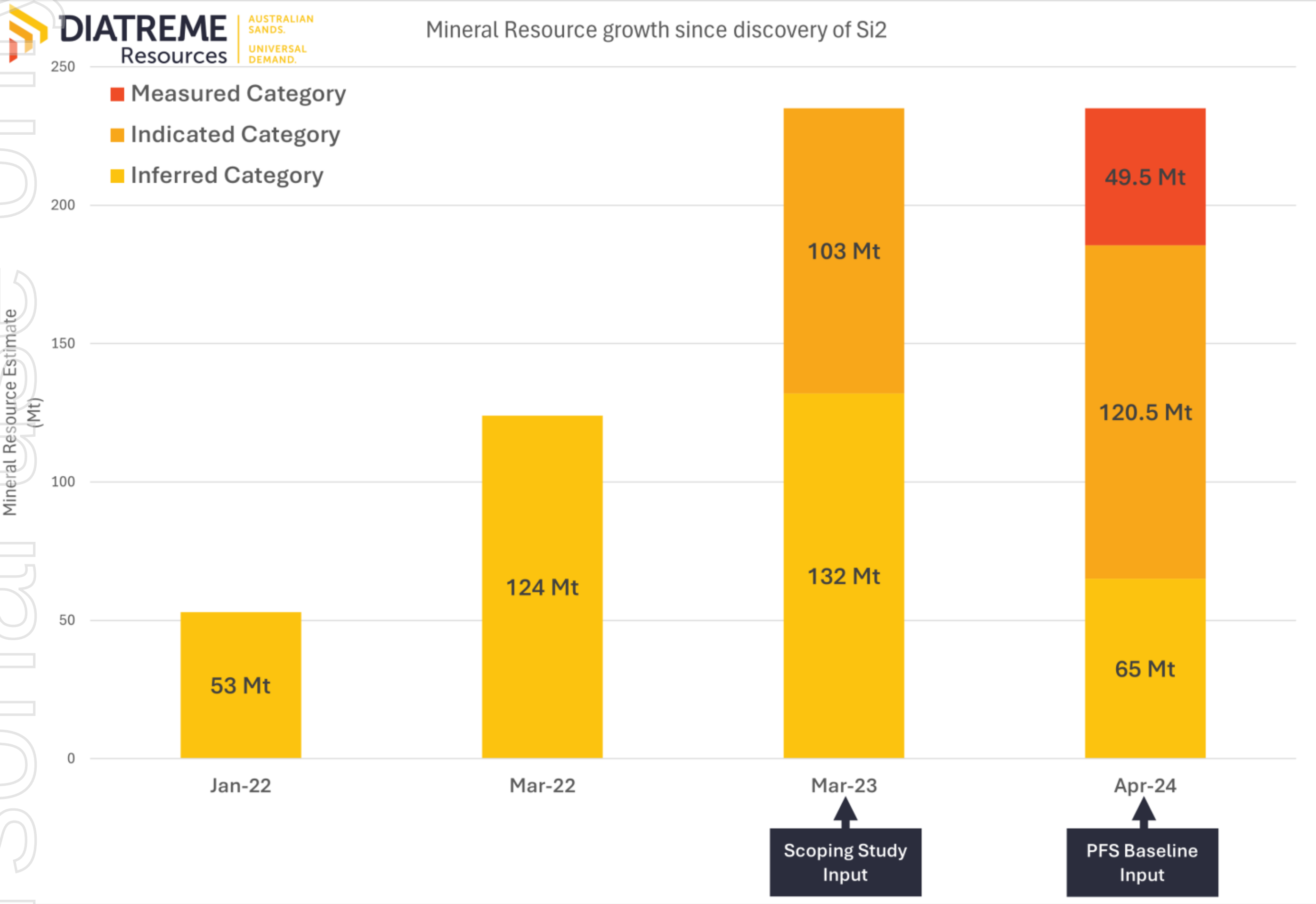

Figure 1: Mineral Resource growth since discovery of Si2

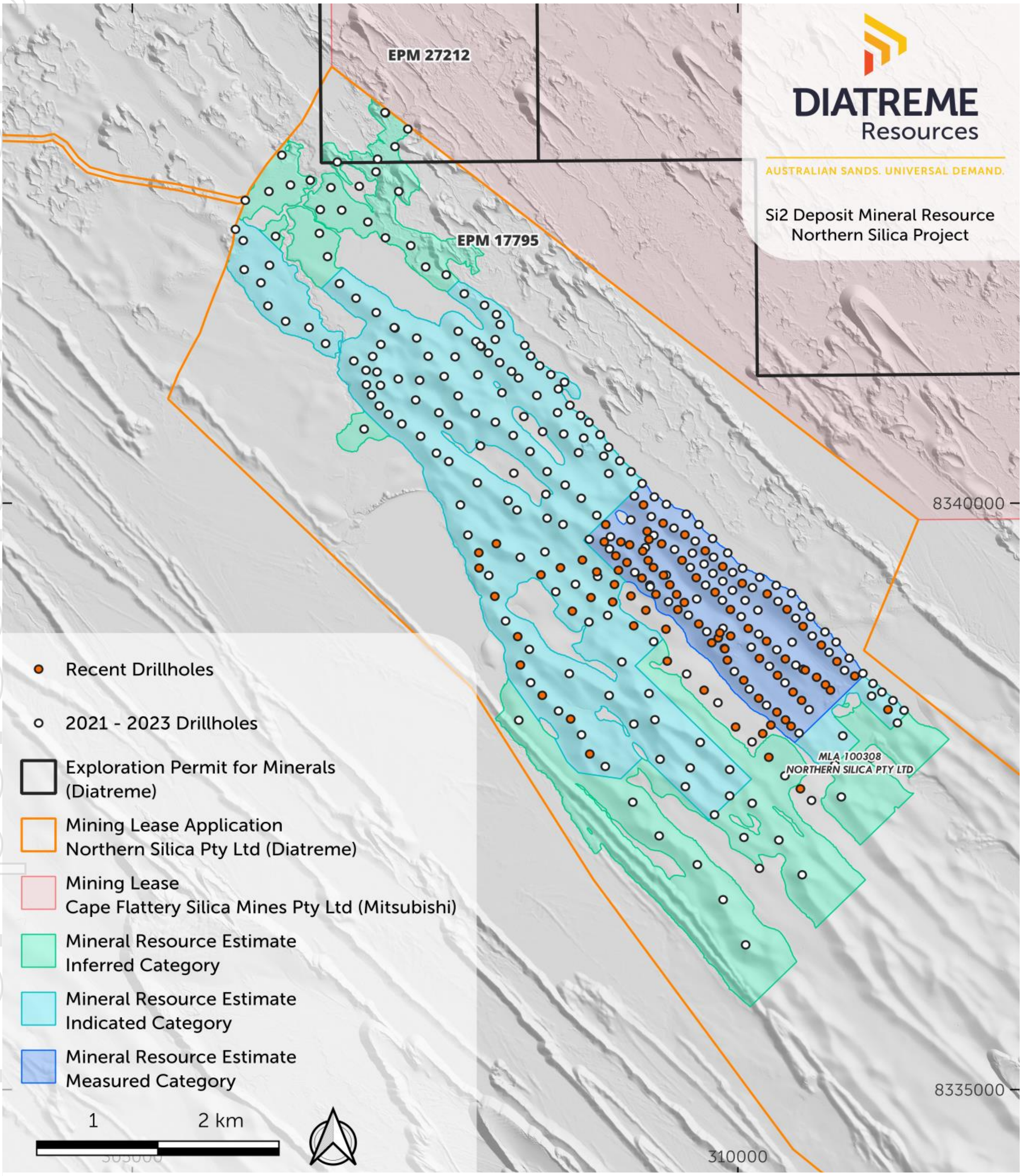

Figure 2: Exploration Summary Map & 2024 Mineral Resource Estimate at Si2

ASX LISTING RULE 5.8.1 SUMMARY

The following summary provided presents a fair and balanced overview of the contents of the technical report undertaken on the Mineral Resource Estimate by independent firm Measured Group.

GEOLOGY AND GEOLOGICAL INTERPRETATION

Silica sand mineralisation at Si2 Deposit occurs within the Cape Bedford / Cape Flattery Dune Field. The targeted silica sand deposits are the trailing arms and apex of elongate parabolic aeolian sand dunes.

The Cape Bedford / Cape Flattery Dune Field is one of several extensive areas of aeolian dunes which occur on the tropical east coast of Cape York Peninsula. The dune field covers an area of 700km2 and contains a variety of depositional and erosional landforms. The dominant source sand of the dune field is considered to be from the weathering of Mesozoic sandstone such as the Gilbert River Fm, and the Dalrymple Sandstone, however coastal granites and the Hodgkinson Fm are likely additional sources of sand. As the Mesozoic sandstones are the aquifer units within the Laura Basin, they are likely to have been exposed to leaching while hosted within the sandstone, prior to exposure to erosional processes. Strong prevailing South-easterly winds appear to have been the consistent wind direction in the region, and still prevail today for most of the year. These winds are the energy source for the establishment and remobilisation of the sand dune systems.

The mineral resource is generally constrained to the trailing arms and apex of elongate parabolic dunes, which can be clearly defined using the surface LiDAR imaging. Drilling often intersects overlapped dunal features, which are not represented by LiDAR or aerial photography.

Conversely, the interdunal areas are often devoid of thick aeolian sand and predominantly exhibit exposed B1 horizons, clays, bedrock, or other sediments. Where drilling has intersected obscured silica sand mineralisation, the sampled sand has been included in the geological model.

There is an observable basement high on the topographic high towards the coastline on the western dunes.

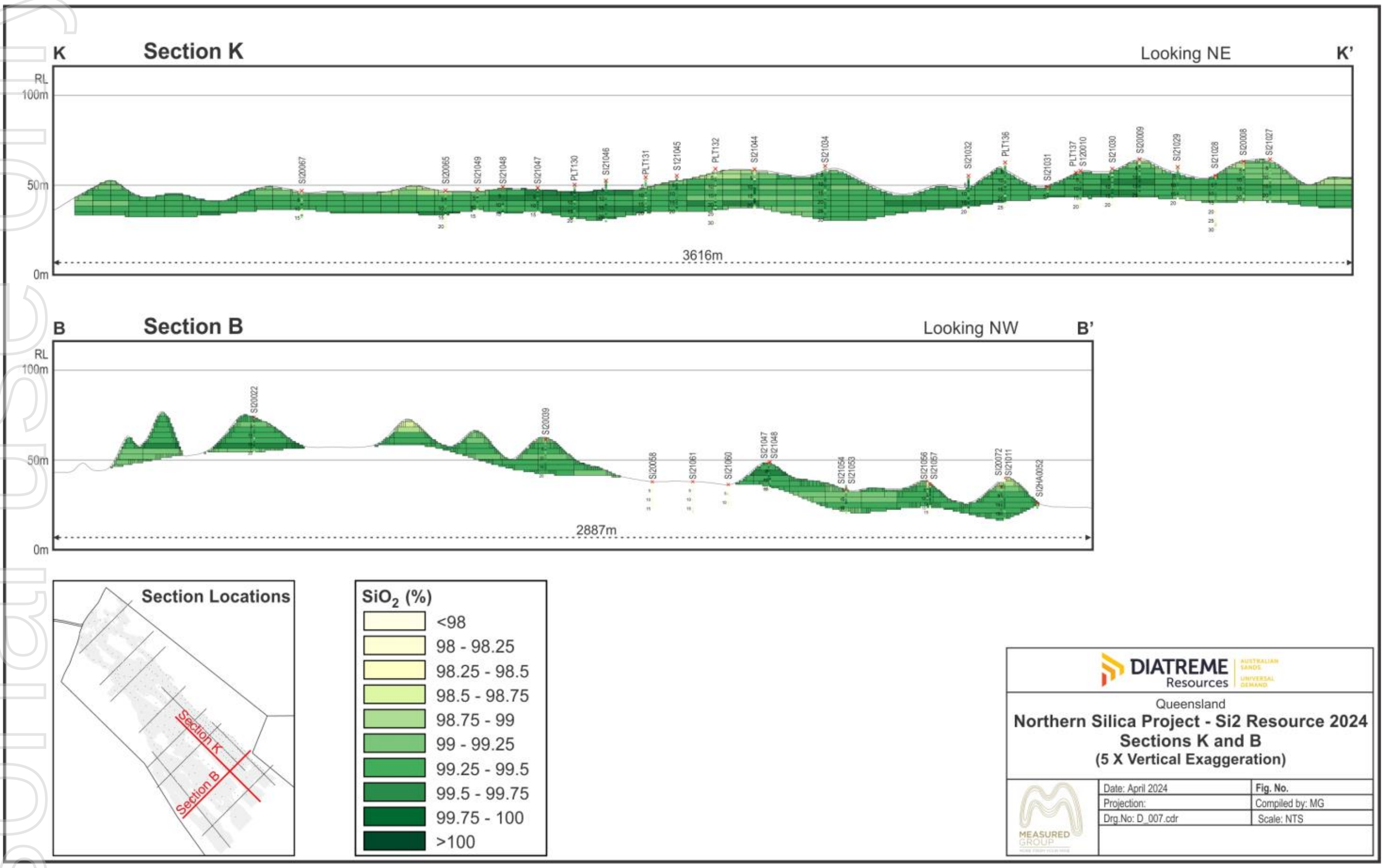

Figure 3: Cross sectional diagram of block model, indicating relevant sections of excluded drillholes and showcasing dune topography.

SAMPLING AND SUB-SAMPLING TECHNIQUES

Prior to April 2022, the vacuum drill collected cuttings reported to a return thick perplex canister mounted on the drill rig with 2-3kg (100% of drill material returned by the vacuum drill rig) after passing through a single tiered (50/50) riffle splitter, collected and bagged in numbered calico sample bags, and sealed ready for assaying, as drilling progressed.

After April 2022, the aircore drill collected samples in 1m increments after passing through a single tiered (50/50) riffle splitter, collected and bagged in numbered calico sample bags, and sealed ready for assaying, as drilling progressed.

Where hand augering was utilised for sample collection, 1m samples were augered, collected and bagged in numbered calico sample bags, and sealed ready for assaying, as sampling progressed.

All drill holes have been photographed, logged and sampled under the supervision of Frazer Watson, Diatreme Resources' Senior Geologist. The samples are stored in clearly labelled chip trays with bagged samples remaining stored at CSHPL's Cooktown laydown yard.

The Competent Person has determined that the quality of the drilling, sampling, and analysis meets the necessary standard for inclusion in a publicly reported Mineral Resource estimate, as per the JORC Code (2012) guidelines.

DRILLING TECHNIQUES

330 drill holes were used to define the Mineral Resource Estimate in accordance with the JORC Code (2012). Samples were obtained by vacuum drilling, aircore drilling or hand augering methods and were drilled vertically.

Drilling programs were mainly concentrated on the trailing arms and apexes of the elongate parabolic dunes. Additionally, hand augering was specifically carried out in the deflationary troughs to ensure continuity in estimating resources. As of April 2024, 170 aircore drillholes, 61 hand auger holes, and 99 vacuum drillholes, totalling 6,108.3m have been drilled within the Si2 Deposit.

Drilling was either completed by a vacuum drilling, aircore drilling or hand augering methods and drilled vertically with an average depth of 18.5m. Vacuum drilling was undertaken by contractor Yearlong Contracting using a 4x4 tractor mounted drill rig with a blade drill bit diameter of 60mm equivalent to NQ sample size with 1.8m rods. Aircore drilling was undertaken by a Diatreme Resource track mounted drill rig, with a 3" blade drill bit, with 3m rods. Drilling terminated immediately when damp clay basement or wet sands were intersected.

Figure 4: Diatreme Resources' Aircore drill rig showing sub-sample collection after the riffle splitter.

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RESOURCE CLASSIFICATION

The Mineral Resource has been classified according to the principles of the JORC Code (2012 edition). The resource has been divided into Measured, Indicated, and Inferred categories, corresponding to a high, moderate and low level of confidence in the structural and grade continuity of the resource. The classification integrates several key factors, including: depth of geological knowledge of the deposit, geological and mineralisation continuity, drill hole spacing, and the results of quality control measures.

Points of Observation are defined as intersections of the silica sand unit, with appropriate assay analysis. Interpretive data includes LIDAR survey interpretation of the top and base of the dunes.

The classification also considers drill hole logging, analytical results from drill samples, geostatistical analysis, and confidence in geological and grade continuity, along with recent metallurgical/process test outcomes. Additionally, search and interpolation parameters, recently completed density data, and considerations from JORC Code Clause 49 are factored into the classification process.

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SAMPLE ANALYSIS METHODS

Analysis of samples prior to April 2022 was via ALS method ME-XRF26 (whole rock by fusion/XRF), and by ME-GRA05 (H2O/LOI) for Loss of Ignition by TGA furnace. Analysis of samples after April 2022 was via Bureau Veritas method XF100 which is considered a total whole rock analysis and by TG002 for LOI. Preparation and analysis of samples utilised tungsten carbide pulverisation to reduce the effect of iron contaminating the sub-sample.

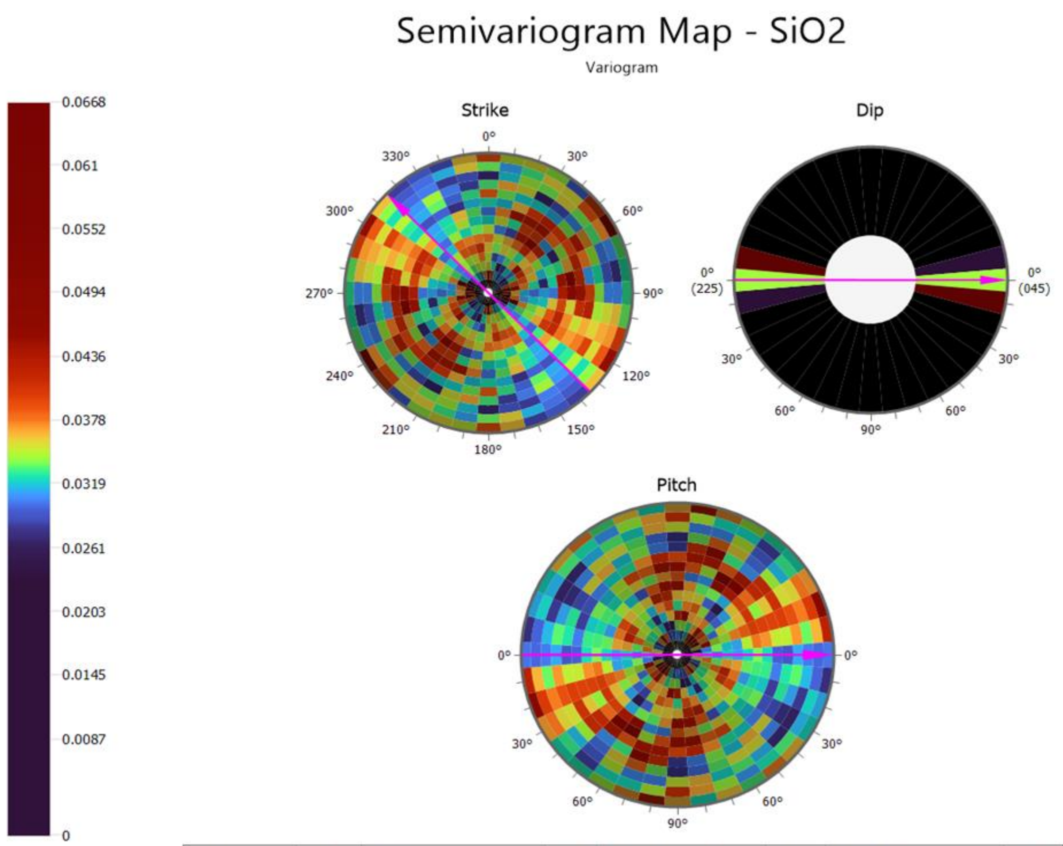
Figure 5: Tungsten carbide pulverising bowl used to ensure Fe-Cr contamination is minimised during sample preparation.

ESTIMATION METHODOLOGY

The Mineral Resources were estimated by modelling of the high-purity silica sand. The geological model incorporated several key parameters. The topography surface was surveyed using LIDAR techniques to a resolution of 1m horizontally and 10cm relative vertical accuracy. The top surface of the resource volume was set at 0.3m below the LIDAR topography, representing the base of the topsoil. The bottom surface of the resource volume was constructed from:

- The base depth of the Silica Sand unit determined from drilling
- The depth of the groundwater table determined from drilling
- Interpretation of the dune edge from LiDAR survey and aerial imagery

The resource boundary was established by geological interpretation and through analysis of surface dune extents visible in LIDAR, and aerial imagery. A block model was generated to estimate the deposit grade. The orientation of



Strike	315°	Plunge	0°	Strike - Max Distance	1550	Pitch - Directions	36
Dip direction	045°	Rotation	0°	Dip - Directions	36	Pitch - Direction Angle	10°
Dip	0°	Strike - Directions	36	Dip - Direction Angle	10°	Pitch - Interval	100
Pitch	0°	Strike - Direction Angle	10°	Dip - Interval	75	Pitch - Interval Count	15
Sense	WEST	Strike - Interval	100	Dip - Interval Count	1	Pitch - Max Distance	1550
Azimuth	315°	Strike - Interval Count	15	Dip - Max Distance	112		

Figure 6: Semivariogram Map - SiO_2

the block model was set to the average strike of the dunes (315 degrees). The dimensions for the parent blocks were determined as 100m across strike by 50m along strike by 3m vertical, which were then subdivided into sub-blocks of 5x5x1m to best fit the undulating geological model. Grade estimation was completed using ordinary kriging, and a validation check estimate was completed using inverse distance weighting squared.

The Ordinary Kriging (OK) method was used to estimate the grades and populate the block model for SiO2, Fe2O3, TiO2, Al2O3 and LOI. The grade estimation process was conducted over 4 (four) sequential passes, each defined by specific search radii that help to guide to the categories of 'Measured', 'Indicated' and 'Inferred' in resource classification. This methodology involved setting the major sample search parameters for each block horizontally in the average strike direction of the dune (315 degrees), the semi-major search direction is also set horizontal (perpendicular to the major search direction) across the dune, and the minor search direction is set to vertical. The search distances used for each pass were derived from variography studies, ensuring that the interpolation aligns with the spatial characteristics of the geological data. All passes used a quadrant-based search with the maximum number of samples set at 32 and required a minimum of three drillholes for reliable grade estimation. Block discretisation of 4 x 4 x 4 (X,Y, Z) was employed.

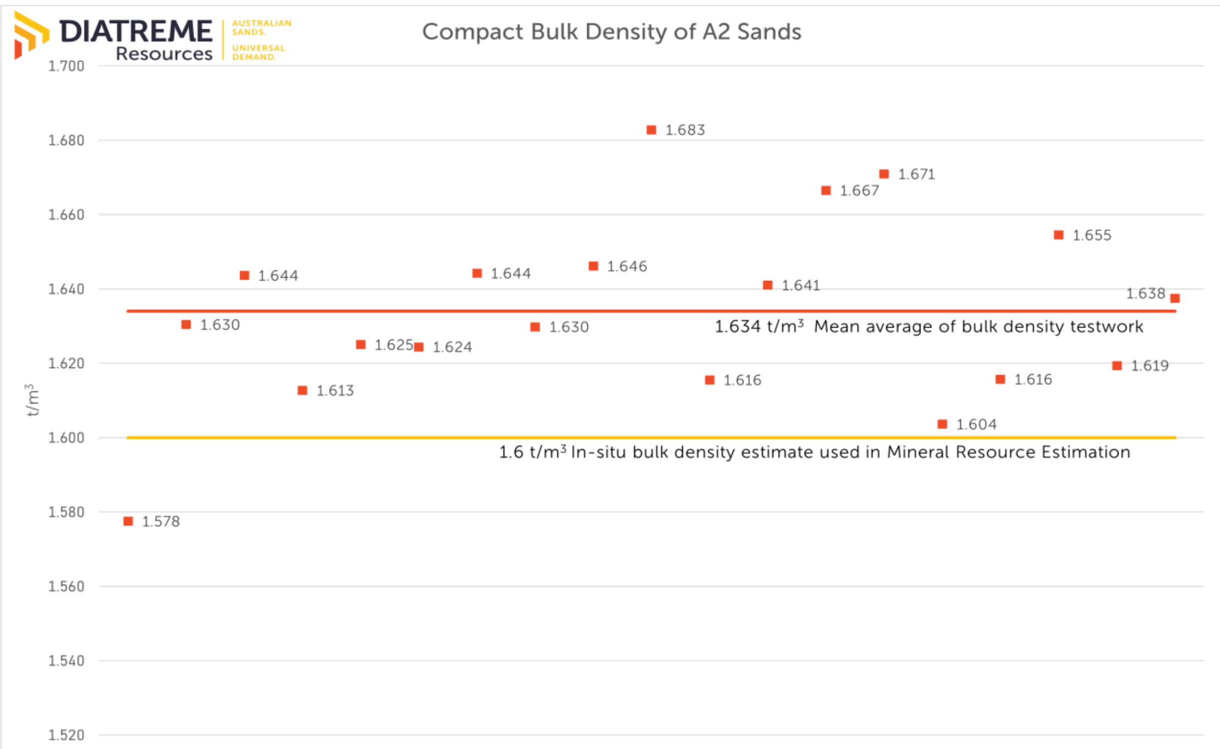


Figure 7: Results of A2 sands from Compact Bulk Density Program

A material density of 1.6 t/m3 was used to estimate tonnes for the Mineral Resource Estimate. The material density was determined by bulk density measurements completed on representative samples of the resource area. The chosen density represents an in-situ moisture of approximately 2.5% and a compaction factor of approximately 1.1.

The reported Mineral Resource includes all classified blocks that are in the geological model, located above the basal surface wireframe designated for the silica sand layer and below the surface layer of overburden (topsoil).

CUT OFF GRADES

No cut-off grades were applied to composites or block estimation, however a minimum grade of 98.5% Si was one of the factors that contributed to picking the base of the resource in drillholes. The Mineral Resource is reported from all classified blocks with interpolated SiO_2 grades. To define the geological model/estimation domain, several factors were considered, including the silica (SiO_2 %) grade, sand colour, and contaminant levels. Some intervals of less than 98.5% Si are included within the high purity silica unit however these do not materially dilute estimation.

MINING AND METALLURGICAL METHODS AND PARAMETERS, AND OTHER MATERIAL FACTORS CONSIDERED TO DATE

Metallurgical testwork completed to-date confirms the silica sand resource is readily amenable to upgrading by conventional washing and screening methods to a low iron, high purity silica sand for photovoltaic applications (solar panels).

The potential for economic extraction at the Si2 Project has been evaluated considering various factors including open-pit mining methods, anticipated product specifications, marketability of the product, and advantageous logistics. Based on these considerations, it is concluded that the Si2 Project has Reasonable Prospects for Eventual Economic Extraction (RPEEE) and can be designated as an industrial Mineral Resource according to JORC Code Clause 49.

The results of the Mineral Resource Estimate are provided in Table 1 of this report and the Resource Area is shown in Figure 2. Representative dune profiles across the Resource Area are shown in the Figure 3 of this report.

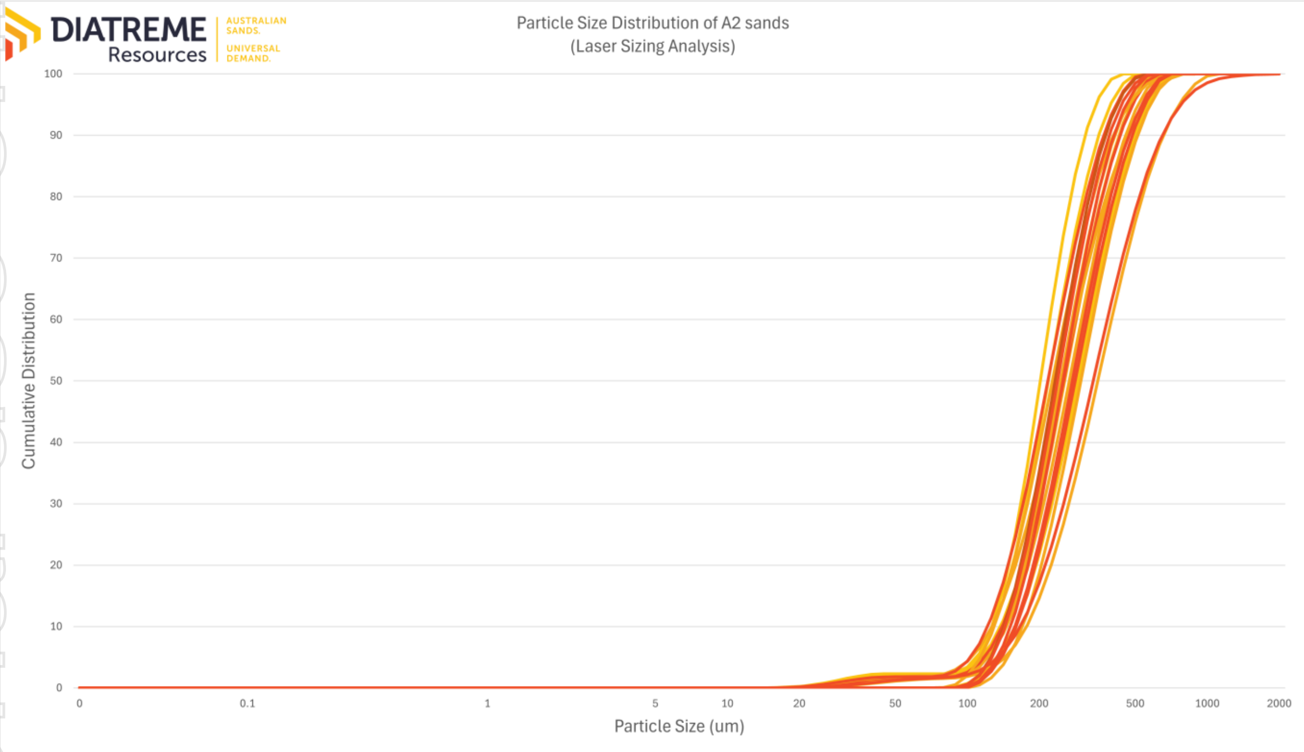


Figure 8: Particle Size Distribution of A2 Sands

Deposit	JORC Resource Category	Silica Sand (Mt)	SiO_2 (%)	Fe_2O_3 (%)	TiO_2 (%)	Al_2O_3 (%)	LOI (%)
Si2	Measured	49.5	99.33	0.11	0.13	0.11	0.12
	Indicated	120.5	99.32	0.10	0.14	0.10	0.14
	Inferred	65	99.20	0.12	0.17	0.12	0.17
	Sub-Total	**235**	**99.29**	**0.11**	**0.15**	**0.11**	**0.14**
Galalar**	Measured	43.12	99.21	0.09	0.11	0.13	0.16
	Indicated	23.12	99.16	0.09	0.13	0.10	0.24
	Inferred	9.22	99.10	0.11	0.16	0.11	0.27
	Sub-Total	**75.46**	**99.18**	**0.09**	**0.12**	**0.12**	**0.20**
WRA*	Indicated	10.3	99.20	0.15	0.24	0.16	0.02
	Inferred	81.4	99.38	0.09	0.15	0.06	0.10
	Sub-Total	**91.7**	**99.36**	**0.10**	**0.16**	**0.07**	**0.09**
Total		**402.16**	**99.31**	**0.10**	**0.15**	**0.09**	**0.12**

Table 2: Mineral Resource Inventory of Diatreme Resources' Silica Sand Projects

- **Refer ASX release September 20th, 2021.
- * Refer ASX release December 6th, 2023.

This announcement is authorised for release by the Board.

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About Diatreme Resources

Diatreme Resources (ASX:DRX) is an emerging Australian producer of mineral and silica sands based in Brisbane. Our key projects comprise the Northern Silica Project and Galalar Silica Sand Project in Far North Queensland, located next to the world's biggest silica sand mine at Cape Flattery.

In Western Australia's Eucla Basin, Diatreme's 'shovel-ready' Cyclone Zircon Project is considered one of a handful of major zircon-rich discoveries of the past decade. Diatreme also holds a 49% interest in the Clermont Copper-Gold Project located in central Queensland. Diatreme has a farm-in agreement with Metallica Minerals Limited (MLM) which already owns a 51% interest, and has provided its intention to earn up to a 75% interest by meeting certain further expenditure obligations of an additional $1 million.

Diatreme has an experienced Board and management, with expertise across all stages of project exploration, mine development and project financing together with strong community engagement skills.

Global material solutions group Sibelco is Diatreme's development partner on its Queensland silica projects portfolio. Sibelco has completed a two-tranche investment of $35 million taking its total project interest to 26.8%, with the balance (73.2%) held by Diatreme. In addition, Sibelco made a $13.97 million investment at the corporate level.

Diatreme's silica sand resources will contribute to global decarbonisation by providing the necessary high-grade silica for use in the solar PV industry. The Company has a strong focus on ESG, working closely with its local communities and all other key stakeholders to ensure the long-term sustainability of our operations, including health, safety and environmental stewardship.

For more information, please visit www.diatreme.com.au

ASX releases referenced for this release:

- Diatreme advances NSP's EIS, port planning – 21 March 2024
- Galalar Silica Resource Expands by 22% to 75.5 Mt – 20 September 2021
- New maiden 91.7Mt silica resource at Western Resource Area – 6 December 2023

Diatreme confirms that it is not aware of any new information or data that materially affects the information included in the original releases and that all material assumptions and technical parameters underpinning the estimates in the original releases continue to apply and have not materially changed. Diatreme confirms that the form and context in which the competent person's findings are presented have not been materially modified from the original releases.

COMPETENT PERSONS STATEMENT

The information in this report that relates to Exploration Targets & Exploration Results is based on information compiled by Mr Frazer Watson, a Competent Person who is a Member of The Australasian Institute of Mining and Metallurgy, and the Australian Institute of Geoscientists. Mr Watson is a full-time employee of Diatreme Resources Limited. Mr Watson has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resource and Ore Reserves'. Mr Watson consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

The information in this report that relates to Mineral Resource at the Si2 Deposit is based on the work carried out by Mr Chris Ainslie, Senior Resource Geologist. Mr Ainslie is an employee of Measured Group Pty Ltd and a Member of the Australian Institute of Geoscientists. Mr Ainslie worked under the supervision of Mr Lyon Barrett, Principal Resource Geologist who is Managing Director of Measured Group Pty Ltd and a Member of the Australasian Institute of Mining & Metallurgy. Measured Group Pty Ltd have been engaged by Cape Silica Holdings Pty Ltd (CSHPL) to prepare this independent report and there is no conflict of interest between the parties. Mr Barrett has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity for which he is undertaking to qualify as a Competent Person as defined in the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (The JORC Code). Mr Barrett consents to the inclusion in the report on the matters based on their information in the form and context in which it appears.

The corresponding JORC 2012 Table 1 is attached to this report can be found in Appendix 1.

DIATREME Resources

APPENDIX 1: JORC TABLE 1
SECTION 1 - SAMPLING TECHNIQUES AND DATA

Criteria	Explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	Prior to April 2022; Vacuum (VX), and Hand Auger (HA) drilling samples were collected in 1m intervals (~2kg) after passing through a single-tiered (50/50) riffle splitter. The samples were then sent for analysis, from which up to 250g was pulverised to produce a fused bead for XRF analysis. After April 2022; Aircore (AC), and Hand Auger (HA) drilling samples were collected in 1m intervals (~2kg) after passing through a single-tiered (50/50) riffle splitter. The samples were then sent for analysis, from which 150g was pulverised to produce a fused bead for XRF analysis. Duplicate samples were taken every 25m as the alternate 50% split of a single-tiered riffle splitter, apart from holes where the alternate split was sampled for metallurgy. Correct interval delineation on VX and AC drilling is achieved with metre intervals marked on the drill mast, and samples are collected when the base of the top drive reaches a metre interval. Correct interval delineation on HA sampling is achieved when the top of the metre extension rod reaches ground level. The Competent Person considers the quality of the sampling to be fit for the deposit style, as mineral sands are not readily delineated with sonic or coring methods.
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	Three (3) types of drilling have been utilised for exploration, Aircore (AC), Vacuum (VX and Hand Auger (HA). Hole Depth (EOH) is determined geologically either at the water table or in clayey sands after the base of mineralisation. This is due to the limitations of VX drilling at the water table, and limitations of the compressor on the AC drilling penetrating the clay layers, and also due to observations of proximal miners AC drilling was by a track mounted drill rig with a 3" blade bit, and a rod length of 3m. VX drilling was by a tractor mounted drill rig with a 60mm diameter blade bit, and a rod length of 1.8m Hand Auguring (HA) was conducted using a Dormer Sand Auger with an internal diameter of 2".
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.*	Aircore and Vacuum drilling achieved ~100% sample recovery throughout.

Criteria	Explanation	Commentary
	• *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	Sample recovery is monitored on the rig for a consistent sample size. Hand auger sampling excluded contamination on the outside of the auger, from the sub-samples to prevent cross-contamination. Sample recovery is maximised within a closed system from the drill bit to the riffle splitter. No relationship between recovery and grade has been observed.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.* • *The total length and percentage of the relevant intersections logged.*	All drillholes have been logged in their entirety, with qualitative descriptions of moisture content, lithology, grainsize and colour. Photography is captured at a chip by chip basis using Imago software, colour is extracted from the imagery, and the RGB channels are recorded. The quality of logging is sufficient for exploration and resource definition.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	Prior to April 2022, sample preparation was completed at ALS in Brisbane, using the PUL-33 and SPL-21 methods, where samples are sorted, weighed wet, and then dried at 105°C. Samples are then split using a rotary sample divider, and volumetrically weighed to a nominal 250g before undergoing the PUL-33 method, where sample are pulverised in a tungsten carbide bowl. After April 2022, sample preparation is completed at Bureau Veritas in Adelaide using the PR001 method where samples are sorted, weighed wet, and then dried at 105°C, samples are then split using a rotary sample divider, and volumetrically weighed to a nominal 150g before undergoing the PR305 method where samples are pulverised in a tungsten carbide bowl. These methods are determined to be appropriate by the Competent Person to avoid sample carry-over contamination, in addition Cr is monitored to ensure that pulverisation is performed in a non-ferrous pulverising bowl. Crushing is not required as the grain size of the sample material is a finer grain size than the output of a crusher, and a crushing stage during preparation would introduce contamination to the sub-sample. Field duplicates were submitted at a nominal rate of 1 in 25 in line with the quality assurance procedure. Prior to 2023, this was 1 in 50.

Criteria	Explanation	Commentary
		The variability observed between field duplicate assay results is considered appropriate for the style of mineralisation by the Competent Person. The Competent Person considers the drill sample sizes as appropriate for the grain size of the material, the style of mineralisation and the nature of the drilling program
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	Prior to April 2022, AC and HA samples had undergone sample preparation and geochemical analysis at Australian Laboratory Services (ALS) in Brisbane, Townsville and Perth. All element results were determined by X-Ray Fluorescence Spectrometry (XRF), method code: XRF26, with H2O/LOI determined by thermogravimetric analysis (TGA) using method code OA-GRA05x. As of April 2022, AC and HA samples have undergone sample preparation and geochemical analysis by Bureau Veritas in Adelaide and Whyalla. All element results were determined using XRF, method code: XF100 which is considered a total whole rock analysis. Field duplicates are conducted every 25th sample which is submitted to the lab as blind duplicates, CRM (ELIM22) is utilised at the start of each hole (nominally every 30 samples), and certification of the ELIM22 CRM by OREAS has yet to be finalised. Bureau Veritas conducts its own internal checks, and these results have been provided to Diatreme and are monitored by both parties as part of the quality control process. No sample contamination in the primary or duplicate interval samples has been detected. Coarse flushes of an unpulverized sample matching ELIM22 CRM has been introduced to both clean the lab pulveriser between drillholes, and test for any contamination. The quality control procedures adopted by Diatreme establish an acceptable level of accuracy and precision
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data*	No twinned holes have been performed during this phase of exploration. Collar and geological logging is captured by and stored within the geological logging/database software MX Deposit. Photographic data is captured by Imago, a software package that acts as a repository and analysis tool for geoscientific imagery.

Criteria	Explanation	Commentary
		Assay data is recorded in MX Deposit, a Drillhole Database software.. No adjustment has been made to assay data.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	All drill hole locations have been surveyed using a Handheld GPS (Garmin Montana 700i) which provides accuracy for collar surveys of ± 5m. The collar data is recorded in the UTM coordinate system: Map Grid of Australia 1994 (MGA94) Zone 55, which uses the Geocentric Datum of Australia 1994 (GDA94) datum on the GRS80 ellipsoid. All drill holes are vertical, no down-hole surveying is conducted. LiDAR elevation models (December 2022) were used as the topographic surface.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	First pass drilling spaced nominally at 380m along dune crests, and infill drilling at a nominal 180 - 200m along the trailing arm of an elongate parabolic dune, and in the interdunal valleys. Auger drilling occasionally is performed at the edge of the dune close to water table. The data spacing and distribution has been assessed to establish geological and grade continuity, and is considered by the Competent Person to be more than appropriate for this style of deposit. No sample compositing has been applied.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	The deposit style is an unlithified aeolian sand deposit, comprised of a series of complex parabolic and elongate parabolic dune systems repeatedly reworked and are superimposed upon older dune systems. The vertical drilling intersects the bedforms at an angle which represents the true width of mineralisation. Angled drilling would result in problematic drilling using vacuum and aircore methods in a semi-compacted silica sand. No sampling bias is introduced by the orientation of drilling.
Sample security	• *The measures taken to ensure sample security.*	Samples were sealed by cable-tie in polywoven bags, and securely stored on-site until transported by TNT courier and their third party to Bureau Veritas in Adelaide. All samples were stored in a locked yard prior to transit. Reconciliation reports are provided by the laboratory and checked against the sample submission forms.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	Measured Group has conducted an audit on the drillhole database, but not the sampling techniques.

Criteria	Explanation	Commentary
		Measured Group have found the drillhole data to be of a high standard.

SECTION 2 - REPORTING OF EXPLORATION RESULTS

(Criteria listed in the preceding section also apply to this section.)

Criteria	Explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	The Northern Silica Project, and Casuarina Silica Deposit are located adjacent to the coastline in Far North Queensland, approximately 53km north of Cooktown. The project is adjacent to the south of the Cape Flattery Silica Mines (CFSM) Mining Lease. CFSM has been in operation since 1967 and is Queensland's largest producer of high purity silica and is reported to have the highest production of high purity silica sand of any mine in the world. The project is located at the northern end of the Cape Flattery/Cape Bedford dune field complex within the Exploration Permits for Minerals (EPM) 17795 & 27212. Most of the EPM is located on one land title, Lot 35/SP232620, a freehold lot of 110,000 hectares. The Project and EPM is in the Mareeba Mining District and falls within the Hope Vale Aboriginal Shire Council area. This lies approximately 35km north of the township of Hope Vale, with a population of approximately 1,500 in the Hope Vale Aboriginal Shire Council. EPM 17795 is owned by Northern Silica Pty Ltd, subsidiary of the Joint Venture Cape Silica Holdings Pty Ltd between Diatreme Resources 73.2% and Sibelco 26.8%. EPM 27212 is owned by Cape Silica Holdings Pty Ltd. Diatreme was granted a renewal on EPM 17795 "Cape Bedford" until 21 June 2026. Targeting heavy mineral sand and silica sand. The EPM was granted under protected Native Title Protection Conditions. As of April 2024, the tenure is in good standing. EPM 17795 is an extensive EPM comprising 147 continuous subblocks (approximately 480km2) covering the majority of the Cape Flattery-Cape Bedford Quaternary dune field complex. Three EPM's contiguous with EPM 17795 have been taken up by Diatreme, EPM 27212 (granted 27th September 2021), EPM 27265 (granted 30th January 2020) and application EPM 27430 (granted 26th October 2021). These tenements cover small areas of the dune field not covered by EPM 17795. EPM 27212 is held by Cape Silica Holdings Pty Ltd, EPM 27430, EPM 27265 are held by Northern Silica Pty Ltd. Cape Silica Holdings and its subsidiaries have two mining lease applications currently undergoing approvals, ML100235, ML100308, and four

Criteria	Explanation	Commentary
		accompanying mining lease infrastructure applications, ML 100310, ML 100311, ML 100312, ML 100313. Casuarina Silica Pty Ltd, a subsidiary of Diatreme Resources has a mining lease approval underway (ML100309).
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	Exploration for silica sand has been undertaken in the Cape Flattery - Cape Bedford area in 11 Authorities to Prospect (ATP's) or Exploration Permits for Minerals (EPMs) since the 1960's. In general, past exploration of the dune field has primarily focused on the prominent active parabolic dunes of clean white silica sand. Potential for economic concentrations of heavy mineral sand also exists throughout the lower dune elevation and older sand areas. As there are no assay certificates for this historic data, and the locations of which are dubious, the data it is considered qualitative and is not used for Mineral Resource Estimation, or Exploration Targeting.
Geology	• *Deposit type, geological setting and style of mineralisation.*	The Northern Silica Project is comprised of unlithified aeolian dune complexes. The Cape Flattery & Cape Bedford dune fields are aeolian dunes established in the Pleistocene epoch and regularly remobilised during the Pleistocene and Holocene epochs. The dune fields are situated on a coastal plain overlying the Hodgkinson Formation basement with Dalrymple Sandstone forming mesa on basement highs. Mineralisation is thought to be due to repeated eluviation and illuviation events on immobilised dune systems comprised of an existing quartzose sand source. Deleterious metals are thought to have been eluviated by organic acids, transported vertically down through the dunes and illuviated either by binding to clay rich horizons, or in the water table.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* • *easting and northing of the drill hole collar* • *elevation or RL (Reduced Level - elevation above sea level in metres) of the drill hole collar* • *dip and azimuth of the hole* • *down hole length and interception depth* • *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding*	All collar information for drillholes has been aggregated in the Table of Material Drillholes attached as an appendix to this report.

Criteria	Explanation	Commentary
	of the report, the Competent Person should clearly explain why this is the case	
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated*	Data aggregation is a calculation of the mean average on the respective podzolization profiles across mineralised and non-mineralised zones. All intercepts have been aggregated in the Table of Material Drillholes attached as an appendix to this report. The aggregation of results is of all results considered to be mineralised A2 aeolian sands.
Relationship between mineralisation widths and intercept length	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. • If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	All drilling was vertical (-90°) intersecting undulating flat-lying aeolian dune sands. Downhole length correlates with true width.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• Plan view of drill hole collar locations and appropriate sectional views are within the text.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	All mineralised silica sand results are reported. Where the results in the table are not published, there is either organic style in the first metre, or unmineralized sands / sandy clays below the mineralised horizon.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Fe_2O_3 percentage is the most significant limiting factor on conversion of ore to high purity silica sand product and determines value after SiO_2 percentage. Fe_2O_3 when found in association with TiO_2, does not act as a contaminant or barrier to refining high- purity silica sand, with testing showing gravity separation to accurately remove this impurity. Mineralisation is unlithified quartzose sand.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).*	Undertake infill drilling to complete a semi-gridded coverage across the wider-tested drill areas to enable further upgrade of the Mineral Resource categories and size.

Criteria	Explanation	Commentary
	• *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	In particular, the B1 horizon needs to be checked and tested in the interdune locations by drilling to assist better defining geological continuity and support potential upgrade areas. Review the model and especially isolated drillhole and assay anomalies, including high Fe_2O_3 zones. Verify topsoil thickness across the resource area, given the variation in vegetation density throughout the Resource Area. Inclusion of additional CRM to better encompass the grade distribution of key deleterious elements. Implementation of more precise assay methods to better understand the nature of deleterious elements. Assessment of hyperspectral responses to a broad suite of samples to ascertain whether hyperspectral imagery can assist in producing a geometalurgical model. Maintain regular "certified" bulk density measurements in future drill programs. Maintain regular "certified" particle size work in future drill programs. Establishment of a geometallurgical model to underpin the relationship between head grade and amenability to processing.

SECTION 3 - ESTIMATION AND REPORTING OF MINERAL RESOURCES

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	Explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	The estimate of Mineral Resources for the Si2 Deposit contained within this report is based on information provided by CSHPL, as well as other published and unpublished data relevant to the area. Measured Group applied a first-principles approach to understanding and interpreting the geology of the deposit, through evaluating all available drillhole data and historical reports. This Mineral Resource Estimate is based on four drilling campaigns conducted by Diatreme Resources, and by way of joint venture, CSHPL. The associated geological data was supplied to Measured Group by CSHPL. This data was independently reviewed by Measured's resource geologists and is considered by the Competent Persons to be appropriate and reasonable for the purpose of estimating Mineral Resources according to the guidelines of the JORC Code (2012). The data, used by Measured for resource estimation, includes but is not limited to: - Drillhole collar information inclusive of total depth drilled per hole; - Drillhole lithological data identified; - Sample table and associated sample assays; - Sample Recovery; - Metallurgical Testwork; - Density Measurements; - QAQC Data
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	The Competent Person has not completed a site visit to the Si2 Deposit, however Senior Resource Geologist Chris Ainslie who assisted with the resource modelling completed a site visit on 18 October 2022 and has extensive experience of the dunefield complex.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.*	Silica sand mineralisation at the Si2 Deposit occurs within the Cape Bedford / Cape Flattery Dune Field. The targeted silica sand deposits are the trailing arms and apex of elongate parabolic aeolian sand dunes. The mineral resource is generally constrained to the trailing arms and apex of elongate parabolic dunes, which can be clearly defined using the surface LiDAR imaging. Drilling often intersects overlapped dunal

Criteria	Explanation	Commentary
	• *The factors affecting continuity both of grade and geology.*	features, which are not represented by LiDAR or aerial photography. Conversely, the interdunal areas are often devoid of thick aeolian sand and predominantly exhibit exposed B1 horizons, clays, bedrock, or other sediments. Where drilling has intersected obscured silica sand mineralisation, the sampled sand has been included in the geological model. There is an observable basement high coincident with the topographic high towards the coastline on the western dunes.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	The Mineral Resource Estimate spans a total area of approximately 1270 hectares with varying dimensions: a maximum length along strike of 7.8 km and a width up to 2.7 km. The average thickness of the resource is 11.6 meters, though it can reach up to 55 meters. The top of the resource varies in elevation from 21.9mRL to 108.5 mRL, corresponding to the topography, while the bottom ranges from 16.9 mRL to 75.6 mRL, aligning with the water table or resource basement level.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* • *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* • *The assumptions made regarding recovery of by-products.* • *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).* • *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* • *Any assumptions behind modelling of selective mining units.* • *Any assumptions about correlation between variables.* • *Description of how the geological interpretation was used to control the resource estimates.* • *Discussion of basis for using or not using grade cutting or capping.*	The Mineral Resources were estimated by modelling of the high-purity silica sand. The geological model incorporated several key parameters. The topography surface was surveyed using LIDAR techniques to a resolution of 1m horizontally and 10cm relative vertical accuracy. The top surface of the resource volume was set at 0.3m below the LIDAR topography, representing the base of the topsoil. The bottom surface of the resource volume was constructed from: - The base depth of the Silica Sand unit determined from drilling - The depth of the groundwater table determined from drilling - Interpretation of the dune edge from LiDAR survey and aerial imagery The resource boundary was established by geological interpretation and through analysis of surface dune extents visible in LIDAR, and aerial imagery. A block model was generated to estimate the deposit grade. The orientation of the block model was set to the average strike of the dunes (315 degrees). The dimensions for the parent blocks were determined as 100m across strike by 50m along strike by 3m vertical, which were then subdivided into sub-blocks of 5x5x1m to best fit the undulating geological model.

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Criteria	Explanation	Commentary
	• *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	Grade estimation was completed using ordinary kriging, and a validation check estimate was completed using inverse distance weighting squared. The Ordinary Kriging (OK) method was used to estimate the grades and populate the block model for SiO_2, Fe_2O_3, TiO_2, Al_2O_3 and LOI. The grade estimation process was conducted over 4 (four) sequential passes, each defined by specific search radii that help to guide to the categories of 'Measured', 'Indicated' and 'Inferred' in resource classification. This methodology involved setting the major sample search parameters for each block horizontally in the average strike direction of the dune (315 degrees), the semi-major search direction is also set horizontal (perpendicular to the major search direction) across the dune, and the minor search direction is set to vertical. The search distances used for each pass were derived from variography studies, ensuring that the interpolation aligns with the spatial characteristics of the geological data. All passes used a quadrant-based search with the maximum number of samples set at 32 and required a minimum of three drillholes for reliable grade estimation. Block discretisation of 4 x 4 x 4 (X,Y, Z) was employed. A material density of 1.6 t/m^3 was used to estimate tonnes for the Mineral Resource Estimate. The material density was determined by bulk density measurements completed on representative samples of the resource area. The chosen density represents an insitu moisture of approximately 2.5% and a compaction factor of approximately 1.1. The reported Mineral Resource includes all classified blocks that are in the geological model, located above the basal surface wireframe designated for the silica sand layer and below the surface layer of overburden (topsoil).
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	The tonnages are estimated on a dry basis based on recent bulk density testwork that supported a density of 1.6 tonnes per cubic meter which is typical for silica sand deposits
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	No cut-off grades were applied to composites or block estimation, however a minimum grade of 98.5% SiO_2 was one of the factors that contributed to picking the base of the resource in drillholes. The Mineral Resource is reported from all classified blocks with interpolated SiO_2 grades. To define the geological model/estimation domain, several factors were considered, including the SiO_2 grade, sand colour, and contaminant levels. Some intervals of less than

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Criteria	Explanation	Commentary
		98.5% SiO_2 are included within the high purity silica unit however these do not materially dilute estimation.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	It is assumed that the mining factors are comparable to adjacent operations. The 2023 Northern Silica Scoping Study identified that mining operations will involve extracting material directly from the face using a Wheel Loader. Once extracted, the material will be transported to the processing plant either through a conveyor system or via a slurry pipeline. Some intervals of less than 98.5% SiO_2 are included within the high purity silica unit however these do not materially dilute estimation. The upper 300 mm is likely to be topsoil and reserved for rehabilitation purposes. This overburden surface forms the upper boundary of the estimated geological domain and is not included in the Mineral Resource Estimate. Topsoil thickness may vary across the Resource Area based on the vegetation density.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	Metallurgical testwork completed to-date confirms the silica sand resource is readily amenable to upgrading by conventional washing and screening methods to a low iron, high purity silica sand for photovoltaic applications (solar panels). The following information was provided by CSHPL 3994643 report rev1.pdf. This information was released to market on 14 June 2023 in the announcement titled “Positive Scoping Study for Northern Silica Project”. 3507598 report rev 1.0.pdf. This information was released to market on 17 March 2022 in the announcement titled “Resource Grows to 200Mt Across High-Grade Silica Projects”. MT Galalar DFS Bulk Sample Testwork.pdf. This information was released to market on 9 November 2021 in the announcement titled “Galalar PFS and Maiden Ore Reserve. These intial metallurgical test results clearly demonstrate that low iron, high purity silica sands are potentially deliverable. As final products may require tight specifications, further systematic metallurgical testing should be considered from future infill and grade control drilling.
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation.*	Measured has not conducted any environmental assessment in the concession. However, environmental factors are not expected to be a significant issue for eventual economic extraction. The 2023 Northern Silica Scoping Study identified in a processing flowsheet where high Fe, oversize, low

Criteria	Explanation	Commentary
	While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	grade or slimes are rejected from product streams. The material will be stacked to form a replacement dune as a post mining surface, suitable for rehabilitation. The flocculants used in processing are considered to environmentally neutral.
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	A material density of 1.6 t/m^3 was used to estimate tonnes for the Mineral Resource Estimate. The material density was determined by bulk density measurements completed on representative samples of the resource area. The chosen density represents an insitu moisture of approximately 2.5% and a compaction factor of approximately 1.1.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	The Mineral Resource has been classified according to the principles of the JORC Code (2012 edition). The resource has been divided into Measured, Indicated, and Inferred categories, corresponding to a high, moderate and low level of confidence in the structural and grade continuity of the resource. The classification integrates several key factors, including: depth of geological knowledge of the deposit, geological and mineralisation continuity, drill hole spacing, and the results of quality control measures. Points of Observation are defined as intersections of the silica sand unit, with appropriate assay analysis. Interpretive data includes LIDAR survey interpretation of the top and base of the dunes. The classification also considers drill hole logging, analytical results from drill samples, geostatistical analysis, and confidence in geological and grade continuity, along with recent metallurgical/process test outcomes. Additionally, search and interpolation parameters, recently completed density data, and considerations from JORC Code Clause 49 are factored into the classification process. All relevant factors have been considered and the result reflects the Competent Person's view of the deposit.

Criteria	Explanation	Commentary
Audits or reviews.	• *The results of any audits or reviews of Mineral Resource estimates.*	Internal reviews of the Mineral Resource Estimate were conducted and confirmed that the results were robust and aligned with industry standards.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	The resource classification is considered to address the level of confidence in the resource distribution and grade variability across the deposit on a global basis The known nature and formation of the dune sands places a high degree of confidence in the geological interpretation. In addition to this, consistent high silica grades achieved in drill holes and continuity of geology and grade can be readily identified and traced between all drill holes. A detailed topographic survey (LIDAR) provides a high level of confidence in the estimated volume of the dunes. The interpreted geology of the Si2 Deposit is robust, and any alternative interpretation of the deposit is considered unlikely to have a material influence on the Mineral Resource Estimate undertaken.

APPENDIX 2: TABLE OF MATERIAL DRILLHOLES

Hole ID	Easting (m)	Northing (m)	Collar RL (m)	Stage	New Release	Drill Type	Hole Depth (m)	From (Top of Resource)	To (Bottom of Resource)	SiO_2	Fe_2O_3	TiO_2	Al_2O_3	LOI
AH001	306235	8342968	27.8	Stage 4		HA	2.0	0.3	2.0	99.2	0.1	0.4	0.1	0.1
PLT002	306128	8342658	32.7	Stage 3		VX	3.5	0.3	3.5	98.8	0.1	0.2	0.1	0.4
PLT003	306306	8342713	30.8	Stage 3		VX	6.0	0.3	6.0	99.3	0.0	0.1	0.0	0.1
PLT004	306470	8342753	28.8	Stage 3		VX	5.0	0.3	5.0	99.0	0.1	0.3	0.1	0.3
PLT005	306640	8342691	31.2	Stage 3		VX	4.0	0.3	4.0	98.9	0.1	0.2	0.1	0.2
PLT006	306874	8342702	31.4	Stage 3		VX	2.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
PLT007	307012	8342825	31.6	Stage 3		VX	2.0	0.3	2.0	99.1	0.0	0.1	0.0	0.4
PLT008	307025	8342934	31.0	Stage 3		VX	2.0	0.3	2.0	99.6	0.0	0.0	0.0	0.1
PLT009	307169	8343040	31.1	Stage 3		VX	2.0	0.3	2.0	99.6	0.0	0.1	0.0	0.2
PLT010	307275	8343190	31.2	Stage 3		VX	2.5	0.3	2.5	99.5	0.0	0.0	0.0	0.2
PLT011A	307086	8343331	32.9	Stage 3		VX	4.0	0.3	4.0	99.2	0.1	0.1	0.0	0.1
PLT011B	307090	8343326	33.0	Stage 3		VX	6.0	0.3	6.0	99.0	0.1	0.2	0.1	0.1
PLT012	306693	8342909	34.4	Stage 3		VX	5.7	0.3	5.7	99.1	0.0	0.1	0.1	0.1
PLT057	306729	8342498	30.9	Stage 1		VX	2.5	0.3	2.5	99.0	0.1	0.2	0.1	0.5
PLT058	306945	8342398	32.5	Stage 1		VX	2.8	0.3	2.8	99.0	0.1	0.1	0.1	0.4
PLT059	307090	8342263	31.9	Stage 1		VX	1.7	0.3	1.7	98.9	0.1	0.1	0.1	0.4
PLT060	307299	8342196	35.7	Stage 1		VX	5.0	0.3	5.0	99.1	0.1	0.2	0.1	0.3
PLT061	307422	8342014	33.5	Stage 1		VX	3.0	0.3	3.0	99.3	0.1	0.1	0.1	0.1
PLT062	307592	8341948	37.7	Stage 1		VX	6.7	0.3	6.7	99.3	0.1	0.1	0.1	0.3
PLT063	307741	8341786	38.5	Stage 1		VX	7.5	0.3	7.5	99.1	0.1	0.2	0.1	0.3
PLT064	307908	8341688	39.6	Stage 1		VX	8.5	0.3	8.5	99.6	0.0	0.1	0.1	0.2
PLT065	308038	8341524	46.0	Stage 1		VX	17.0	0.3	14.0	99.5	0.0	0.1	0.1	0.3
PLT066	307875	8341341	53.6	Stage 1		VX	23.5	0.3	23.5	99.6	0.1	0.1	0.1	0.1
PLT067	307691	8341466	49.8	Stage 1		VX	19.5	0.3	19.5	99.4	0.1	0.2	0.1	0.2
PLT068	308033	8341199	51.6	Stage 1		VX	32.5	0.3	16.0	99.7	0.1	0.1	0.1	0.2
PLT069	307575	8341081	73.8	Stage 1		VX	40.0	0.3	40.0	99.0	0.2	0.3	0.1	0.2
PLT070	305852	8342335	41.6	Stage 1		VX	10.0	0.3	10.0	99.2	0.1	0.2	0.1	0.1
PLT071	305916	8342239	40.6	Stage 1		VX	9.7	0.3	9.7	99.5	0.0	0.1	0.1	0.2
PLT072	305924	8341992	46.1	Stage 1		VX	15.5	0.3	15.5	99.2	0.1	0.1	0.1	0.3
PLT073	306133	8342028	36.9	Stage 1		VX	8.5	0.3	8.5	99.6	0.1	0.1	0.1	0.1
PLT074	306062	8341879	40.8	Stage 1		VX	10.8	0.3	10.8	99.5	0.1	0.2	0.1	0.1
PLT075	306120	8341683	41.1	Stage 1		VX	11.0	0.3	11.0	99.4	0.1	0.2	0.1	0.2
PLT076	306266	8341551	34.3	Stage 1		VX	4.4	0.3	4.4	99.5	0.0	0.1	0.1	0.3
PLT077	306459	8341498	36.4	Stage 1		VX	7.0	0.3	7.0	99.1	0.1	0.2	0.1	0.2
PLT078	306596	8341360	34.2	Stage 1		VX	6.0	0.3	6.0	99.3	0.0	0.2	0.1	0.2
PLT079	307443	8341253	65.6	Stage 1		VX	37.0	0.3	28.0	99.1	0.2	0.3	0.1	0.1
PLT080	307348	8341408	58.3	Stage 1		VX	31.0	0.3	29.0	99.2	0.1	0.1	0.1	0.1
PLT081	307163	8341498	56.4	Stage 1		VX	3.0	0.3	3.0	98.6	0.2	0.3	0.1	0.3
PLT081A	307169	8341493	57.1	Stage 1		VX	27.0	0.3	22.0	99.2	0.1	0.2	0.1	0.2
PLT082	307014	8341625	50.3	Stage 1		VX	22.0	0.3	22.0	99.4	0.1	0.1	0.1	0.2
PLT083	306847	8341748	49.5	Stage 1		VX	20.5	0.3	20.5	99.4	0.1	0.2	0.1	0.1

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Unit 8, 55–61 Holdsworth St
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DIATREME Resources

Hole ID	Easting (m)	Northing (m)	Collar RL (m)	Stage	New Release	Drill Type	Hole Depth (m)	From (Top of Resource)	To (Bottom of Resource)	SiO_2	Fe_2O_3	TiO_2	Al_2O_3	LOI
PLT084	306711	8341872	49.1	Stage 1		VX	20.0	0.3	20.0	99.5	0.1	0.1	0.1	0.2
PLT085	306552	8342503	30.3	Stage 1		VX	3.0	0.3	3.0	98.4	0.0	0.1	0.4	0.7
PLT086	306545	8342301	30.2	Stage 1		VX	3.0	0.3	3.0	98.7	0.1	0.1	0.2	0.7
PLT087	306612	8342102	31.0	Stage 1		VX	3.0	0.3	3.0	98.8	0.1	0.3	0.1	0.6
PLT088	307690	8340916	66.6	Stage 1		VX	35.0	0.3	35.0	99.4	0.1	0.2	0.1	0.1
PLT089	307833	8340766	58.6	Stage 1		VX	26.0	0.3	26.0	99.5	0.1	0.1	0.1	0.2
PLT090	307998	8340691	68.4	Stage 1		VX	30.0	0.3	30.0	99.3	0.1	0.2	0.1	0.1
PLT091	308189	8341067	48.0	Stage 1		VX	26.5	0.3	12.0	98.9	0.2	0.3	0.1	0.2
PLT092	308340	8340919	45.3	Stage 1		VX	14.5	0.3	8.0	99.0	0.2	0.3	0.1	0.3
PLT093	308511	8340772	44.9	Stage 1		VX	14.5	0.3	10.0	99.3	0.1	0.2	0.1	0.2
PLT094	307052	8341354	54.7	Stage 1		VX	26.0	0.3	26.0	99.2	0.1	0.1	0.1	0.1
PLT095	306985	8341251	60.2	Stage 1		VX	32.0	0.3	32.0	99.0	0.1	0.2	0.1	0.2
PLT096	306829	8341213	54.8	Stage 1		VX	26.0	0.3	26.0	99.2	0.1	0.1	0.0	0.2
PLT097	306930	8341133	63.4	Stage 1		VX	35.0	0.3	35.0	99.1	0.1	0.2	0.1	0.1
PLT098	307020	8341119	70.3	Stage 1		VX	42.5	0.3	42.5	99.1	0.1	0.1	0.1	0.2
PLT099	306933	8341010	71.0	Stage 1		VX	42.0	0.3	42.0	99.2	0.1	0.1	0.1	0.1
PLT100	307049	8341005	68.5	Stage 1		VX	39.5	0.3	39.5	99.2	0.1	0.1	0.1	0.1
PLT101	306975	8340923	66.5	Stage 1		VX	36.5	0.3	36.5	99.3	0.1	0.1	0.1	0.1
PLT102	307040	8340830	58.5	Stage 1		VX	27.0	0.3	27.0	99.2	0.1	0.2	0.1	0.1
PLT103	307115	8340756	56.9	Stage 1		VX	25.0	0.3	25.0	99.4	0.1	0.2	0.1	0.1
PLT104	308562	8340590	63.3	Stage 2		VX	35.0	0.3	33.0	99.3	0.1	0.1	0.1	0.1
PLT105	308684	8340431	49.8	Stage 2		VX	26.0	0.3	23.0	99.4	0.1	0.2	0.1	0.2
PLT106	308893	8340402	42.2	Stage 2		VX	14.0	0.3	14.0	99.3	0.1	0.1	0.1	0.2
PLT107	309033.4	8340253	38.7	Stage 2		VX	10.5	0.3	10.5	99.1	0.1	0.1	0.1	0.2
PLT108	309145	8340061	52.0	Stage 2		VX	24.0	0.3	24.0	99.1	0.1	0.2	0.1	0.1
PLT109	309285	8339886	67.0	Stage 2		VX	39.0	0.3	39.0	99.0	0.2	0.3	0.1	0.1
PLT110	309472	8339788	69.2	Stage 2		VX	42.0	0.3	42.0	99.1	0.1	0.2	0.1	0.1
PLT111	309648	8339677	51.2	Stage 2		VX	23.5	0.3	23.5	99.2	0.1	0.1	0.1	0.2
PLT112	309799	8339540	49.9	Stage 2		VX	22.0	0.3	22.0	99.3	0.1	0.1	0.1	0.2
PLT113	309957	8339410	41.5	Stage 2		VX	14.5	0.3	14.5	99.2	0.1	0.2	0.1	0.1
PLT114	310120	8339280	44.5	Stage 2		VX	17.5	0.3	17.0	99.1	0.1	0.2	0.1	0.2
PLT115	310331	8339163	56.2	Stage 2		VX	29.0	0.3	29.0	98.8	0.2	0.4	0.1	0.1
PLT116	310478	8339020	48.3	Stage 2		VX	22.0	0.3	22.0	99.3	0.1	0.1	0.1	0.1
PLT117	310614	8338868	43.9	Stage 2		VX	18.5	0.3	18.5	99.2	0.1	0.2	0.1	0.2
PLT118	310478	8338620	53.3	Stage 2		VX	28.0	0.3	25.0	99.4	0.1	0.1	0.1	0.1
PLT119	310321	8338751	62.6	Stage 2		VX	37.0	0.3	35.0	99.3	0.1	0.1	0.1	0.2
PLT120	310172	8338884	54.9	Stage 2		VX	29.5	0.3	29.5	99.3	0.1	0.1	0.1	0.2
PLT121	310027	8339033	50.8	Stage 2		VX	25.0	0.3	25.0	99.1	0.1	0.2	0.1	0.2
PLT122	309872	8339172	54.6	Stage 2		VX	29.0	0.3	29.0	99.4	0.1	0.1	0.1	0.2
PLT123	309733	8339302	56.5	Stage 2		VX	32.0	0.3	31.0	99.5	0.1	0.1	0.1	0.1
PLT124	309607	8339452	62.2	Stage 2		VX	40.0	0.3	40.0	99.1	0.2	0.3	0.1	0.2
PLT125	309477	8339606	59.1	Stage 2		VX	34.0	0.3	34.0	99.4	0.1	0.1	0.1	0.1
PLT126	309306	8339726	68.0	Stage 2		VX	42.0	0.3	42.0	99.4	0.1	0.2	0.1	0.1
PLT127	309236	8339622	62.6	Stage 2		VX	30.0	0.3	29.0	99.3	0.2	0.2	0.1	0.2

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Unit 8, 55–61 Holdsworth St
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Hole ID	Easting (m)	Northing (m)	Collar RL (m)	Stage	New Release	Drill Type	Hole Depth (m)	From (Top of Resource)	To (Bottom of Resource)	SiO_2	Fe_2O_3	TiO_2	Al_2O_3	LOI
PLT128	310260	8338610	44.9	Stage 2		VX	12.0	0.3	10.0	99.4	0.1	0.1	0.1	0.2
PLT129	310110	8338773	59.5	Stage 2		VX	31.0	0.3	29.0	99.5	0.1	0.1	0.1	0.1
PLT130	310236	8338278	50.4	Stage 2		VX	21.0	0.3	18.0	99.4	0.1	0.1	0.1	0.1
PLT131	310094	8338415	54.5	Stage 2		VX	21.0	0.3	19.0	99.1	0.1	0.2	0.1	0.1
PLT132	309971	8338566	59.2	Stage 2		VX	31.0	0.3	23.0	99.1	0.1	0.2	0.1	0.1
PLT133	309888	8338764	63.2	Stage 2		VX	36.8	0.3	29.0	99.0	0.1	0.2	0.1	0.1
PLT134	309743	8338905	66.8	Stage 2		VX	44.5	0.3	38.0	99.1	0.1	0.1	0.1	0.1
PLT135	309591	8339046	62.8	Stage 2		VX	33.0	0.3	29.0	99.1	0.1	0.1	0.1	0.1
PLT136	309427	8339160	62.7	Stage 2		VX	25.0	0.3	22.0	99.3	0.1	0.1	0.1	0.2
PLT137	309276	8339287	57.1	Stage 2		VX	2.0	0.3	2.0	99.7	0.1	0.2	0.1	0.2
PLT243	307200	8342658	47.3	Stage 3		VX	9.0	0.3	9.0	99.4	0.1	0.0	0.1	0.1
PLT244	307226	8340676	54.7	Stage 3		VX	23.0	0.3	23.0	99.2	0.1	0.1	0.1	0.2
PLT245	307340	8340880	60.8	Stage 3		VX	30.0	0.3	30.0	99.3	0.1	0.1	0.1	0.1
PLT246	307531	8340772	49.7	Stage 3		VX	17.7	0.3	17.7	99.2	0.1	0.1	0.1	0.3
PLT247	307196	8341060	59.7	Stage 3		VX	33.0	0.3	32.0	99.5	0.0	0.1	0.1	0.1
SI20001	308145	8340578	56.5	Stage 3		AC	22.0	0.3	19.0	99.1	0.2	0.2	0.1	0.1
SI20002	308284	8340441	57.8	Stage 3		AC	30.0	0.3	16.0	99.1	0.1	0.2	0.1	0.2
SI20003	308425	8340270	56.6	Stage 3		AC	15.0	0.3	13.0	99.0	0.2	0.2	0.2	0.1
SI20004	308574	8340155	59.8	Stage 3		AC	28.0	0.3	20.0	99.1	0.1	0.1	0.1	0.2
SI20005	308707	8340042	58.3	Stage 3		AC	31.0	0.3	19.0	99.2	0.1	0.1	0.2	0.2
SI20006	308835	8339897	51.9	Stage 3		AC	18.0	0.3	16.0	99.2	0.2	0.2	0.2	0.2
SI20007	308948	8339714	56.2	Stage 3		AC	21.0	0.3	12.0	99.2	0.1	0.2	0.1	0.3
SI20008	308940	8339610	63.1	Stage 3		AC	24.0	0.3	22.0	99.1	0.1	0.2	0.2	0.3
SI20009	309149	8339410	64.5	Stage 3		AC	24.0	0.3	21.0	99.4	0.1	0.1	0.1	0.2
SI20010	309273	8339302	58.1	Stage 3		AC	21.0	0.3	15.0	99.4	0.1	0.1	0.1	0.1
SI20011	308773	8339692	45.2	Stage 3		AC	21.0	0.3	10.0	99.5	0.1	0.1	0.1	0.2
SI20012	308556	8339819	59.0	Stage 3		AC	36.0	0.3	22.0	99.4	0.1	0.1	0.1	0.1
SI20013	308176	8339942	62.5	Stage 3		AC	30.0	0.3	30.0	99.5	0.0	0.1	0.1	0.1
SI20014	308102	8340023	66.0	Stage 3		AC	39.0	0.3	36.0	99.5	0.1	0.1	0.1	0.1
SI20015	307848	8340174	55.9	Stage 3		AC	30.0	0.3	30.0	99.3	0.1	0.1	0.2	0.2
SI20016	307613	8340356	59.1	Stage 3		AC	30.0	0.3	30.0	99.3	0.1	0.2	0.1	0.2
SI20017	307511	8340427	61.6	Stage 3		AC	30.0	0.3	30.0	99.2	0.1	0.2	0.1	0.2
SI20018	307381	8340571	54.2	Stage 3		AC	27.0	0.3	27.0	99.4	0.1	0.1	0.1	0.2
SI20019	310064	8336235	107.4	Stage 3		AC	54.0	0.3	54.0	99.1	0.2	0.2	0.1	0.2
SI20020	309878	8336620	99.3	Stage 3		AC	40.0	0.3	37.0	99.3	0.1	0.1	0.1	0.2
SI20021	309665	8336919	79.1	Stage 3		AC	21.0	0.3	18.0	99.2	0.1	0.2	0.1	0.2
SI20022	309350	8337164	73.8	Stage 3		AC	21.0	0.3	19.0	99.4	0.1	0.1	0.1	0.1
SI20023	309132	8337451	75.8	Stage 3		AC	36.0	0.3	31.0	99.3	0.1	0.1	0.1	0.1
SI20024	308905	8337756	63.9	Stage 3		AC	27.0	0.3	24.0	99.2	0.1	0.2	0.1	0.2
SI20025	308709	8338026	74.9	Stage 3		AC	39.0	0.3	36.0	99.2	0.1	0.2	0.1	0.2
SI20026	308519	8338229	53.3	Stage 3		AC	21.0	0.3	18.0	99.3	0.1	0.2	0.1	0.2
SI20027	308289	8338470	57.1	Stage 3		AC	27.0	0.3	27.0	99.3	0.1	0.2	0.1	0.2
SI20028	308278	8338754	68.3	Stage 3		AC	36.0	0.3	36.0	99.4	0.1	0.1	0.1	0.1
SI20029	308082	8338996	52.7	Stage 3		AC	21.0	0.3	21.0	99.3	0.1	0.2	0.1	0.1

Hole ID	Easting (m)	Northing (m)	Collar RL (m)	Stage	New Release	Drill Type	Hole Depth (m)	From (Top of Resource)	To (Bottom of Resource)	SiO_2	Fe_2O_3	TiO_2	Al_2O_3	LOI
SI20030	307943	8339384	48.6	Stage 3		AC	18.0	0.3	18.0	99.4	0.1	0.2	0.1	0.1
SI20031	307771	8339729	60.7	Stage 3		AC	30.0	0.3	30.0	99.4	0.1	0.1	0.1	0.2
SI20032	308204	8339539	50.3	Stage 3		AC	30.0	0.3	30.0	99.3	0.1	0.1	0.1	0.2
SI20033	308496	8339245	44.2	Stage 3		AC	9.0	0.3	5.0	99.2	0.1	0.1	0.1	0.2
SI20034	308770	8338987	42.4	Stage 3		AC	9.0	0.3	4.0	99.0	0.2	0.2	0.2	0.4
SI20035	309042	8338647	62.2	Stage 3		AC	21.0	0.3	19.0	99.6	0.1	0.1	0.1	0.1
SI20036	309266	8338378	77.5	Stage 3		AC	34.0	0.3	33.0	99.4	0.1	0.2	0.1	0.1
SI20037	309315	8338154	96.1	Stage 3		AC	48.0	0.3	47.0	99.3	0.1	0.1	0.1	0.2
SI20038	309689	8337961	67.4	Stage 3		AC	36.0	0.3	29.0	99.2	0.1	0.2	0.1	0.2
SI20039	309932	8337729	61.2	Stage 3		AC	21.0	0.3	19.0	99.3	0.1	0.1	0.1	0.1
SI20040	310118	8337442	71.6	Stage 3		AC	21.0	0.3	19.0	99.1	0.2	0.3	0.1	0.1
SI20041	310338	8337128	78.9	Stage 3		AC	21.0	0.3	18.0	99.3	0.1	0.1	0.1	0.2
SI20042	310531	8336832	107.9	Stage 3		AC	51.0	0.3	49.0	99.2	0.2	0.2	0.1	0.1
SI20043	310178	8336887	69.8	Stage 3		AC	6.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI20044	310050	8337151	69.7	Stage 3		AC	9.0	0.3	7.0	98.5	0.3	0.4	0.2	0.4
SI20045	309807	8337344	68.2	Stage 3		AC	12.0	0.3	7.0	99.1	0.2	0.2	0.2	0.2
SI20046	309566	8337584	75.5	Stage 3		AC	18.0	0.3	15.0	98.6	0.2	0.3	0.1	0.4
SI20047	309357	8337817	58.3	Stage 3		AC	9.0	0.3	6.0	98.9	0.1	0.2	0.1	0.5
SI20048	309141	8338117	58.3	Stage 3		AC	12.0	0.3	9.0	99.1	0.1	0.2	0.1	0.4
SI20049	309932	8337505	61.3	Stage 3		AC	24.0	0.3	14.0	99.3	0.1	0.2	0.1	0.2
SI20050	309606	8337744	66.9	Stage 3		AC	18.0	0.3	15.0	99.2	0.1	0.2	0.1	0.2
SI20051	308937	8338361	66.9	Stage 3		AC	21.0	0.3	19.0	99.1	0.2	0.2	0.2	0.2
SI20052	308608	8338547	60.7	Stage 3		AC	24.0	0.3	22.0	99.1	0.1	0.2	0.1	0.2
SI20053	308191	8338150	48.0	Stage 3		AC	18.0	0.3	16.0	99.1	0.1	0.1	0.1	0.2
SI20054	307709	8339986	40.4	Stage 3		AC	12.0	0.3	12.0	98.9	0.1	0.1	0.2	0.5
SI20055	308407	8339585	34.3	Stage 3		AC	15.0	0.3	6.0	99.1	0.1	0.2	0.1	0.3
SI20056	308925	8339044	44.2	Stage 3		AC	21.0	0.3	17.0	99.3	0.1	0.2	0.1	0.2
SI20057	309577	8338544	41.8	Stage 3		AC	17.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI20058	310117	8337965	38.0	Stage 3		AC	15.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI20059	310608	8337466	48.1	Stage 3		AC	18.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI20060	310388	8337676	38.4	Stage 3		AC	15.0	0.3	7.0	99.6	0.1	0.1	0.1	0.2
SI20061	309835	8338299	37.7	Stage 3		AC	21.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI20062	309305	8338820	35.5	Stage 3		AC	18.0	0.3	16.0	99.4	0.0	0.1	0.1	0.2
SI20063	308659	8339309	42.0	Stage 3		AC	21.0	0.3	19.0	99.3	0.1	0.1	0.1	0.2
SI20064	308425	8339872	50.0	Stage 3		AC	24.0	0.3	20.0	99.1	0.1	0.2	0.1	0.2
SI20065	310505	8338040	47.1	Stage 3		AC	21.0	0.3	13.0	99.2	0.1	0.2	0.1	0.3
SI20066	310854	8337496	67.6	Stage 3		AC	34.0	0.3	32.0	99.2	0.1	0.2	0.1	0.2
SI20067	310801	8337771	46.9	Stage 3		AC	15.0	0.3	10.0	99.0	0.2	0.3	0.1	0.4
SI20068	310389	8338469	39.6	Stage 3		AC	12.0	0.3	7.0	99.1	0.2	0.2	0.1	0.3
SI20069	310866	8338017	31.8	Stage 3		AC	12.0	0.3	11.0	99.0	0.1	0.1	0.2	0.3
SI20070	311098	8337828	30.5	Stage 3		AC	12.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI20071	310588	8338240	31.3	Stage 3		AC	15.0	0.3	9.0	99.1	0.1	0.1	0.1	0.3
SI20072	310881	8338575	35.2	Stage 3		AC	15.0	0.3	15.0	99.3	0.1	0.2	0.1	0.1
SI20073	311317	8338127	43.4	Stage 3		AC	24.0	0.3	24.0	98.6	0.3	0.5	0.2	0.1

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Hole ID	Easting (m)	Northing (m)	Collar RL (m)	Stage	New Release	Drill Type	Hole Depth (m)	From (Top of Resource)	To (Bottom of Resource)	SiO_2	Fe_2O_3	TiO_2	Al_2O_3	LOI
SI20074	311104	8338356	37.9	Stage 3		AC	18.0	0.3	17.0	99.0	0.2	0.3	0.1	0.2
SI20075	310753	8338729	44.0	Stage 3		AC	21.0	0.3	21.0	99.0	0.2	0.2	0.1	0.2
SI20076	307665	8341248	46.4	Stage 3		AC	12.0	0.3	9.0	99.3	0.0	0.1	0.1	0.2
SI20077	307838	8341379	54.8	Stage 4		AC	27.0	0.3	26.0	99.3	0.1	0.1	0.1	0.1
SI20078	307881	8341337	53.6	Stage 4		AC	24.0	0.3	23.0	99.3	0.1	0.1	0.1	0.1
SI20079	308007	8341609	39.3	Stage 4		AC	12.0	0.3	11.0	99.1	0.0	0.1	0.1	0.1
SI20080	307997	8341396	40.3	Stage 4		AC	12.0	0.3	11.0	99.4	0.1	0.1	0.1	0.0
SI20081	307941	8341281	54.0	Stage 4		AC	21.0	0.3	19.0	99.3	0.1	0.1	0.1	0.1
SI20082	308131	8341124	44.5	Stage 4		AC	12.0	0.3	8.0	99.1	0.1	0.2	0.1	0.1
SI21001	309220.5	8339986	53.8	Stage 4	X	AC	30.0	0.3	30.0	99.2	0.2	0.2	0.1	0.2
SI21002	309382.3	8339830	60.8	Stage 4	X	AC	39.0	0.3	37.0	99.4	0.1	0.2	0.1	0.1
SI21003	309562	8339731	60.3	Stage 4	X	AC	36.0	0.3	36.0	99.3	0.1	0.2	0.1	0.2
SI21004	309731	8339594	51.8	Stage 4	X	AC	27.0	0.3	27.0	99.4	0.1	0.1	0.1	0.2
SI21005	309875	8339460	50.8	Stage 4	X	AC	27.0	0.3	27.0	99.5	0.1	0.1	0.1	0.2
SI21006	310036	8339317	48.3	Stage 4	X	AC	24.0	0.3	24.0	99.3	0.1	0.1	0.1	0.2
SI21007	310242	8339227	44.3	Stage 4	X	AC	21.0	0.3	18.0	99.3	0.1	0.2	0.1	0.2
SI21008	310406	8339095	55.5	Stage 4	X	AC	33.0	0.3	33.0	99.0	0.3	0.3	0.1	0.2
SI21009	310538	8338950	44.3	Stage 4	X	AC	24.0	0.3	24.0	99.3	0.2	0.2	0.1	0.2
SI21010	310689	8338791	47.5	Stage 4	X	AC	30.0	0.3	28.0	99.3	0.1	0.2	0.1	0.2
SI21011	310818	8338651	40.1	Stage 4	X	AC	24.0	0.3	23.0	99.2	0.1	0.2	0.1	0.3
SI21012	310965	8338527	35.5	Stage 4	X	AC	15.0	0.3	15.0	99.3	0.1	0.1	0.2	0.2
SI21013	310392	8338672	65.7	Stage 4	X	AC	40.0	0.3	36.0	99.5	0.1	0.1	0.1	0.1
SI21014	310237	8338824	56.0	Stage 4	X	AC	33.0	0.3	33.0	99.3	0.1	0.1	0.2	0.2
SI21015	310086	8338932	58.2	Stage 4	X	AC	34.0	0.3	32.0	99.4	0.1	0.2	0.1	0.1
SI21016	309938	8339094	52.6	Stage 4	X	AC	30.0	0.3	29.0	99.1	0.1	0.2	0.2	0.2
SI21017	309812	8339241	56.4	Stage 4	X	AC	33.0	0.3	33.0	99.3	0.1	0.1	0.1	0.2
SI21018	309656	8339365	59.1	Stage 4	X	AC	42.0	0.3	40.0	99.4	0.1	0.1	0.1	0.2
SI21019	309539	8339513	57.9	Stage 4	X	AC	36.0	0.3	34.0	99.3	0.1	0.1	0.1	0.2
SI21020	309371	8339654	60.0	Stage 4	X	AC	36.0	0.3	36.0	99.4	0.1	0.2	0.1	0.2
SI21021	309251	8339761	69.2	Stage 4	X	AC	45.0	0.3	45.0	99.4	0.1	0.2	0.1	0.1
SI21022	309266	8339691	66.9	Stage 4	X	AC	42.0	0.3	39.0	99.5	0.1	0.1	0.1	0.1
SI21023	309215	8339592	63.4	Stage 4	X	AC	33.0	0.3	28.0	99.0	0.2	0.3	0.2	0.2
SI21024	309106	8339646	62.5	Stage 4	X	AC	27.0	0.3	24.0	99.2	0.2	0.2	0.1	0.1
SI21025	309034	8339670	59.0	Stage 4	X	AC	21.0	0.3	20.0	99.1	0.2	0.2	0.1	0.2
SI21026	308909	8339818	52.4	Stage 4	X	AC	15.0	0.3	13.0	99.2	0.1	0.2	0.1	0.2
SI21027	308897	8339671	64.5	Stage 4	X	AC	24.0	0.3	23.0	99.2	0.2	0.2	0.1	0.2
SI21028	308992	8339552	55.3	Stage 4	X	AC	30.0	0.3	15.0	99.3	0.1	0.1	0.1	0.2
SI21029	309084	8339495	60.2	Stage 4	X	AC	21.0	0.3	17.0	99.2	0.1	0.1	0.1	0.2
SI21030	309208	8339362	59.1	Stage 4	X	AC	21.0	0.3	16.0	99.2	0.1	0.1	0.1	0.2
SI21031	309323	8339223	49.0	Stage 4	X	AC	9.0	0.3	6.0	99.4	0.1	0.1	0.1	0.3
SI21032	309504	8339093	55.3	Stage 4	X	AC	24.0	0.3	18.0	99.4	0.1	0.1	0.1	0.2
SI21033	309677	8338971	59.8	Stage 4	X	AC	32.0	0.3	27.0	99.5	0.1	0.1	0.1	0.1
SI21034	309784	8338810	60.8	Stage 4	X	AC	30.0	0.3	30.0	99.3	0.1	0.1	0.1	0.2
SI21035	309851	8338895	70.4	Stage 4	X	AC	45.0	0.3	42.0	99.2	0.1	0.1	0.1	0.1

Hole ID	Easting (m)	Northing (m)	Collar RL (m)	Stage	New Release	Drill Type	Hole Depth (m)	From (Top of Resource)	To (Bottom of Resource)	SiO_2	Fe_2O_3	TiO_2	Al_2O_3	LOI
SI21036	309558	8339154	56.0	Stage 4	X	AC	27.0	0.3	25.0	99.0	0.1	0.2	0.1	0.1
SI21037	309494	8339222	55.7	Stage 4	X	AC	36.0	0.3	25.0	98.7	0.2	0.3	0.1	0.1
SI21038	309438	8339305	56.5	Stage 4	X	AC	27.0	0.3	23.0	99.0	0.2	0.3	0.1	0.2
SI21039	309386	8339386	60.2	Stage 4	X	AC	27.0	0.3	24.0	99.2	0.1	0.1	0.1	0.2
SI21040	309303	8339452	63.1	Stage 4	X	AC	30.0	0.3	27.0	99.4	0.1	0.2	0.1	0.1
SI21041	309259	8339512	64.4	Stage 4	X	AC	30.0	0.3	28.0	98.9	0.2	0.3	0.2	0.2
SI21042	309892	8338758	62.9	Stage 4	X	AC	33.0	0.3	29.0	99.1	0.2	0.2	0.1	0.2
SI21043	309838	8338851	67.5	Stage 4	X	AC	39.0	0.3	36.0	99.3	0.1	0.2	0.1	0.1
SI21044	309913	8338662	59.0	Stage 4	X	AC	24.0	0.3	21.0	99.3	0.2	0.3	0.1	0.1
SI21045	310048	8338491	55.3	Stage 4	X	AC	21.0	0.3	20.0	99.3	0.1	0.1	0.1	0.2
SI21046	310172	8338337	52.6	Stage 4	X	AC	24.0	0.3	21.0	99.5	0.1	0.1	0.1	0.1
SI21047	310322	8338219	48.7	Stage 4	X	AC	15.0	0.3	13.0	99.5	0.1	0.1	0.1	0.2
SI21048	310393	8338153	49.0	Stage 4	X	AC	15.0	0.3	14.0	99.4	0.1	0.1	0.1	0.2
SI21049	310439	8338099	47.8	Stage 4	X	AC	15.0	0.3	11.0	99.3	0.1	0.1	0.1	0.2
SI21050	309940	8338868	62.3	Stage 4	X	AC	39.0	0.3	34.0	99.0	0.1	0.2	0.2	0.2
SI21051	310178	8338677	53.8	Stage 4	X	AC	24.0	0.3	22.0	99.3	0.1	0.1	0.1	0.1
SI21052	310327	8338533	40.4	Stage 4	X	AC	12.0	0.3	7.0	99.0	0.1	0.1	0.1	0.2
SI21053	310455	8338390	38.1	Stage 4	X	AC	18.0	0.3	16.0	98.9	0.1	0.2	0.3	0.3
SI21054	310526	8338319	33.5	Stage 4	X	AC	12.0	0.3	12.0	99.2	0.0	0.1	0.1	0.2
SI21055	310556	8338577	43.4	Stage 4	X	AC	21.0	0.3	20.0	99.3	0.0	0.1	0.1	0.2
SI21056	310650	8338516	38.4	Stage 4	X	AC	16.0	0.3	15.0	99.1	0.1	0.2	0.2	0.2
SI21057	310723	8338453	36.0	Stage 4	X	AC	15.0	0.3	11.0	99.5	0.1	0.1	0.1	0.3
SI21058	310764	8338406	34.5	Stage 4	X	AC	15.0	0.3	12.0	99.1	0.1	0.1	0.2	0.3
SI21059	311239	8338240	40.0	Stage 4	X	AC	21.0	0.3	21.0	98.8	0.2	0.2	0.2	0.2
SI21060	310272	8338109	36.5	Stage 4	X	AC	12.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI21061	310205	8338036	38.1	Stage 4	X	AC	18.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI21062	310255	8337834	37.5	Stage 4	X	AC	15.0	0.3	5.0	99.0	0.1	0.1	0.2	0.4
SI21063	310516	8337565	46.9	Stage 4	X	AC	16.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI21064	309981	8338092	37.4	Stage 4	X	AC	15.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI21065	309721	8338406	39.5	Stage 4	X	AC	14.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI21066	309417	8338654	38.3	Stage 4	X	AC	18.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI21067	309140	8338955	33.0	Stage 4	X	AC	12.0	0.3	7.0	99.7	0.1	0.1	0.1	0.2
SI21068	308966	8339158	31.6	Stage 4	X	AC	9.0	0.3	3.0	98.8	0.1	0.2	0.2	0.4
SI21069	309117	8339209	34.6	Stage 4	X	AC	14.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI21070	309240	8339087	33.8	Stage 4	X	AC	12.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI21071	309406	8338926	34.8	Stage 4	X	AC	12.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI21072	309014	8339428	43.9	Stage 4	X	AC	9.0	0.3	8.0	99.3	0.0	0.1	0.1	0.2
SI21073	308981	8339307	37.2	Stage 4	X	AC	9.0	0.3	8.0	99.3	0.1	0.1	0.1	0.2
SI21074	308835	8339415	34.6	Stage 4	X	AC	12.0	0.3	6.0	99.2	0.0	0.1	0.2	0.3
SI21075	308716	8339516	31.8	Stage 4	X	AC	12.0	0.3	10.0	99.2	0.0	0.1	0.1	0.3
SI21076	308535	8339450	32.4	Stage 4	X	AC	12.0	0.3	8.0	99.1	0.1	0.1	0.2	0.3
SI21077	308787	8339196	42.0	Stage 4	X	AC	23.0	0.3	15.0	99.3	0.1	0.1	0.1	0.2
SI21078	308633	8339080	46.0	Stage 4	X	AC	19.0	0.3	10.0	99.4	0.1	0.1	0.1	0.2
SI21079	308374	8339390	43.6	Stage 4	X	AC	9.0	0.3	5.0	99.3	0.1	0.1	0.1	0.2

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Hole ID	Easting (m)	Northing (m)	Collar RL (m)	Stage	New Release	Drill Type	Hole Depth (m)	From (Top of Resource)	To (Bottom of Resource)	SiO_2	Fe_2O_3	TiO_2	Al_2O_3	LOI
SI21080	308006	8339655	59.3	Stage 4	X	AC	30.0	0.3	27.0	99.2	0.1	0.1	0.1	0.1
SI21081	307861	8339578	48.0	Stage 4	X	AC	18.0	0.3	18.0	99.1	0.1	0.2	0.1	0.2
SI21082	307863	8339447	51.5	Stage 4	X	AC	21.0	0.3	21.0	99.2	0.1	0.2	0.1	0.1
SI21083	307993	8339206	43.5	Stage 4	X	AC	15.0	0.3	15.0	99.3	0.1	0.1	0.1	0.1
SI21084	308182	8338863	57.2	Stage 4	X	AC	24.0	0.3	24.0	98.8	0.2	0.3	0.1	0.2
SI21085	308204	8338621	57.1	Stage 4	X	AC	27.0	0.3	27.0	99.3	0.1	0.1	0.1	0.1
SI21086	308385	8338362	52.4	Stage 4	X	AC	21.0	0.3	21.0	99.4	0.1	0.1	0.1	0.2
SI21087	308619	8338160	62.4	Stage 4	X	AC	27.0	0.3	23.0	99.2	0.1	0.1	0.1	0.2
SI21088	308777	8337862	62.7	Stage 4	X	AC	30.0	0.3	27.0	99.3	0.1	0.1	0.1	0.1
SI2HA0002	306183	8342276	31.8	Stage 3		HA	3.0	0.3	3.0	98.7	0.1	0.1	0.1	0.6
SI2HA0003	307372	8341048	55.6	Stage 3		HA	5.0	0.3	5.0	98.7	0.2	0.3	0.1	0.7
SI2HA0004	307609	8340668	40.9	Stage 3		HA	5.0	0.3	5.0	99.2	0.1	0.1	0.1	0.3
SI2HA0005	308415	8340076	42.7	Stage 3		HA	5.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI2HA0006	307874	8340489	35.3	Stage 3		HA	3.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI2HA0007	308150	8340256	37.3	Stage 3		HA	3.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI2HA0008	307854	8341095	42.3	Stage 3		HA	5.0	0.3	4.0	98.8	0.1	0.2	0.2	0.6
SI2HA0009	308052	8340942	33.1	Stage 3		HA	5.0	0.3	4.0	98.9	0.0	0.1	0.1	0.7
SI2HA0010	308233	8340739	41.4	Stage 3		HA	4.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI2HA0011	308388	8340610	37.5	Stage 3		HA	4.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI2HA0012	306914	8340632	37.2	Stage 3		HA	5.0	0.3	5.0	99.2	0.1	0.2	0.1	0.2
SI2HA0013	308842	8339375	32.5	Stage 3		HA	5.0	0.3	5.0	99.2	0.0	0.1	0.1	0.2
SI2HA0014	309116	8339858	34.2	Stage 4		HA	5.0	0.3	3.0	98.7	0.1	0.1	0.1	0.4
SI2HA0015	309409	8339388	57.5	Stage 4		HA	5.0	0.3	5.0	98.1	0.2	0.4	0.1	0.2
SI2HA0016	309660	8339183	38.0	Stage 4		HA	5.0	0.3	5.0	98.7	0.1	0.1	0.1	0.3
SI2HA0017	309877	8338934	64.2	Stage 4		HA	5.0	0.3	5.0	98.2	0.2	0.4	0.1	0.1
SI2HA0018	310165	8339088	28.9	Stage 4		HA	3.0	0.3	3.0	98.9	0.1	0.1	0.1	0.1
SI2HA0019	310448	8338815	30.0	Stage 4		HA	4.0	0.3	4.0	98.8	0.1	0.1	0.1	0.2
SI2HA0020	310443	8339232	29.1	Stage 4		HA	2.0	0.3	2.0	99.0	0.1	0.2	0.1	0.2
SI2HA0021	310534	8339124	30.0	Stage 4		HA	3.0	0.3	3.0	98.9	0.1	0.3	0.1	0.2
SI2HA0022	310600	8339032	28.2	Stage 4		HA	2.0	0.3	2.0	98.7	0.1	0.1	0.1	0.6
SI2HA0023	310180	8339368	29.1	Stage 4		HA	2.0	0.3	2.0	98.7	0.1	0.2	0.1	0.4
SI2HA0024	310039	8339445	29.2	Stage 4		HA	2.0	0.3	2.0	98.8	0.1	0.3	0.1	0.4
SI2HA0025	308363	8341172	33.6	Stage 4		HA	4.0	0.3	1.0	98.7	0.1	0.2	0.1	0.4
SI2HA0026	308456	8341097	33.6	Stage 4		HA	3.0	0.3	3.0	99.0	0.1	0.1	0.1	0.2
SI2HA0027	308569	8341032	34.3	Stage 4		HA	3.0	0.3	3.0	98.9	0.1	0.2	0.1	0.2
SI2HA0028	308518	8340974	32.1	Stage 4		HA	2.0	0.3	2.0	98.9	0.1	0.2	0.1	0.5
SI2HA0029	308240	8341345	33.9	Stage 4		HA	3.0	0.3	3.0	98.9	0.1	0.2	0.1	0.4
SI2HA0030	308289	8341255	33.3	Stage 4		HA	3.0	0.3	3.0	98.6	0.1	0.1	0.1	0.5
SI2HA0031	308613	8340835	30.5	Stage 4		HA	1.0	0.3	1.0	99.2	0.1	0.2	0.1	0.3
SI2HA0032	308702	8340748	30.9	Stage 4		HA	2.0	0.3	2.0	98.7	0.0	0.1	0.1	0.7
SI2HA0033	308770	8340689	31.0	Stage 4		HA	2.0	0.3	2.0	99.1	0.0	0.1	0.1	0.4
SI2HA0034	308727	8340556	48.8	Stage 4		HA	4.0	0.3	4.0	99.0	0.1	0.2	0.1	0.3
SI2HA0035	308862	8340585	30.8	Stage 4		HA	2.0	0.3	2.0	99.2	0.1	0.2	0.1	0.3
SI2HA0036	308933	8340476	30.3	Stage 4		HA	2.0	0.3	2.0	99.0	0.1	0.2	0.1	0.3

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Unit 8, 55–61 Holdsworth St
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Hole ID	Easting (m)	Northing (m)	Collar RL (m)	Stage	New Release	Drill Type	Hole Depth (m)	From (Top of Resource)	To (Bottom of Resource)	SiO_2	Fe_2O_3	TiO_2	Al_2O_3	LOI
SI2HA0037	309025	8340361	30.7	Stage 4		HA	2.0	0.3	2.0	98.8	0.1	0.2	0.1	0.6
SI2HA0038	309118	8340269	29.8	Stage 4		HA	1.0	0.3	1.0	98.8	0.1	0.2	0.1	0.4
SI2HA0039	309210	8340168	30.1	Stage 4		HA	2.0	0.3	2.0	99.0	0.1	0.1	0.1	0.4
SI2HA0040	309310	8340054	30.4	Stage 4		HA	2.0	0.3	2.0	98.9	0.0	0.1	0.1	0.5
SI2HA0041	309410	8339991	29.8	Stage 4		HA	2.0	0.3	2.0	98.1	0.0	0.1	0.1	1.4
SI2HA0042	309574	8339907	30.6	Stage 4		HA	3.0	0.3	3.0	99.2	0.1	0.2	0.1	0.3
SI2HA0043	309677	8339818	29.9	Stage 4		HA	2.0	0.3	2.0	98.9	0.0	0.1	0.1	0.3
SI2HA0044	309791	8339698	30.0	Stage 4		HA	2.0	0.3	2.0	99.3	0.1	0.2	0.1	0.2
SI2HA0045	309916	8339576	30.0	Stage 4		HA	2.0	0.3	2.0	99.5	0.1	0.2	0.1	0.1
SI2HA0046	310316	8339300	29.7	Stage 4		HA	3.0	0.3	3.0	99.0	0.1	0.3	0.1	0.3
SI2HA0047	311372	8338234	23.5	Stage 4		HA	2.0	0.3	1.0	98.7	0.0	0.1	0.1	0.9
SI2HA0048	311280	8338318	24.1	Stage 4		HA	3.0	0.3	2.0	98.9	0.0	0.1	0.1	0.5
SI2HA0049	311189	8338390	25.2	Stage 4		HA	3.0	0.3	3.0	98.6	0.1	0.3	0.1	0.4
SI2HA0050	311115	8338463	23.8	Stage 4		HA	2.0	0.3	2.0	97.4	0.1	0.2	0.1	1.7
SI2HA0051	311032	8338549	25.2	Stage 4		HA	3.0	0.3	N/A	N/A	N/A	N/A	N/A	N/A
SI2HA0052	310919	8338679	26.0	Stage 4		HA	3.0	0.3	3.0	99.0	0.2	0.4	0.1	0.2
SI2HA0053	310811	8338816	26.7	Stage 4		HA	2.0	0.3	2.0	98.8	0.1	0.1	0.1	0.3
SI2HA0054	310719	8338903	27.6	Stage 4		HA	3.0	0.3	3.0	99.0	0.1	0.3	0.1	0.2
SI2HA0055	310538	8338585	45.6	Stage 4		HA	5.0	0.3	5.0	98.9	0.1	0.2	0.1	0.3
SI2HA0056	309625	8339574	42.2	Stage 4		HA	5.0	0.3	5.0	99.3	0.1	0.1	0.1	0.2
SI2HA0057	309721	8339481	43.0	Stage 4		HA	5.0	0.3	5.0	99.0	0.1	0.2	0.1	0.2
SI2HA0058	309794	8339402	41.1	Stage 4		HA	5.0	0.3	5.0	99.3	0.1	0.1	0.1	0.1
SI2HA0059	309875	8339335	38.7	Stage 4		HA	5.0	0.3	5.0	99.3	0.1	0.1	0.1	0.1
SI2HA0060	309955	8339257	35.4	Stage 4		HA	5.0	0.3	5.0	99.3	0.1	0.1	0.1	0.2
SI2HA0061	310060	8339171	30.5	Stage 4		HA	4.0	0.3	4.0	99.3	0.1	0.1	0.1	0.2

*Holes marked x in the column “New Release” are material holes being reported for the first time.
*Holes marked "N/A" signify the interdunal holes that were utilised for constraining MRE