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SUCCESSFUL PHASE 1 HYDROGEOLOGICAL TESTS AND PUMP INJECTION WELL STRIKES CONSIDERABLE DOWN DIP EXTENSION TO COPPER MINERALISATION

NGAMI COPPER PROJECT, BOTSWANA

Cobre Limited (ASX: **CBE**, **Cobre** or **Company**) is pleased to announce successful completion of the first phase of hydrogeological test work on the Ngami Copper Project (**NCP**) in the Kalahari Copper Belt (**KCB**), Botswana. The programme has been designed to provide essential information to demonstrate the viability of an In-Situ Copper Recovery (**ISCR**) process for extraction of copper-silver from the significant strike of mineralisation (estimated scale of between 103 and 166Mt @ 0.38 to 0.46% Cu¹):

1. Initial short-term hydraulic tests conducted on recently completed production and monitoring wells have **verified the presence of an enhanced permeability zone within a representative portion of the copper mineralised compartment**. This zone is bounded by low permeability footwall and hanging wall competent "seal" rocks.
2. In addition, production well PW001, drilled down the main mineralised fracture zone, has intersected (open-ended) **78m @ 0.59% Cu from 187 to 265m** demonstrating the continuity and depth extent of copper mineralisation at the target.
3. A second phase of long-term pumping and injection tests designed to evaluate aquifer characteristics over a greater distance for longer period will now commence.

The results represent a considerable milestone for the company, providing demonstrable support for the potential to inject a leaching fluid into the orebody.

¹ At this stage the results are in an exploration target category. The estimates of tonnage and grade are conceptual in nature, there has been insufficient exploration to estimate a Mineral Resource and it is uncertain if further exploration will result in the estimation of a Mineral Resource.

Commenting on the hydrogeological programme, Adam Wooldridge, Cobre's Chief Executive Officer, said:

"Having our desktop work successfully validated with in-field tests marks a pivotal advancement in our journey to developing the ISCR project potential. Given the scale of the target, proving up a low cost, environmentally friendly extraction method for copper-silver beneficiation will be a game changer for the company, local communities, and greater Kalahari Copper Belt."

The ongoing hydrogeological programme at the NCP (**Figure 1 and 2**) includes 3 monitoring wells strategically located along strike of mineralisation and offset laterally in the footwall and hanging wall which are markedly less permeable. In addition to the monitoring wells, a large diameter injection/production well (PW001) intersecting a representative portion of the mineralised contact has been completed. The production well intersected sub-vertically dipping mineralisation associated with the target fracture zone which is expected to provide a natural aquifer allowing for injection of a leaching fluid directly into the associated copper mineralisation.

Initial hydraulic (slug) testing was conducted on the production well (PW001) and monitoring wells to provide estimates of the 'near well' aquifer permeabilities. A 10,000 litre slug of potable water was rapidly injected into PW001, revealing enhanced permeability associated with the main mineralisation compartment. Enhanced permeability in this context is preferred for facilitating fluid transfer between production wells, particularly for ISCR operations. Conversely, slug tests performed on monitoring wells constructed outside of the mineralisation compartment, targeting the hanging wall (HW) and footwall (FW) seals, demonstrated lower permeabilities.

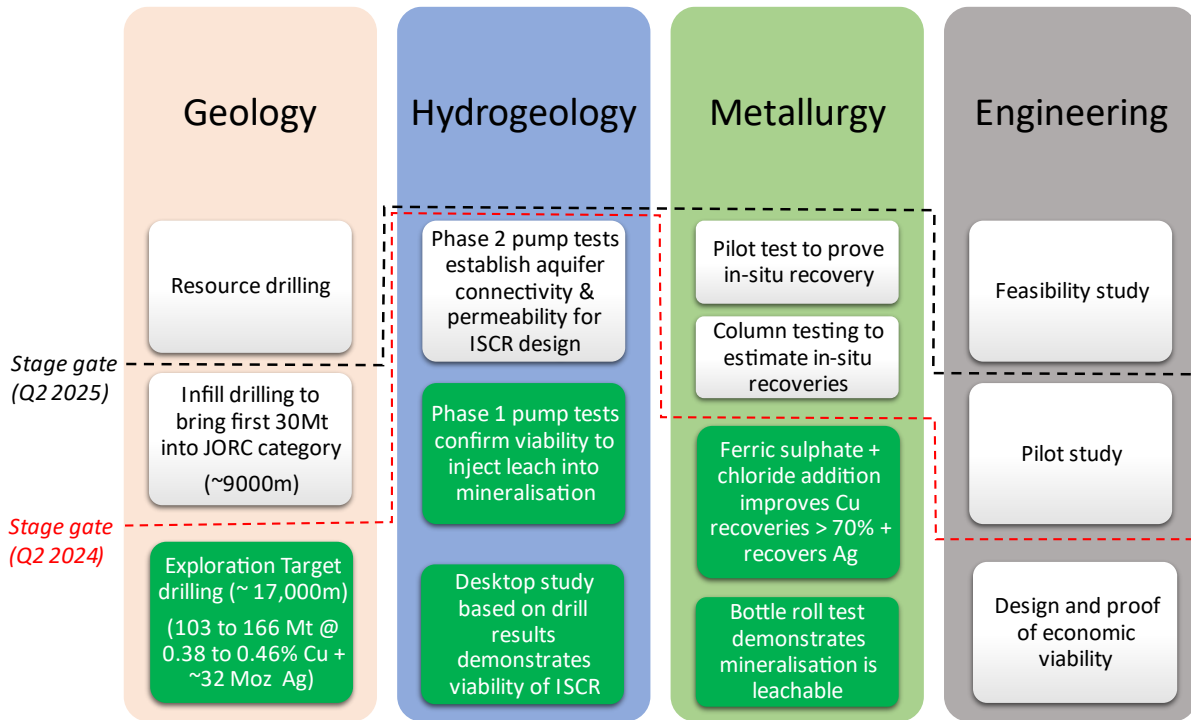
The depth to water table was confirmed at 123 m below ground surface and is sufficiently below the Kalahari Group cover. The deep groundwater level is considered beneficial for ISCR operations as this reduces the risk of water returning to surface during the injection phase.

A second phase of hydrogeological test work will include longer term pumping and injection testing to verify these results over a larger distance. Work on this phase has now commenced and will be reported in the upcoming months.

In addition to providing important hydrogeological information, the production well has intersected an extensive zone of copper mineralisation effectively demonstrating the down-dip grade continuity at depth which adds further support to ISCR model.

A roadmap for progressing the ISCR process to a development project is graphically illustrated overleaf.

Graphical illustration of the ISCR journey to development with key stage gates highlighted. Green boxes highlight milestones completed. With over 500,000 tons of contained copper in this target, proof of the method presents a game changer for the district.



Geology and Mineralisation

Mineralisation at NCP is sedimentary-hosted, structurally controlled, copper-silver associated with the redox contact between oxidised Ngwako Pan Formation red beds and overlying reduced marine sedimentary rocks of the D'Kar Formation on the limbs of anticlinal structures. Drilling has focussed on the southern anticlinal structure which extends for over 40km across the NCP with evidence for anomalous copper-silver mineralisation on both northern and southern limbs.

Drilling results to date have returned consistent, wide intersections of anomalous to moderate-grade copper-silver values over extensive strike lengths with smaller structurally controlled higher-grade zones (**Figure 1**). This style of mineralisation is dominated by fine-grained chalcocite which occurs along cleavage planes (S_1) and in fractures rather than the vein hosted bornite with chalcopyrite more typical of the KCB style. Importantly, the chalcocite mineralisation is amenable to acid leaching, occurs below the water table and is associated with well-developed fracture zones bounded by more competent hanging and footwall units satisfying key considerations for ISCR.

Pumping test design and objectives

The next test phase entails conducting a series of pumping and injection tests utilising production well PW001. This procedure is depicted on **Figure 3**. The pumping test aims to evaluate aquifer characteristics, including permeability and storage properties, while the injection test seeks to

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determine the aquifer's water-receiving capacity. Throughout these tests, the monitoring of groundwater levels in surrounding monitoring wells will offer insights into fluid movement within the mineralised compartment, as well as lateral movement through the footwall and hanging wall competent "seal" rocks.

The results obtained will provide valuable insights into aquifer permeability, anisotropy, extent, and preferential groundwater flow directions. This comprehensive understanding of the hydrogeological system will help assess the viability of an in-situ recovery program.

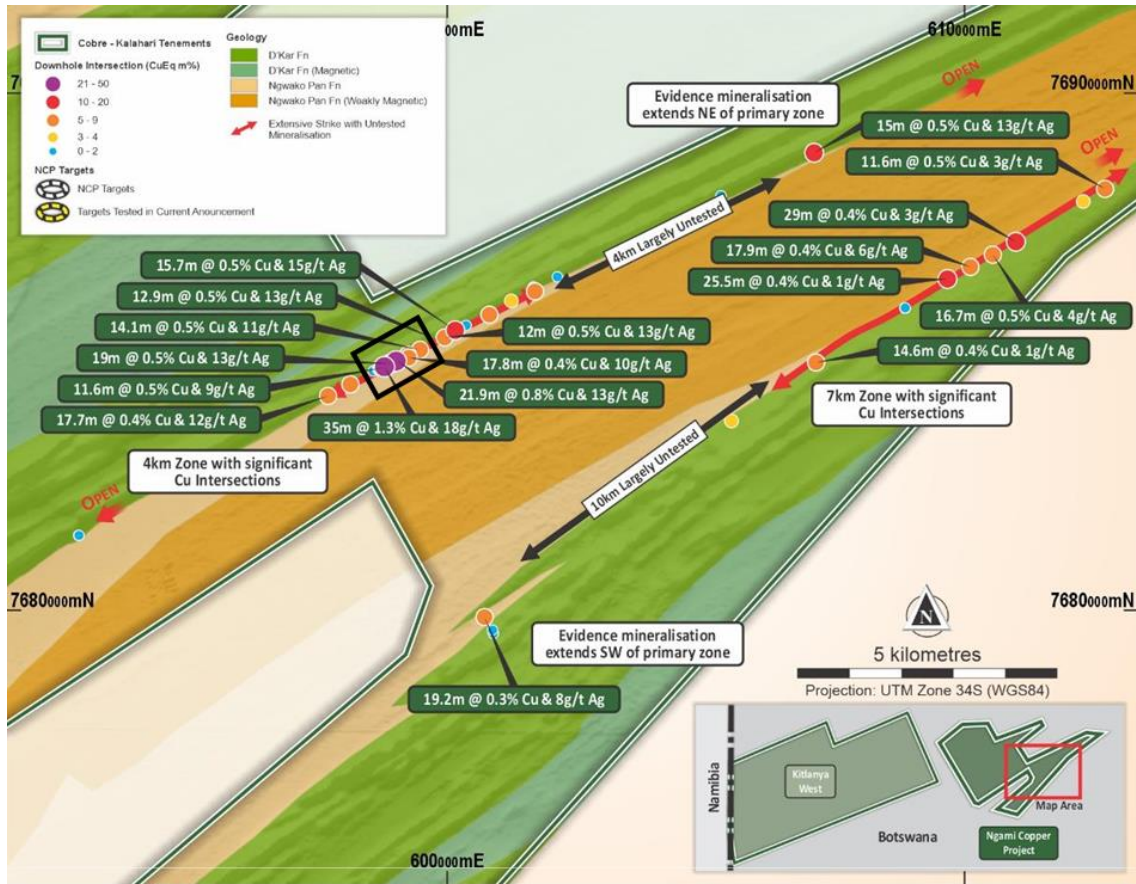
WSP Australia Ltd have been engaged to provide oversight and modelling of the pumping-injection test results.




Hydrogeological drilling, NCP Botswana

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 Hydrogeological study area

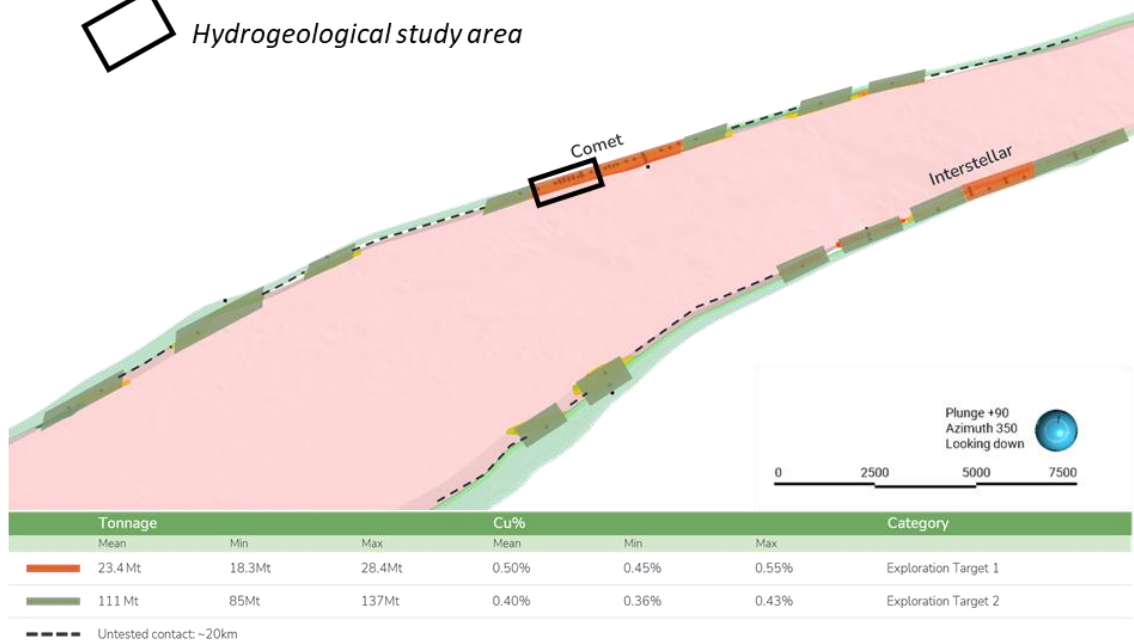


Figure 1. Locality map (plan above and oblique 3D view below) illustrating the position of the test study on the Southern Anticline of the NCP. The test study area is illustrated in detail in Figure 2.

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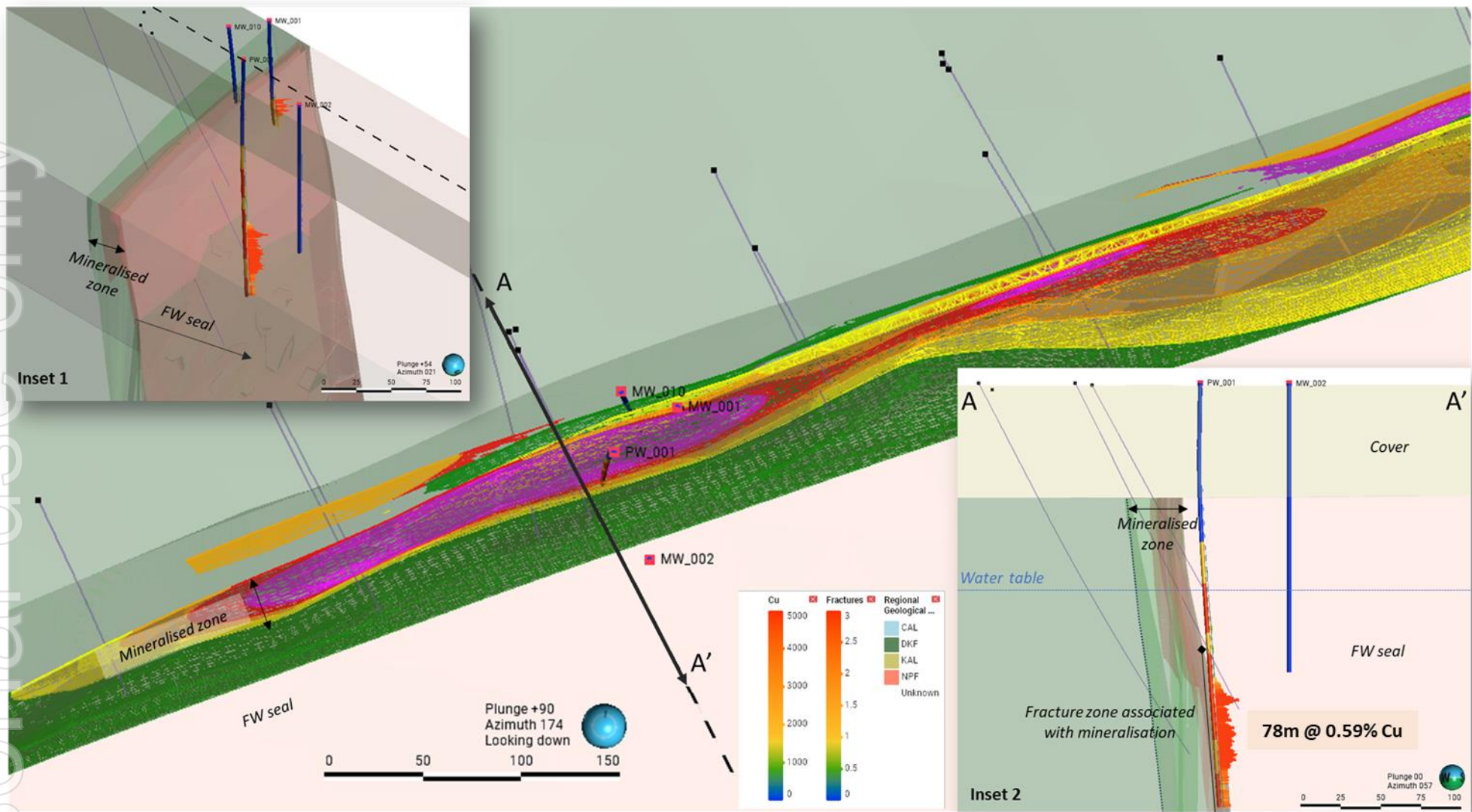


Figure 2. Plan view (looking down) of the geological and mineralisation model illustrating monitoring and injection wells. An oblique view (inset 1) and section (inset 2) highlight the key components of the hydrogeological model. In both insets the hole traces are coloured by fracture intensity (0 = no fractures, 3 = high fracturing) with copper recoveries graphically illustrated in ppm.

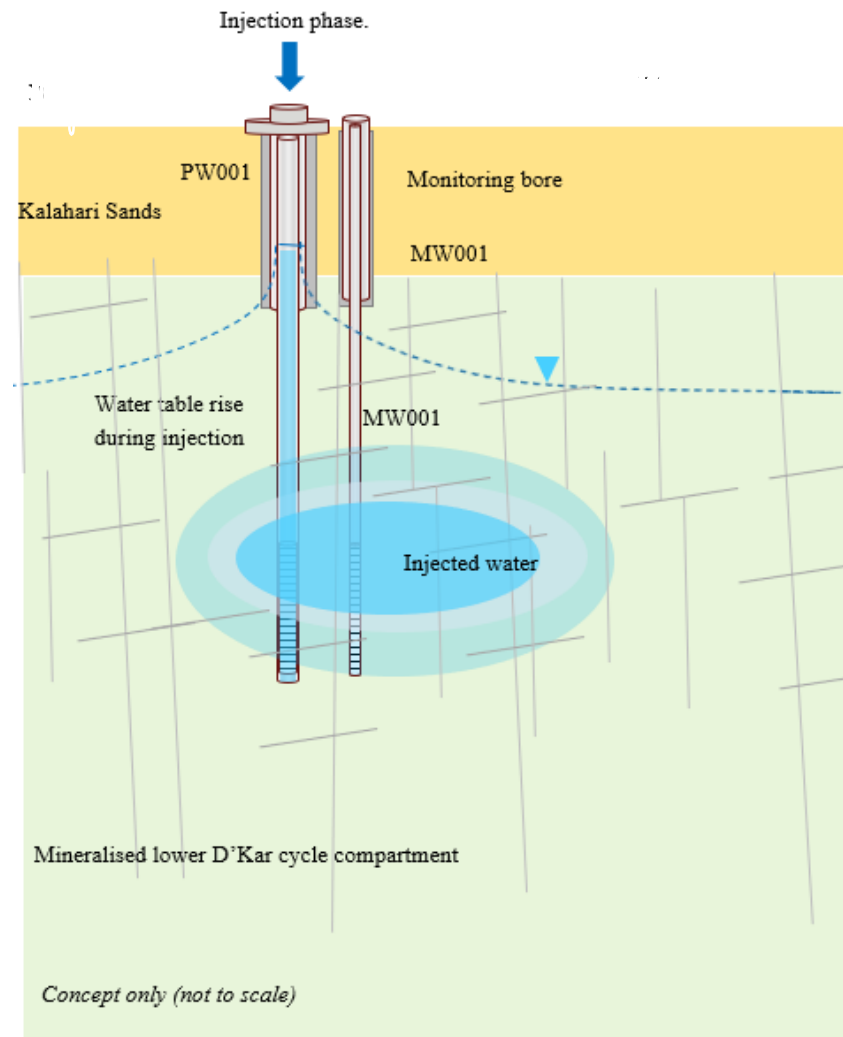
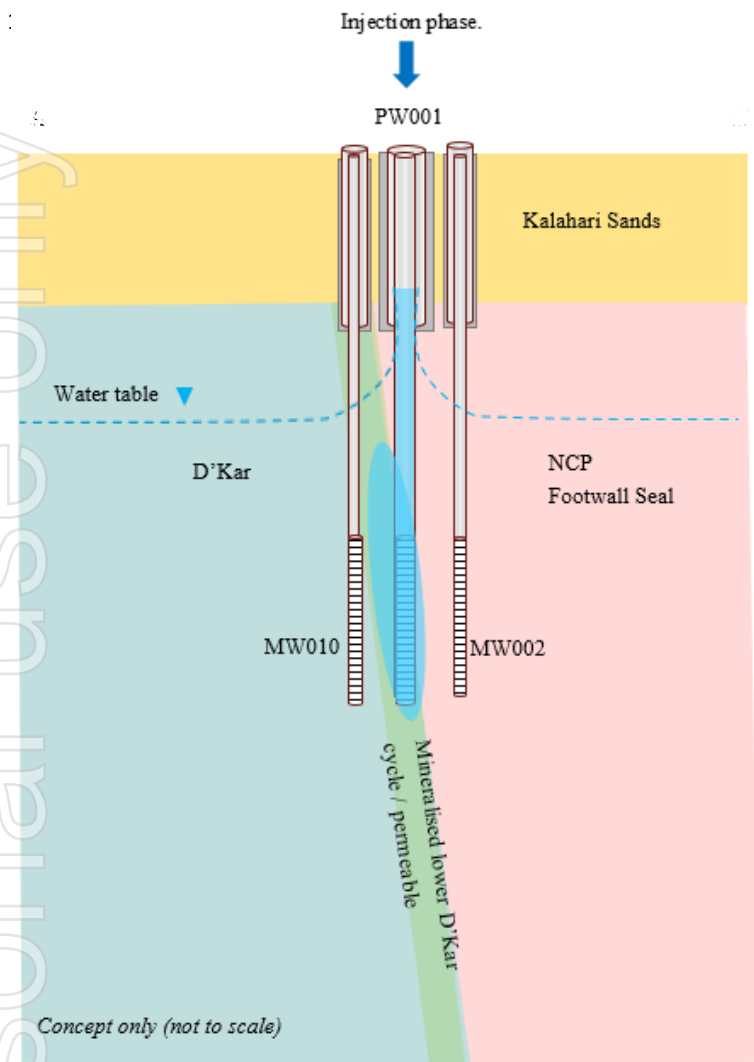


Figure 3. Conceptual illustration of injection test and monitoring well set up, showing cross section (left) and long section (right)

ISCR background and viability

ISCR utilises a series of injection wells to pump a weak acid (similar pH to lemon juice) solution under low pressure to dissolve the copper (and silver) mineralisation in situ. The method relies on naturally developed fractures to focus the solution into the orebody where the copper is leached after which the copper-rich solution is pumped to surface through recovery wells for processing into copper cathode sheets using an electro-chemical process that separates the copper from the solution. As there is no need for excavation, mine development, waste piles, milling or smelting, the technique provides a cost-effective technology with an extremely small environmental footprint.

For a deposit at NCP to be considered viable for ISCR, several specific hydrogeological and metallurgical factors need to be satisfied:

1. *Is the mineralisation amenable to acid leaching?*
 - Mineralisation is predominantly fine-grained chalcocite easily treated with an acid leach process.
 - Mineralisation is hosted in fractures and along cleavages, providing porosity and permeability and providing fluid flow through the mineralised horizon for the leaching solution.
 - IBR Leach tests carried out on approximate 5m composite samples of moderate- and high-grade intersections have confirmed an acid leach with ferric sulphate and chloride is viable for copper and silver extraction.
2. *Is the mineralisation below the water table?*
 - Groundwater measurements estimate the water table to be at 123m depth below surface.
 - This appears to be an optimal depth, sufficiently below the Kalahari cover to ensure fracture control preventing lateral migration, with a small portion of the orebody exposed above the water table.
3. *Does the host rock have fractured permeability for solution to permeate through and dissolve the copper?*
 - Detailed fracture logging and AI driven fracture logging carried out on holes through the Comet Target has confirmed:
 - High density fracture zone associated with the lower mineralised cycle of the D'Kar Formation, particularly associated with the mineralisation above the contact.
 - Lower (less-permeable) fracture counts associated with the underlying Ngwako Pan Formation footwall and overlying sandstone packages in the D'Kar Formation provide lateral seals.

- The primary fracture orientation is sub-parallel to the (mineralised) D'Kar/Ngwako Pan Formations redox contact, allowing fluid flow parallel to and along the contact zone.
- These results have been substantiated with results from the recently completed production and monitoring wells.

The current study addresses (2) and (3) above.

Target Model

The NCP area is located near the northern margin of the KCB and includes significant strike of sub-cropping Ngwako Pan / D'Kar Formation contact on which the majority of the known deposits in the KCB occur.

Cobre is aiming to prove up a similar ISCR process to Taseko Mines Ltd's (TSX:TKO, NYSE:TGB) Florence Copper Deposit (320Mt @ 0.36% Cu) in Arizona which shares a similar scale to NCP².

For full exploration results including relevant JORC table information, background on the project scale and ISCR opportunity, see Cobre's ASX announcements as follows:

- NCP Exploration Target Estimate Highlights Significant Scale, 30 August 2023
- Potential for Extensive In-Situ Copper Mining – Botswana, 8 August 2023
- Metallurgical Test Work at NCP Highlights Recovery Potential, 9 October 2023.

This ASX release was authorised on behalf of the Cobre Board by: Adam Wooldridge, Chief Executive Officer.

For more information about this announcement, please contact:

Adam Wooldridge

Chief Executive Officer

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² [Florence Copper | Taseko Mines Limited](#)

COMPETENT PERSONS STATEMENT

The information in this announcement that relates to exploration results is based on information compiled by Mr David Catterall, a Competent Person and a member of a Recognised Professional Organisations (ROPO). David Catterall has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC 2012). David is the principal geologist at Tulia Blueclay Limited and a consultant to Kalahari Metals Limited. David Catterall is a member of the South African Council for Natural Scientific Professions, a recognised professional organisation.

David Catterall consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

APPENDIX 1

JORC Table 1 - Section 1 Sampling Techniques and Data for the NCP

(Criteria in this section apply to all succeeding sections)

JORC Code, 2012 Edition – Table 1 report template

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<i>Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</i>	<ul style="list-style-type: none"> • <i>The information in this release relates to the technical details from the Company's exploration and drilling program at the Ngami Copper Project (NCP) located within the Ngamiland District on the Kalahari Copper Belt, Republic of Botswana.</i> • <i>Representative diamond half core samples are taken from zones of interest. Samples were taken consistently from the same side of the core cutting line. Core cutting line is positioned to result in two splits as mirror images with regards to the mineralisation, and to preserve the orientation line.</i> • <i>Down-the-hole (DTH) percussion drilling was used to obtain 1m samples.</i> • <i>A Reference sample (unsieved) was taken from each meter drilled.</i> • <i>A representative sample, sieved to -180µm fraction, was prepared for each meter drilled into bedrock as well as selected Kalahari intervals. These samples were analysed using pXRF at the field laboratory in camp</i>
	<i>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used</i>	<ul style="list-style-type: none"> • <i>Diamond core sample representativity was ensured by bisecting structures of interest, and by the sample preparation technique in the laboratory.</i> • <i>The diamond drill core samples were selected based on geological logging and pXRF results,</i>

	<p><i>Aspects of the determination of mineralisation that are Material to the Public Report.</i></p>	<p><i>with the ideal sampling interval being 1m, whilst ensuring that sample interval does not cross any logged significant feature of interest.</i></p> <ul style="list-style-type: none"> • <i>Individual core samples were crushed entirely to 90% less than 2mm, riffle split off 1kg, pulverise split to better than 85% passing 75 microns (ALS PREP-31D).</i> • <i>Sample representivity and calibration for ICP AES analysis is ensured by the insertion of suitable QAQC samples.</i> • <i>Samples are digested using 4-acid near total digest and analysed for 34 elements by ICP-AES (ALS ME-ICP61, and ME-ICP61a).</i> • <i>Over range for Cu and Ag are digested and analysed with the same method but higher detection limits (ALS ME-OG62).</i> • <i>The DTH drill methodology somewhat homogenizes the sample over each meter. In order to ensure sample representivity, the sample was thoroughly mixed prior to sub-sampling and screening to -180 micron.</i> • <i>Duplicates and Replicate samples were taken every 20 samples to assess further the sample representivity.</i> • <i>pXRF instruments are calibrated using calibration disks at the start of each batch run.</i> • <i>pXRF measurements are carried out with appropriate blanks and reference material (as well as duplicates and replicates where available) analysed routinely to verify instrument accuracy and repeatability.</i>
	<p><i>In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.</i></p>	

<p>Drilling techniques</p>	<p>Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</p>	<ul style="list-style-type: none"> • COBRE's Diamond drilling is being conducted with Tricone (Kalahari Sands), followed by PQ/HQ/NQ core sizes (standard tube) with HQ and NQ core oriented using AXIS Champ ORI tool. • COBRE's DTH drilling is being conducted with Tricone (very top part), followed by 11 inch (injection well only), 8 inch, and 5.5 inch sized hammer.
<p>Drill sample recovery</p>	<p>Method of recording and assessing core and chip sample recoveries and results assessed.</p>	<ul style="list-style-type: none"> • Core recovery is measured and recorded for all drilling. Once bedrock has been intersected, sample recovery has been very good >98%. • DTH samples are visually checked for recovery, moisture, and contamination.
	<p>Measures taken to maximise sample recovery and ensure representative nature of the samples.</p>	<ul style="list-style-type: none"> • Samples were taken consistently from the same side of the core cutting line to avoid bias. • Geologists frequently check the core cutting procedures to ensure the core cutter splits the core correctly in half. • Core samples are selected within logged geological, structural, mineralisation and alteration constraints. • Samples are collected from distinct geological domains with sufficient width to avoid overbias. • With regards to the DTH drilling, attempts were made to recover sufficient representative material during the drilling by the use of a stuffing box that is threaded onto the pre-collar casing.
	<p>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</p>	<ul style="list-style-type: none"> • For Diamond drilling, sample recovery was generally very good and as such it is not expected that any such bias exists. • The use of the stuffing box for the DTH drilling allowed fairly consistently recovery 10-15kg of material once in bedrock and dry, and around 5kg of material in wet conditions. There is no clear sample bias towards finer or coarser samples.

Logging	<p><i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i></p>	<ul style="list-style-type: none"> • <i>COBRE Diamond drill core samples are logged by a team of qualified geologists using predefined lithological, mineralogical, physical characteristic (colour, weathering etc) and logging codes.</i> • <i>The geologists on site followed industry best practice and standard operating procedure for Diamond core drilling processes.</i> • <i>Diamond drill core was marked up on site and logged back at camp where it is securely stored.</i> • <i>COBRE DTH drill programme is designed to be used for a primarily hydrogeological programme and is not intended for resource delineation purposes. Data is recorded digitally using Ocris geological logging software.</i> • <i>The QA/QC'd compilation of all logging results are stored and backed up on the cloud.</i>
	<p><i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i></p>	<ul style="list-style-type: none"> • <i>All logging used standard published logging charts and classification for grain size, abundance, colour and lithologies to maintain a qualitative and semi-quantitative standard based on visual estimation.</i> • <i>Magnetic susceptibility readings are also taken every meter and/or half meter using a ZH Instruments SM-20/SM-30 reader.</i>
	<p><i>The total length and percentage of the relevant intersections logged.</i></p>	<ul style="list-style-type: none"> • <i>100% of all recovered intervals are geologically logged.</i>
Sub-sampling techniques and sample preparation	<p><i>If core, whether cut or sawn and whether quarter, half or all core taken.</i></p>	<ul style="list-style-type: none"> • <i>Selected intervals are currently being cut (in half) with a commercial core cutter, using a 2mm thick blade, for one half to be sampled for analysis while the other half is kept for reference.</i> • <i>For selected samples core is quartered and both quarters being sampled as an original and field replicate sample.</i>
	<p><i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry</i></p>	<ul style="list-style-type: none"> • <i>A representative sample is collected from homogenised bulk samples using an aluminium sampling scoop. The sample is then reduced to approximately 100g of -</i>

		<p><i>180µm fraction which is retained for analysis.</i></p>
	<p><i>For all sample types, the nature, quality and appropriateness of the sample preparation techniques</i></p>	<ul style="list-style-type: none"> • <i>Soil samples are sieved to -180µm in the field and then further sieved to -90µm by the laboratory.</i> • <i>Field sample preparation is suitable for the core samples.</i> • <i>The laboratory sample preparation technique (ALS PREP-31D) is considered appropriate and suitable for the core samples and expected grades.</i> • <i>For metallurgical work, composite samples were collected from both high-grade and low-grade intersections totalling approximately 5 – 6m each.</i> • <i>Metallurgical intermittent bottle roll test work was carried out on a relatively fine reserve sample crush with plans to carry out future work on a coarse crush along with column testing which is deemed to be more representative of the in-situ environment.</i> • <i>DTH 1m samples for analysis are sieved to -180µm in the field camp (resulting in approximately 100g) and then assayed using pXRF at the camp laboratory.</i> • <i>1m samples for reference purpose consists of approximately 300g of unsieved material. Field sample preparation is suitable for the programme objective.</i>
	<p><i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i></p>	<ul style="list-style-type: none"> • <i>COBRE's standard field QAQC procedures for drilling and soil samples include the field insertion of blanks, selection of standards, field duplicates, replicates, and selection of requested laboratory pulp and coarse crush duplicates. These are being inserted at a rate of 2.5- 5% each to ensure an appropriate rate of QAQC.</i> • <i>Metallurgical samples were composited, homogenised and split into test charges.</i>

	<p><i>Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.</i></p>	<ul style="list-style-type: none"> • <i>Sampling is deemed appropriate for the type of survey and equipment used.</i> • <i>The duplicate sample data (field duplicate and lab duplicates) indicates that the results are representative and repeatable.</i> • <i>Metallurgical samples were taken from two drill intersections located 1km apart.</i> • <i>The DTH field duplicate and replicates samples indicates that the results are representative and repeatable.</i> • <i>Repeat pXRF readings are taken on very anomalous samples to ensure consistency and data veracity.</i>
	<p><i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i></p>	<ul style="list-style-type: none"> • <i>Initial metallurgical results quoted have been carried out on a fine crush sample. Future studies will utilise a coarser crush.</i>
<p>Quality of assay data and laboratory tests</p>	<p><i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i></p>	<ul style="list-style-type: none"> • <i>COBRE's core samples are being sent for 4-acid digest for "near total" digest and ICP-AES analysis (34 elements) at ALS laboratories in Johannesburg, South Africa.</i> • <i>The analytical techniques (ALS ME-ICP61 and ME-OG62) are considered appropriate for assaying.</i> • <i>Intermittent Bottle Roll Leach test work has been carried out on 6m composite samples from a high and low grade intersection in different portions of the Comet Target. Results provide an indication of the copper leach performance.</i> • <i>Comprehensive head assay was carried out on metallurgical samples to determine Cu speciation (acid soluble Cu, cyanide soluble Cu, residual Cu).</i> • <i>The objective of the DTH drill programme is primarily for hydrogeological test purposes, but is also being used to assess and monitor the down-dip variations of the mineralisation. The pXRF results are considered appropriate for the task</i>

	<p><i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i></p>	<ul style="list-style-type: none"> • <i>COBRE use ZH Instruments SM20 and SM30 magnetic susceptibility meters for measuring magnetic susceptibilities and readings are randomly repeated to ensure reproducibility and consistency of the data.</i> • <i>A Niton FXL950 pXRF instrument is used with reading times on Soil Mode of 120seconds in total.</i> • <i>For the DTH sample analysis, a Olympus Vanta VMR pXRF instrument are used with reading times on Geochem Mode of 150seconds in total. For the pXRF analyses, well established in-house SOPs were strictly followed and data QAQC'd before accepted in the database.</i> • <i>A test study of 5 times repeat analyses on selected soil samples is conducted to establish the reliability and repeatability of the pXRF at low Cu-Pb-Zn values.</i> • <i>For the pXRF Results, no user factor was applied, and as per SOP the units calibrated daily with their respective calibration disks.</i> • <i>All QAQC samples were reviewed for consistency and accuracy. Results were deemed repeatable and representative:</i>
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	<p><i>Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.</i></p>	<ul style="list-style-type: none"> • <i>Appropriate certified reference material was inserted on a ratio of 1:20 samples.</i> • <i>Laboratory coarse crush and pulp duplicate samples were alternated requested for every 20 samples.</i> • <i>Blanks were inserted on a ratio of 1:20.</i> • <i>ALS Laboratories insert their own standards, duplicates and blanks and follow their own SOP for quality control.</i> • <i>Both internal and laboratory QAQC samples are reviewed for consistency.</i> • <i>The inserted CRM's have highlighted acceptable laboratory accuracy and precision for Cu. The inserted CRM (OREAS96), highlighted acceptable accuracy and precision for results above 10ppm Ag. There is a rather poor precision for Ag at concentration levels of less than 10x the analytical method's detection limit (e.g. < 10ppm Ag).</i> • <i>The coarse Blank and lab internal pulp Blank results suggest a low risk of contamination during the sample preparation and analytical stages respectively.</i> • <i>The duplicate sample data indicates that the results are representative and repeatable for Cu and Ag.</i> • <i>External laboratory checks were carried out by Scientific Services Laboratories showing an excellent correlation and a high degree of repeatability of the results. The laboratory comparative sample data indicates that the analytical results from ALS Laboratories for Cu and Ag are representative and repeatable</i> • <i>For DTH pXRF analysis, the CRM's accuracy, precision and control charts are within acceptable limits for Cu.</i> • <i>The DTH duplicate and replicate sample data indicates that the results are representative and repeatable</i>
<p>Verification of sampling and assaying</p>	<p><i>The verification of significant intersections by either independent or alternative company personnel.</i></p>	<ul style="list-style-type: none"> • <i>All drill core intersections were verified by peer review.</i>

	<p><i>The use of twinned holes.</i></p>	<ul style="list-style-type: none"> • <i>No twinned holes have been drilled to date.</i>
	<p><i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i></p>	<ul style="list-style-type: none"> • <i>All data is electronically stored with peer review of data processing and modelling.</i> • <i>Data entry procedures standardized in SOP, data checking and verification routine.</i> • <i>Data storage on partitioned drives and backed up on server and on the cloud.</i>
	<p><i>Discuss any adjustment to assay data.</i></p>	<ul style="list-style-type: none"> • <i>No adjustments were made to assay data.</i>
<p>Location of data points</p>	<p><i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i></p>	<ul style="list-style-type: none"> • <i>COBRE's Drill collar coordinates are captured by using handheld Garmin GPS and verified by a second handheld Garmin GPS.</i> • <i>Drill holes are re-surveyed with differential DGPS at regular intervals to ensure sub-meter accuracy.</i> • <i>Downhole surveys of drill holes is being undertaken using an AXIS ChampMag tool or the Champ Gyro (for DTH)</i>
	<p><i>Specification of the grid system used.</i></p>	<ul style="list-style-type: none"> • <i>The grid system used is WGS84 UTM Zone 34S. All reported coordinates are referenced to this grid.</i>
	<p><i>Quality and adequacy of topographic control.</i></p>	<ul style="list-style-type: none"> • <i>Topographic control is based on satellite survey data collected at 30m resolution. Quality is considered acceptable.</i>
<p>Data spacing and distribution</p>	<p><i>Data spacing for reporting of Exploration Results.</i></p> <p><i>Whether the data spacing, and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i></p>	<ul style="list-style-type: none"> • <i>Data spacing and distribution of all survey types is deemed appropriate for the type of survey and equipment used.</i> • <i>Drill hole spacing is broad varying between 125 m to greater than 1 600 m, as might be expected for this stage of exploration.</i> • <i>DTH drill hole spacing is deemed appropriate for the type of survey and use intended.</i>
	<p><i>Whether sample compositing has been applied.</i></p>	<ul style="list-style-type: none"> • <i>N/A</i>

<p>Orientation of data in relation to geological structure</p>	<p>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</p>	<ul style="list-style-type: none"> • Drill spacing is currently broad and hole orientation is aimed at intersecting the bedding of the host stratigraphy as perpendicular as practically possible (e.g. within the constraint of the cover thickness). This is considered appropriate for the geological setting and for the known mineralisation styles in the Copperbelt.
	<p>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</p>	<ul style="list-style-type: none"> • Existence, and orientation, of preferentially mineralised structures is not yet fully understood but current available data indicates mineralisation occurs within steep, sub-vertical structures, sub-parallel to foliation. • No significant sampling bias is therefore expected. • For the DTH drilling, the holes were drilled mostly down-dip of the mineralisation and have introduced a sample bias.
<p>Sample security</p>	<p>The measures taken to ensure sample security.</p>	<ul style="list-style-type: none"> • Sample bags are logged, tagged, double bagged and sealed in plastic bags, stored at the field office. • Diamond core is stored in a secure facility at the field office and then moved to a secure warehouse. • Sample security includes a chain-of-custody procedure that consists of filling out sample submittal forms that are sent to the laboratory with sample shipments to make certain that all samples are received by the laboratory. Prepared samples were transported to the analytical laboratory in sealed gravel bags that are accompanied by appropriate paperwork, including the original sample preparation request numbers and chain-of-custody forms
<p>Audits or reviews</p>	<p>The results of any audits or reviews of sampling techniques and data.</p>	<ul style="list-style-type: none"> • COBRE's drill hole sampling procedure is done according to industry best practice. • Hydrogeological results are reviewed by WSP Australia • Metallurgical test work was conducted by and reviewed by Independent Metallurgical Operations Pty Ltd.

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		<ul style="list-style-type: none">• <i>Geological modelling was carried out and reviewed by Caracle Creek International Consulting.</i>
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JORC Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<p>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</p> <p>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</p>	<ul style="list-style-type: none"> • Cobre Ltd holds 100% of Kalahari Metals Ltd. • Kalahari Metals in turn owns 100% of Triprop Holdings Ltd and Kitlanya (Pty) Ltd both of which are locally registered companies. • Triprop Holdings holds the NCP licenses PL035/2017 (306.76km²) and PL036/2017 (49.8km²), which, following a recent renewal, are due their next extension on 30/09/2024
Exploration done by other parties	<p>Acknowledgment and appraisal of exploration by other parties.</p>	<ul style="list-style-type: none"> • Previous exploration on portions of the NCP and KITW projects was conducted by BHP. • BHP collected approximately 125 and 113 soil samples over the KITW and NCP projects respectively in 1998. • BHP collected Geotem airborne electromagnetic data over a small portion of PL036/2012 and PL342/2016, with a significant coverage over PL343/2016.
Geology	<p>Deposit type, geological setting and style of mineralisation.</p>	<ul style="list-style-type: none"> • The regional geological setting underlying all the Licences is interpreted as Neoproterozoic meta sediments, deformed during the Pan African Damara Orogen into a series of ENE trending structural domes cut by local structures. • The style of mineralisation expected comprises strata-bound and structurally controlled disseminated and vein hosted Cu/Ag mineralisation.

Drill hole Information

A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:

easting and northing of the drill hole collar

elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar

dip and azimuth of the hole

down hole length and interception depth

hole length.

If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.

- *Summary table of all completed core drill holes on the NCP licenses is presented below. All coordinates are presented in UTM Zone 34S, WGS84 datum. HGPS indicates that the holes were surveyed using a handheld GPS; DGPS indicates that the holes have been re-surveyed with differentially corrected GPS. Drill holes designated TRDH are original holes drilled by Triprop in 2014.*
- *Summary results of intersections are provided using a cut-off of 0.2% Cu to provide a comparable Cu_{eq} m% estimate ($Cu_{eq}\% = Cu\% + Ag(g/t) * 0.0087$) using metal prices from March 2023.*
- *Summary results for of > 1% Cu over 1m are provided in the next table.*

SiteID	Easting	Northing	RL	Grid	Method	Date	Company		
NCP01	594786.0	7694068.0	1052.0	UTM34S	HGPS	2019/07/06	Orezone		
NCP01A	594786.0	7694070.0	1052.0	UTM34S	HGPS	2019/06/13	Orezone		
NCP02	617226.0	7692104.0	999.0	UTM34S	HGPS	2019/06/20	Orezone		
NCP03	594746.0	7693874.0	1034.0	UTM34S	HGPS	2019/05/07	Orezone		
NCP04	590768.0	7691124.0	1054.0	UTM34S	HGPS	2019/06/30	Orezone		
NCP05	590566.0	7691488.0	1053.0	UTM34S	HGPS	2019/05/08	Orezone		
NCP06	590610.0	7691398.0	1050.0	UTM34S	HGPS	2019/12/08	Orezone		
NCP07	599889.5	7685403.0	1099.2	UTM34s	DGPS	2022/11/07	Mitchell Drilling		
NCP08	598985.5	7684909.0	1101.9	UTM34s	DGPS	2022/07/23	Mitchell Drilling		
NCP09	598092.8	7684452.0	1102.5	UTM34s	DGPS	2022/07/28	Mitchell Drilling		
NCP10	601620.3	7686327.4	1092.4	UTM34s	DGPS	2022/04/08	Mitchell Drilling		
NCP11	598960.0	7684952.0	1068.0	UTM34s	HGPS	2022/11/08	Mitchell Drilling		
NCP11-A	598963.0	7684949.0	1083.0	UTM34s	HGPS	2022/08/13	Mitchell Drilling		
NCP11-B	598958.5	7684956.8	1101.9	UTM34s	DGPS	2022/08/13	Mitchell Drilling		
NCP12	599431.6	7685158.1	1100.5	UTM34s	DGPS	2022/08/31	Mitchell Drilling		

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NCP13	598533.8	7684688.8	1102.8	UTM34s	DGPS	2022/05/09	Mitchell Drilling		
NCP14	600311.2	7685611.5	1097.5	UTM34s	DGPS	2022/12/09	Mitchell Drilling		
NCP15	601192.3	7686073.9	1095.5	UTM34s	DGPS	2022/09/20	Mitchell Drilling		
NCP16	602078.3	7686537.5	1092.0	UTM34s	DGPS	2022/09/27	Mitchell Drilling		
NCP17	599185.6	7685059.8	1100.6	UTM34s	DGPS	2022/03/10	Mitchell Drilling		
NCP18	598730.0	7684840.0	1098.0	UTM34s	HGPS	2023/03/10	Mitchell Drilling		
NCP18A	598727.0	7684848.1	1102.1	UTM34s	DGPS	2022/07/10	Mitchell Drilling		
NCP19	599212.0	7685019.7	1100.3	UTM34s	DGPS	2022/11/10	Mitchell Drilling		
NCP20	598762.0	7684798.0	1115.0	UTM34s	HGPS	2022/10/15	Mitchell Drilling		
NCP20A	598758.7	7684796.7	1102.2	UTM34s	DGPS	2022/10/22	Mitchell Drilling		
NCP21	589691.0	7679008.0	1104.0	UTM34s	HGPS	2022/10/17	Mitchell Drilling		
NCP22	587387.0	7677006.0	1103.0	UTM34s	HGPS	2022/10/25	Mitchell Drilling		
NCP23	599161.4	7685097.5	1100.9	UTM34s	DGPS	2022/10/28	Mitchell Drilling		
NCP24	605254.0	7688076.0	1075.0	UTM34s	HGPS	2022/07/11	Mitchell Drilling		
NCP25	598876.3	7684850.8	1101.4	UTM34s	DGPS	2022/12/21	Mitchell Drilling		
NCP26	598643.5	7684747.6	1102.8	UTM34s	DGPS	2022/11/19	Mitchell Drilling		
NCP27	605504.0	7683642.0	1066.0	UTM34s	HGPS	2022/12/11	Mitchell Drilling		
NCP28	598622.2	7684786.0	1102.7	UTM34s	DGPS	2022/11/24	Mitchell Drilling		
NCP29	600751.0	7679853.0	1097.0	UTM34s	HGPS	2022/11/20	Mitchell Drilling		
NCP30	598851.9	7684887.0	1101.7	UTM34s	DGPS	2022/11/24	Mitchell Drilling		
NCP31	599441.0	7678120.0	1104.0	UTM34s	HGPS	2022/11/26	Mitchell Drilling		
NCP31A	599444.0	7678119.0	1099.0	UTM34s	HGPS	2022/11/24	Mitchell Drilling		
NCP32	610528.0	7686927.0	1046.0	UTM34s	HGPS	2022/11/30	Mitchell Drilling		
NCP33	610575.0	7686839.0	1053.0	UTM34s	HGPS	2022/03/12	Mitchell Drilling		
NCP34	590274.0	7679998.0	1103.0	UTM34s	HGPS	2022/12/05	Mitchell Drilling		
NCP35	610144.0	7686583.0	1049.0	UTM34s	HGPS	2023/01/20	Mitchell Drilling		
NCP36	601039.0	7679350.0	1096.0	UTM34s	HGPS	2023/01/22	Mitchell Drilling		
NCP37	612295.0	7687857.0	1060.0	UTM34s	HGPS	2023/01/27	Mitchell Drilling		
NCP38	612746.0	7688085.0	1060.0	UTM34s	HGPS	2023/02/04	Mitchell Drilling		
NCP39	600936.0	7679534.0	1090.0	UTM34s	HGPS	2023/02/03	Mitchell Drilling		
NCP40	611022.0	7687064.0	1039.0	UTM34s	HGPS	2023/02/08	Mitchell Drilling		
NCP41	592796.0	7681630.0	1097.0	UTM34s	HGPS	2023/02/14	Mitchell Drilling		
NCP42	607051.0	7688937.0	1052.0	UTM34s	HGPS	2023/02/19	Mitchell Drilling		

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NCP43	599098.0	7684964.0	1085.0	UTM34s	HGPS	2023/02/23	Mitchell Drilling		
NCP44	586591.5	7676382.2	1123.7	UTM34s	HGPS	2023/03/07	Mitchell Drilling		
NCP45	600106.8	7685494.0	1099.4	UTM34s	HGPS	2023/03/04	Mitchell Drilling		
NCP46	600529.7	7685715.5	1096.7	UTM34s	HGPS	2023/03/10	Mitchell Drilling		
NCP47	595337.9	7670959.5	1133.1	UTM34s	HGPS	2023/03/21	Mitchell Drilling		
NCP48	601417.1	7686190.8	1093.7	UTM34s	HGPS	2023/03/16	Mitchell Drilling		
NCP49	600005.8	7685434.3	1100.4	UTM34s	HGPS	2023/03/21	Mitchell Drilling		
NCP50	599790.2	7685325.2	1097.3	UTM34s	HGPS	2023/03/25	Mitchell Drilling		
NCP51	597630.8	7684254.0	1101.2	UTM34s	HGPS	2023/03/31	Mitchell Drilling		
NCP52	598764.0	7684788.0	1101.0	UTM34s	HGPS	2023/04/03	Mitchell Drilling		
MW_001	598846.1	7684767.8	1102.2	UTM34s	DGPS	2023/10/11	Mitchell Drilling		
MW_002	598840.0	7684690.7	1101.0	UTM34s	DGPS	2024/01/18	Mitchell Drilling		
MW_010	598817.1	7684772.7	1102.3	UTM34s	DGPS	2023/08/12	Mitchell Drilling		
PW_001	598816.8	7684742.0	1102.3	UTM34s	DGPS	2024/01/29	Mitchell Drilling		
TRDH14-01	612238.0	7687953.0	1042.0	UTM34s	HGPS	2014/11/07	RDS		
TRDH14-02	612339.0	7687802.0	1047.0	UTM34s	HGPS	2014/07/14	RDS		
TRDH14-02A	612338.0	7687804.0	1047.0	UTM34s	HGPS	2014/07/16	RDS		
TRDH14-03	612281.0	7687887.0	1042.0	UTM34s	HGPS	2014/07/18	RDS		
TRDH14-04	609703.0	7686345.0	1040.0	UTM34s	HGPS	2014/07/21	RDS		
TRDH14-05	609596.0	7686512.0	1040.0	UTM34s	HGPS	2014/07/21	RDS		
TRDH14-06	609653.0	7686433.0	1038.0	UTM34s	HGPS	2014/07/24	RDS		
TRDH14-07	609663.0	7686414.0	1042.0	UTM34s	HGPS	2014/07/25	RDS		
TRDH14-08	607204.0	7684683.0	1056.0	UTM34s	HGPS	2014/01/08	RDS		
TRDH14-09	607133.0	7684805.0	1055.0	UTM34s	HGPS	2014/05/08	RDS		
TRDH14-10	607061.0	7684936.0	1024.0	UTM34s	HGPS	2014/06/08	RDS		
TRDH14-11	607150.0	7684776.0	1014.0	UTM34s	HGPS	2014/08/08	RDS		
TRDH14-12	600845.0	7685696.0	1080.0	UTM34s	HGPS	2014/08/18	RDS		
TRDH14-13	600924.0	7685567.0	1073.0	UTM34s	HGPS	2014/08/20	RDS		
TRDH14-14	600816.0	7685737.0	1070.0	UTM34s	HGPS	2014/08/22	RDS		
TRDH14-15	600721.0	7685893.0	1042.0	UTM34s	HGPS	2014/03/09	RDS		
TRDH14-16	600758.0	7685834.0	1081.0	UTM34s	HGPS	2014/09/15	RDS		
TRDH14-16A	600764.0	7685829.0	1083.0	UTM34s	HGPS	2014/09/17	RDS		
TRDH14-17	608880.0	7685776.0	1027.0	UTM34s	HGPS	2014/09/30	RDS		

TRDH14-17A	608862.0	7685805.0	1028.0	UTM34s	HGPS	2014/03/10	RDS		
Down hole intersections using low grade cut-off (0.2% Cu) to establish Cu _{eq} m% for each hole. Resulted sorted by Cu _{eq} m%									
Hole Id	FROM	TO	Length	Cu _{eq} m%	Intersection				
PW_001	187.0	265.0	78.0	45.8	78m @ 0.59% Cu pXRF, drilled down-dip				
NCP20A	124.0	159.0	35.0	41.6	35m @ 1.3% Cu & 18g/t Ag				
NCP08	125.0	146.9	21.9	20.1	21.9m @ 0.8% Cu & 13g/t Ag				
MW_001	97.0	122.0	25.0	13.1	25.0m @ 0.52% Cu pXRF, drilled down-dip				
NCP25	122.0	141.0	19.0	11.8	19m @ 0.5% Cu & 13g/t Ag				
NCP40	269.0	298.0	29.0	11.3	29m @ 0.4% Cu & 3g/t Ag				
NCP45	188.9	204.6	15.7	10.4	15.7m @ 0.5% Cu & 15g/t Ag				
TRDH14-07	62.0	87.5	25.5	9.5	25.5m @ 0.4% Cu & 1g/t Ag				
NCP42	142.5	157.5	15.0	9.4	15m @ 0.5% Cu & 13g/t Ag				
NCP43	157.0	174.8	17.8	8.8	17.8m @ 0.4% Cu & 10g/t Ag				
NCP33	228.0	244.7	16.7	8.8	16.7m @ 0.5% Cu & 4g/t Ag				
NCP51	221.2	238.9	17.7	8.6	17.7m @ 0.4% Cu & 12g/t Ag				
NCP29	187.0	206.2	19.2	7.8	19.2m @ 0.3% Cu & 8g/t Ag				
NCP50	177.9	192.0	14.1	7.6	14.1m @ 0.5% Cu & 11g/t Ag				
NCP35	238.0	255.9	17.9	7.5	17.9m @ 0.4% Cu & 6g/t Ag				
NCP49	177.8	190.8	12.9	7.2	12.9m @ 0.5% Cu & 13g/t Ag				
NCP07	249.0	261.0	12.0	7.0	12m @ 0.5% Cu & 13g/t Ag				
NCP38	261.0	272.6	11.6	6.2	11.6m @ 0.5% Cu & 7g/t Ag				
TRDH14-11	125.9	140.5	14.6	6.2	14.6m @ 0.4% Cu & 1g/t Ag				
NCP18A	280.5	292.2	11.6	6.1	11.6m @ 0.5% Cu & 9g/t Ag				
NCP09	108.2	121.3	13.1	5.9	13.1m @ 0.4% Cu & 7g/t Ag				
NCP37	186.0	203.0	17.0	5.5	17m @ 0.3% Cu & 3g/t Ag				
NCP19	147.3	157.0	9.7	4.8	9.7m @ 0.4% Cu & 10g/t Ag				
NCP11-B	345.0	353.6	8.6	4.7	8.6m @ 0.5% Cu & 12g/t Ag				
TRDH14-16A	169.2	173.7	4.5	4.4	4.5m @ 0.8% Cu & 4g/t Ag				

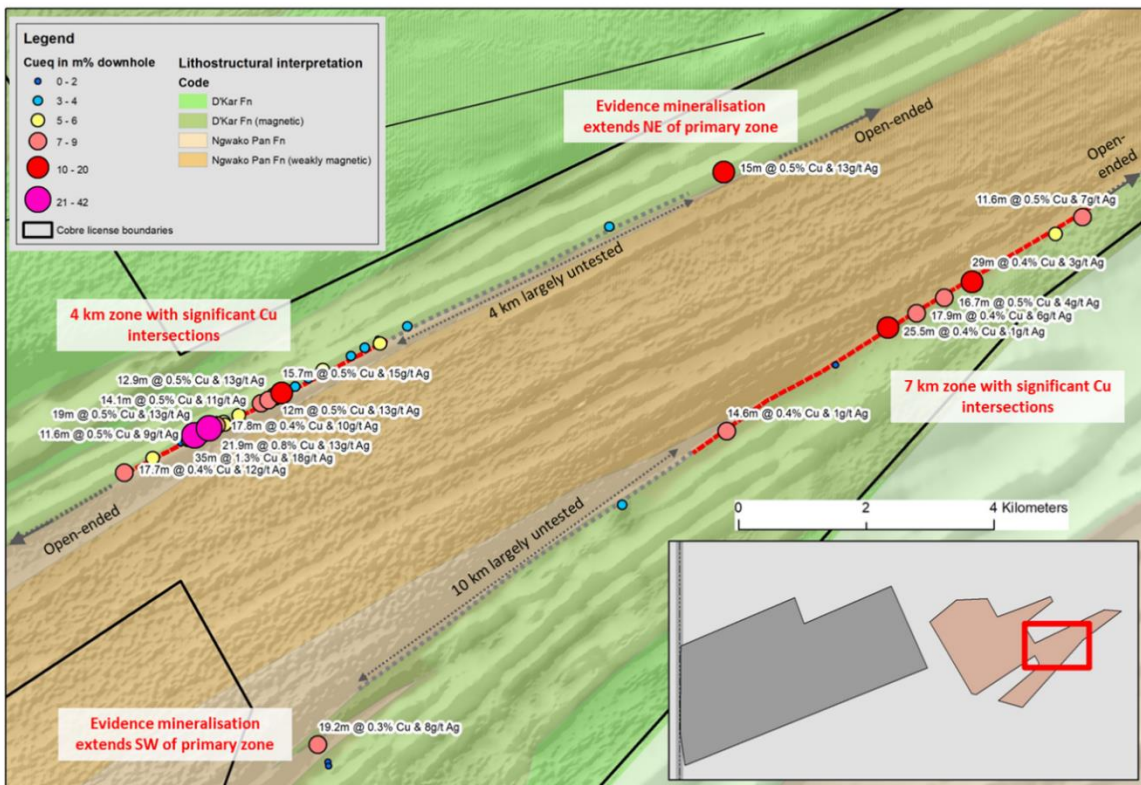
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NCP12	215.5	223.4	7.9	4.4	7.9m @ 0.5% Cu & 12g/t Ag
NCP10	311.3	319.2	7.9	4.4	7.9m @ 0.5% Cu & 12g/t Ag
MW_010	186.0	194.0	8.0	4.4	8.0m @ 0.55% Cu <i>pXRF</i>
NCP30	237.0	246.2	9.2	4.2	9.2m @ 0.4% Cu & 9g/t Ag
NCP23	424.0	431.7	7.7	4.2	7.7m @ 0.5% Cu & 9g/t Ag
NCP26	199.7	208.7	9.0	4.1	8.9m @ 0.4% Cu & 8g/t Ag
NCP48	171.2	182.0	10.8	4.0	10.8m @ 0.3% Cu & 6g/t Ag
NCP34	398.9	409.5	10.7	3.5	10.7m @ 0.2% Cu & 16g/t Ag
NCP17	236.8	243.5	6.6	3.2	6.6m @ 0.4% Cu & 11g/t Ag
NCP15	192.0	198.9	6.8	3.0	6.8m @ 0.4% Cu & 9g/t Ag
NCP24	178.0	191.3	13.3	2.9	13.3m @ 0.2% Cu & 3g/t Ag
NCP21	118.0	129.0	11.0	2.9	11m @ 0.2% Cu & 4g/t Ag
NCP14	232.0	238.6	6.6	2.6	6.6m @ 0.3% Cu & 10g/t Ag
NCP22	144.0	149.6	5.6	2.4	5.6m @ 0.3% Cu & 15g/t Ag
NCP46	170.0	175.4	5.4	2.4	5.4m @ 0.4% Cu & 3g/t Ag
NCP44	283.0	288.4	5.4	2.3	5.4m @ 0.2% Cu & 26g/t Ag
NCP27	152.4	156.2	3.8	2.2	3.8m @ 0.5% Cu & 6g/t Ag
NCP16	188.0	196.2	8.3	2.1	8.3m @ 0.2% Cu & 6g/t Ag
NCP28	274.0	279.9	5.9	1.9	5.9m @ 0.3% Cu & 6g/t Ag
NCP13	171.4	176.8	5.4	1.4	5.4m @ 0.2% Cu & 2g/t Ag
NCP39	333.0	338.5	5.5	1.3	5.5m @ 0.2% Cu & 1g/t Ag
NCP43	123.6	126.0	2.4	1.3	2.4m @ 0.5% Cu & 9g/t Ag
NCP35	169.0	175.0	6.0	1.3	6m @ 0.2% Cu & 1g/t Ag
NCP36	509.5	514.2	4.7	1.2	4.7m @ 0.2% Cu & 2g/t Ag
NCP10	211.0	213.0	2.0	1.0	2m @ 0.4% Cu & 12g/t Ag
NCP26	135.0	136.0	1.0	0.8	1m @ 0.7% Cu & 4g/t Ag
NCP31A	310.1	311.8	1.7	0.8	1.7m @ 0.3% Cu & 17g/t Ag
NCP43	152.0	155.0	3.0	0.8	3m @ 0.2% Cu & 5g/t Ag
NCP10	149.0	151.0	2.0	0.8	2m @ 0.4% Cu & 4g/t Ag
NCP11-B	338.0	340.1	2.1	0.7	2.1m @ 0.3% Cu & 8g/t Ag

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NCP52	106.5	108.7	2.2	0.6	2.2m @ 0.2% Cu & 5g/t Ag
NCP52	96.0	98.3	2.3	0.6	2.3m @ 0.2% Cu & 4g/t Ag
NCP41	435.1	436.5	1.4	0.5	1.4m @ 0.2% Cu & 12g/t Ag
Down hole intersections calculated using a grade cut-off 1% Cu. Results sorted by Hole id.					
Hole id	FROM	TO	Length (m)	Intersection	
MW_001	97.0	98.0	1.0	1m @ 1% Cu pXRF	
MW_001	106.0	107.0	1.0	1m @ 1.1% Cu pXRF	
MW_010	189.0	190.0	1.0	1m @ 1.1% Cu pXRF	
NCP08	136.2	146.9	10.7	10.7m @ 1.3% Cu & 18g/t Ag	
NCP10	318.0	319.2	1.2	1.2m @ 1.1% Cu & 26g/t Ag	
NCP20A	148.7	158.0	9.3	9.3m @ 3.4% Cu & 30g/t Ag	
NCP25	133.0	136.0	3.0	3m @ 1% Cu & 15g/t Ag	
NCP26	207.7	208.7	1.0	1m @ 1.3% Cu & 16g/t Ag	
NCP29	198.7	201.0	2.3	2.3m @ 1.1% Cu & 14g/t Ag	
NCP33	240.2	242.0	1.8	1.8m @ 1% Cu & 12g/t Ag	
NCP38	270.7	272.6	1.9	1.9m @ 1.1% Cu & 21g/t Ag	
NCP40	296.8	298.0	1.2	1.2m @ 1.1% Cu & 1g/t Ag	
PW_001	198.0	199.0	1.0	1m @ 1.3% Cu pXRF	
TRDH14-16A	171.2	173.72	2.5	2.5m @ 1.4% Cu & 11g/t Ag	
Data aggregation methods	<p><i>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.</i></p> <p><i>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</i></p> <p><i>The assumptions used for any reporting of metal equivalent values should be clearly stated.</i></p>				<ul style="list-style-type: none"> <i>Results > 0.2% Cu have been averaged weighted by downhole lengths, and exclusive of internal waste to determine a Cu metre percent average for the holes.</i> <i>A second result with cutoff > 1% Cu has been included to highlight higher grade portions of the drill hole intersections.</i> <i>No aggregation of intercepts has been reported.</i> <i>Where copper equivalent has been calculated it is at current metal prices: 1g/t Ag = 0.0081% Cu.</i>

<p>Relationship between mineralisation widths and intercept lengths</p>	<p>These relationships are particularly important in the reporting of Exploration Results.</p> <p>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</p> <p>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').</p>	<ul style="list-style-type: none"> Down hole intersection widths are used throughout. Most of the drill intersections are into steep to vertically dipping units. True thickness is anticipated to be in the order of 50% of the downhole thickness although step-out drilling will be required to accurately model this particularly for the new targets. All measurements state that downhole lengths have been used, as the true width has not been suitably established by the current drilling.
<p>Diagrams</p>	<p>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</p>	



Plan map illustrating the position of drill holes coloured by Cu_{eq}m%.

Balanced reporting

Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.

- *Results from the previous exploration programmes are summarised in the target priorities which are based on an interpretation of these results.*
- *The accompanying document is considered to be a balanced and representative report.*