

Tuesday, 30<sup>th</sup> January 2024

## Maiden Mineral Resource Estimate at Storm Project, Canada

### *Initial resource drilling has established a remarkable foundation for the rapid growth of copper resources*

- **Maiden independent JORC 2012 Indicated and Inferred Mineral Resource Estimate (MRE) defines 17.5Mt @ 1.2% Cu and 3.4g/t Ag (0.35% Cu cut-off)<sup>1</sup>, comprising:**
  - A total metal content of **205Kt of copper and 1.9Moz of silver**
  - 30% of metal is classified in the high-confidence **indicated** category
- **The MRE contains a higher-grade core of 11.2Mt @ 1.5% Cu, 4.3g/t Ag (0.7% Cu cut-off) with 173Kt of copper and 1.5Moz of silver<sup>1</sup>**
- **Near-surface resource indicates potential for low-cost development:**
  - Mineralisation commences at, or very close to surface, and can potentially be accessed with **open-pit mining**
  - **100% of the MRE is categorised as fresh, chalcocite dominant copper sulphide** with preliminary studies showing amenability to low-cost beneficiation processing, including ore sorting
- **Located in a Tier 1 mining jurisdiction in Canada with strong Territorial and Federal Government support for critical minerals projects including copper**
- **Extraordinary growth and upside potential:**
  1. **Open in all directions** – the Storm resource remains open in all directions, creating confidence in the potential for significant and rapid growth during 2024 and beyond
  2. **MRE does not include several discoveries** – high-grade 2023 copper discoveries at **Thunder** (48.6m @ 3% Cu in ST23-03), **Lightning Ridge** (15.2m @ 2.3% Cu and 15.2m @ 2.1% Cu in ST23-52) and **Cyclone North** (7.6m @ 1% Cu in ST23-55) have not yet been included in the MRE
  3. **Emerging camp** – potential copper mining camp with multiple deposits already defined and numerous large targets to be tested in 2024 including six near-surface, high-priority EM anomalies where there has been a 100% correlation between geophysical anomalies and high-grade copper sulphides
  4. **Belt scale** – less than 5% of the 100km long prospective copper bearing horizon within the Project area has been drill tested, including the Tempest Prospect which has a 4km long copper-zinc gossan identified at surface
- **Major drilling program planned for 2024 to significantly expand the Mineral Resource, and to test the Storm area as well as other discoveries and regional exploration targets**

<sup>1</sup> Detailed supporting information for the MRE is presented in Appendices A and B of this ASX announcement.



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American West Metals Limited (**American West** or **the Company**) (ASX: AW1 | OTCQB: AWMLF) is pleased to announce the maiden JORC Code 2012 compliant Indicated and Inferred Mineral Resource Estimate (**MRE**) for its 80% owned Storm Copper Project (**Storm** or **the Project**) on Somerset Island, Nunavut, Canada.

**Dave O'Neill, Managing Director of American West Metals commented:**

*“The maiden JORC compliant mineral resource estimate (MRE) for the Storm Project has exceeded our expectations and delivered the foundations to what we believe will be a globally significant copper district.*

*“Within only a single season of resource drilling we have rapidly defined four robust copper deposits very close to surface: Cyclone, Chinook, Corona, and Cirrus. The setting and scale of the mineralisation gives us the opportunity to potentially mine 100% of the resource with open-pit methods and use cut-off grades much lower than underground deposits. The outcome is more copper metal.*

*“The initial resource is blessed with outstanding and immediate growth potential. The known copper deposits remain open and the high-grade Thunder, Lightning Ridge and Cyclone North discoveries of 2023 are not yet included in the MRE.*

*“A major drilling program has been planned to drill out the 2023 discoveries, expand the known deposits and test new, high-priority exploration targets that appear to be analogues to the known copper mineralisation. Work is also underway on the Canadian NI 43-101 compliant MRE, which will also be released soon.*

*“The maiden JORC MRE has underlined the exceptional opportunity presented by Storm to create further significant value for American West Metals shareholders. We look forward to updating investors and discussing our 2024 exploration and resource expansion plans via a Webinar tomorrow, and through further news updates in the coming weeks.”*

Deposit	Category	Ore Type	Tonnes	Cu (%)	Ag (g/t)	Cu (t)	Ag (Oz)
<b>Cyclone</b> (4100N Zone)	Inferred	Sulphide	7,210,000	1.20	4.03	86,800	934,700
	Indicated	Sulphide	4,880,000	1.26	3.45	61,600	541,100
<b>Chinook</b> (2750N Zone)	Inferred	Sulphide	2,190,000	1.47	4.00	32,300	282,300
<b>Corona</b> (2200N Zone)	Inferred	Sulphide	1,639,228	0.89	1.48	14,700	77,700
<b>Cirrus</b> (3500N Zone)	Inferred	Sulphide	1,554,155	0.62	1.29	9,700	64,400
<b>Total</b>	<b>Inferred</b>	<b>Sulphide</b>	<b>12,600,000</b>	<b>1.14</b>	<b>3.35</b>	<b>143,400</b>	<b>1,359,200</b>
<b>Total</b>	<b>Indicated</b>	<b>Sulphide</b>	<b>4,880,000</b>	<b>1.26</b>	<b>3.45</b>	<b>61,600</b>	<b>541,100</b>
<b>Total</b>	<b>Ind + Inf</b>	<b>Sulphide</b>	<b>17,480,000</b>	<b>1.17</b>	<b>3.38</b>	<b>205,000</b>	<b>1,900,200</b>

Table 1: Total unconstrained MRE of all material categories using a 0.35% Cu cut-off. The above MRE is reported in accordance with the Australian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (**JORC Code – 2012**). Some totals may not add up due to rounding. Appendices A and B of this ASX announcement contain detailed supporting information for the MRE.



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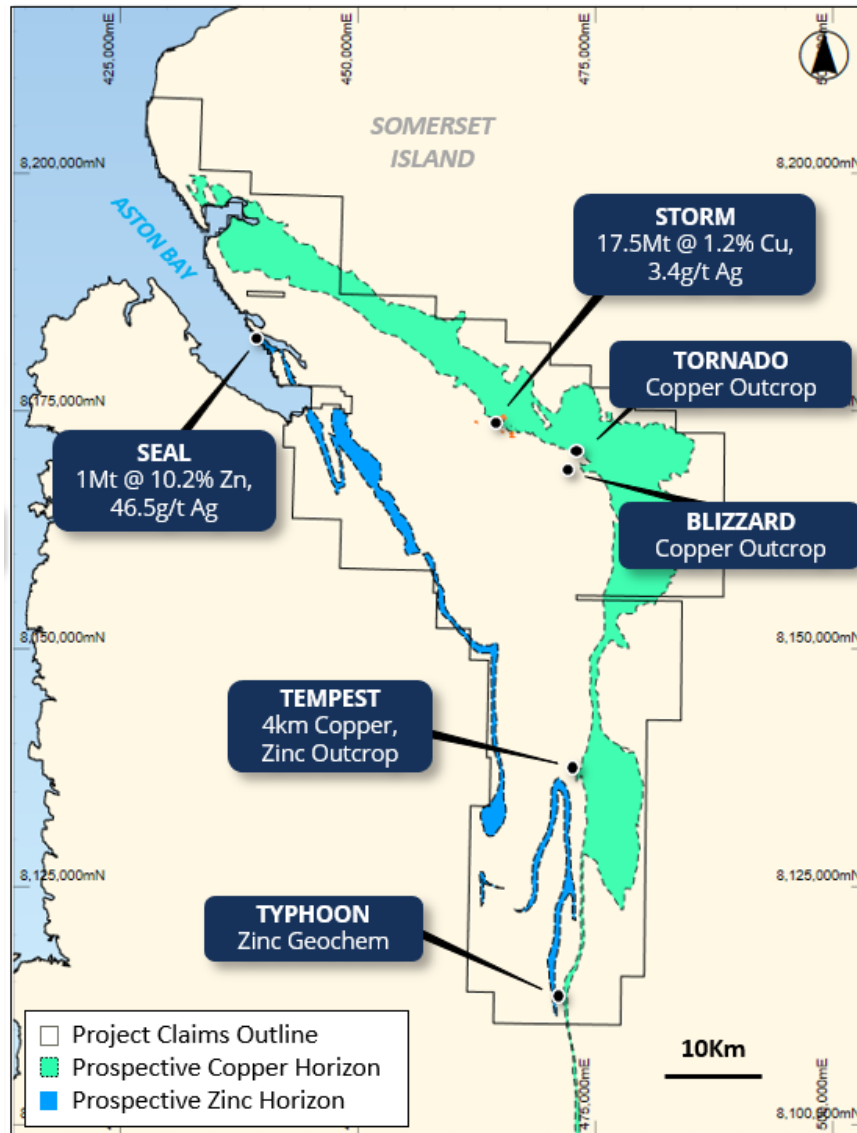


Figure 1: Map of the Project area showing the known copper and base metal deposits/prospects, project boundary, and interpreted prospective copper and zinc horizons. The prospective strike of the known copper horizon is more than 100km.

Note - The resources for the Seal Deposit are historical and foreign and are reported under Canadian NI 43-101 standards, not in accordance with the 2012 JORC Code. For details of the Seal resource, see our Prospectus dated 29 October 2021.

### STORM MINERAL RESOURCE ESTIMATION AND CLASSIFICATION

The maiden JORC compliant Indicated and Inferred Mineral Resource Estimation (MRE) for Storm was completed by international geological consulting company APEX Geoscience Ltd.

The Storm MRE includes data from 50 Reverse Circulation (RC) and 53 diamond drill holes, 52% of which were completed during the 2023 field season. Four high-grade, indicated and inferred, copper-silver deposits have been defined which include the Cyclone Deposit (4100N Zone), Chinook Deposit (2750N Zone), Corona Deposit (2200N Zone) and Cirrus Deposit (3750N Zone) (Figure 2).



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The copper-silver mineralisation within the Storm Deposits is sediment-hosted and outcropping or located near-surface. The Deposits are defined as flat-lying, stratabound and laterally extensive (Cyclone and Corona), and breccia/fault hosted and sub-vertical/steeply dipping (Chinook and Cirrus). All of the mineralisation defined within the MRE is classified as fresh sulphide, and is chalcocite dominant. The Deposits remain open in every direction and will require further drilling to determine the full extent of the high-grade copper mineralisation.

The Company has initiated mining and processing studies which are a critical step in the preparation of future mine permitting applications. The initial studies suggest that due to the shallow nature and favourable geometry of the Storm copper mineralisation, the Deposits may potentially be mined with traditional open-pit methods. The ongoing metallurgical studies by American West have confirmed the amenability of ores to a range of low-cost ore-sorting and beneficiation process methods with excellent recoveries of copper. All mining and metallurgical studies are preliminary in nature and not considered to be 'Scoping Level,' with test and further study work still underway. Figures 2 to 6 below are based on the assumptions used in the MRE; they are conceptual in nature and subject to further mining studies which are required to confirm the potential for a mining operation at Storm. (See Appendix A for a summary of the studies considered for the MRE).

The shallow nature, favourable geometry and high copper grades of the Storm deposits have set the foundation for what the company believes will be a large scale, open-pit copper mining camp in the Storm area.

Appendices A and B of this ASX announcement contain detailed supporting information for the MRE.

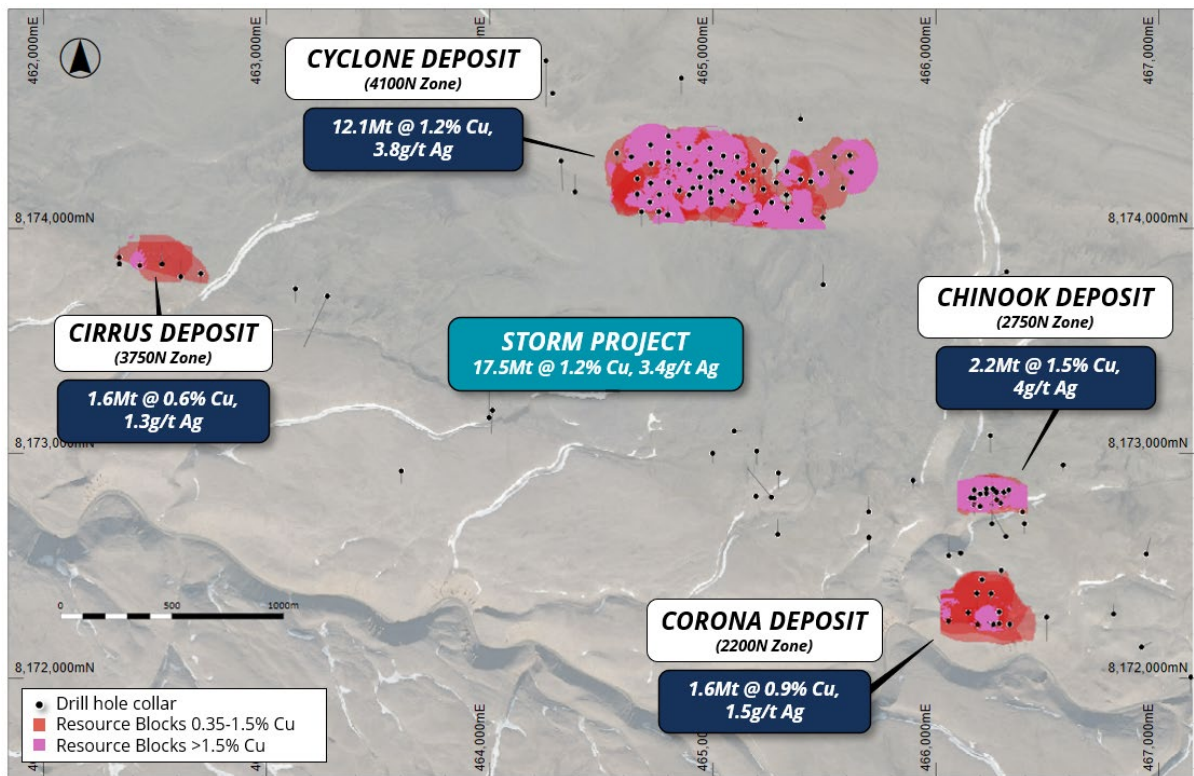


Figure 2: Plan view of the total MRE blocks (Indicated + Inferred) for the Storm Project overlaying aerial photography. Resource blocks are coloured with a 0.35% and 1.5% Cu cut-off.



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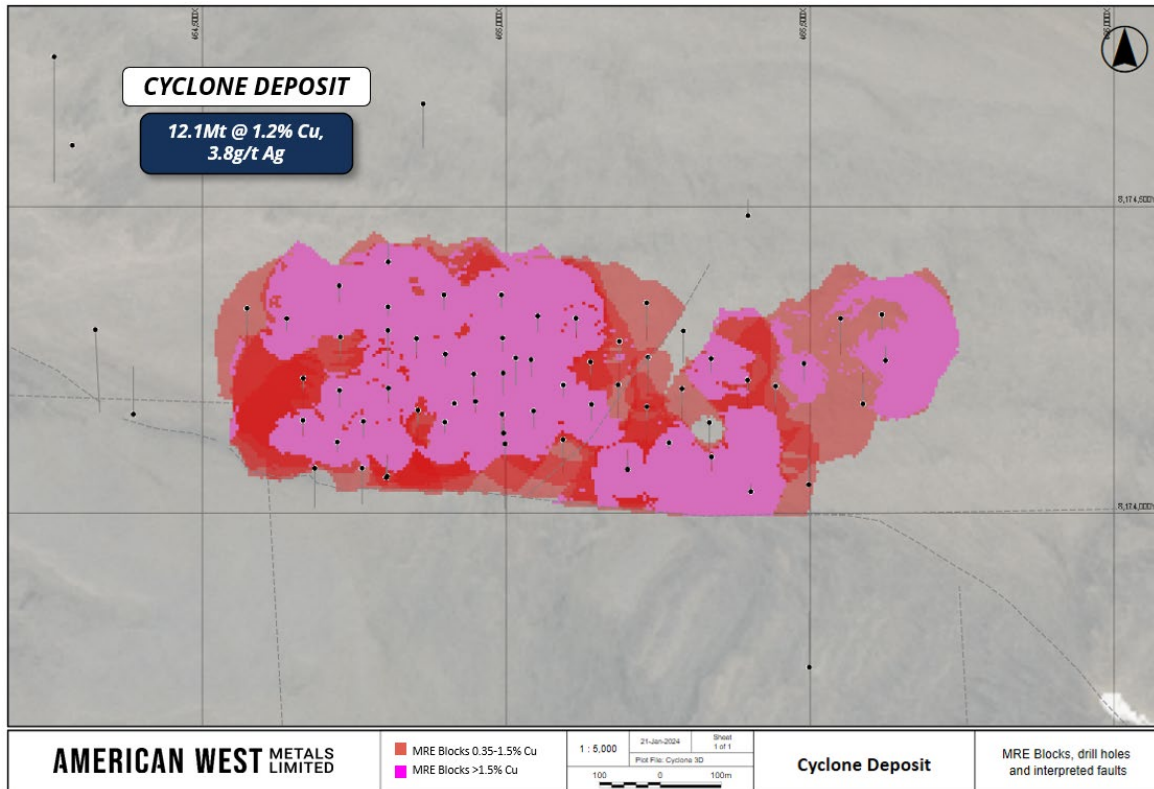


Figure 3: Plan view of the Cyclone Deposit showing conceptual MRE blocks.

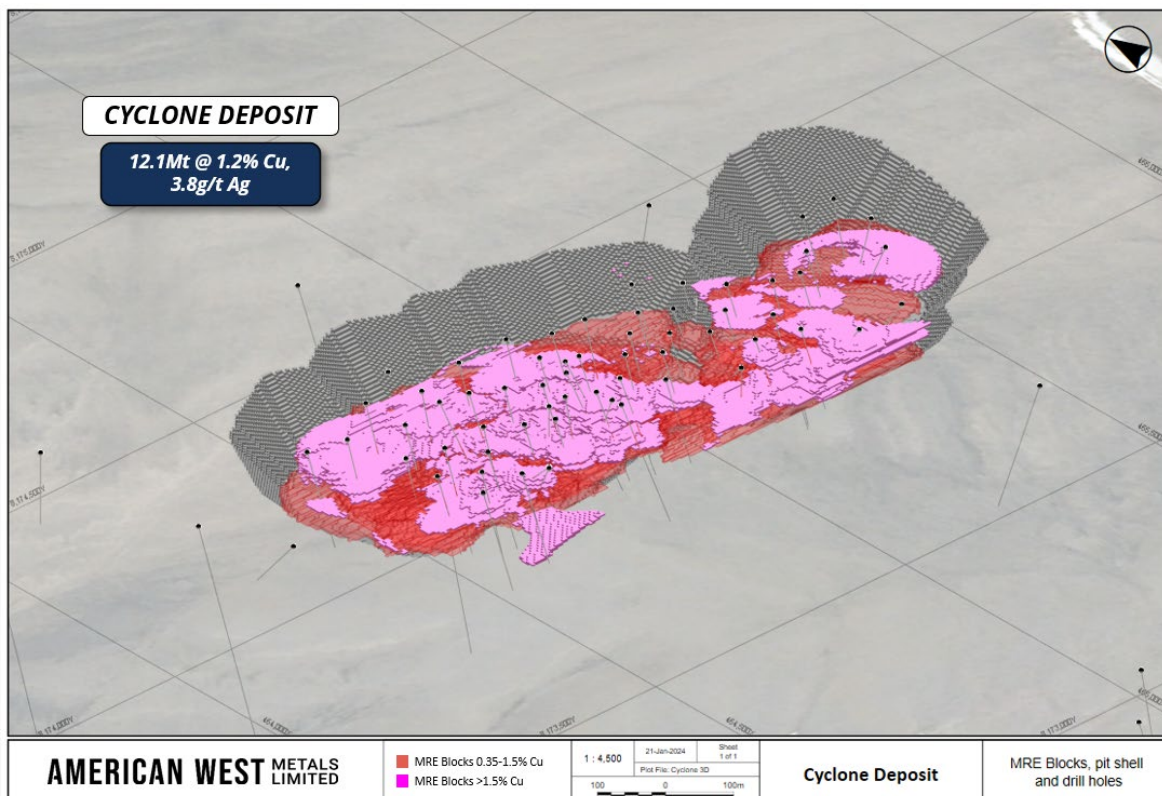


Figure 4: Orthographic view (looking NE) of the Cyclone Deposit and conceptual pit shell.

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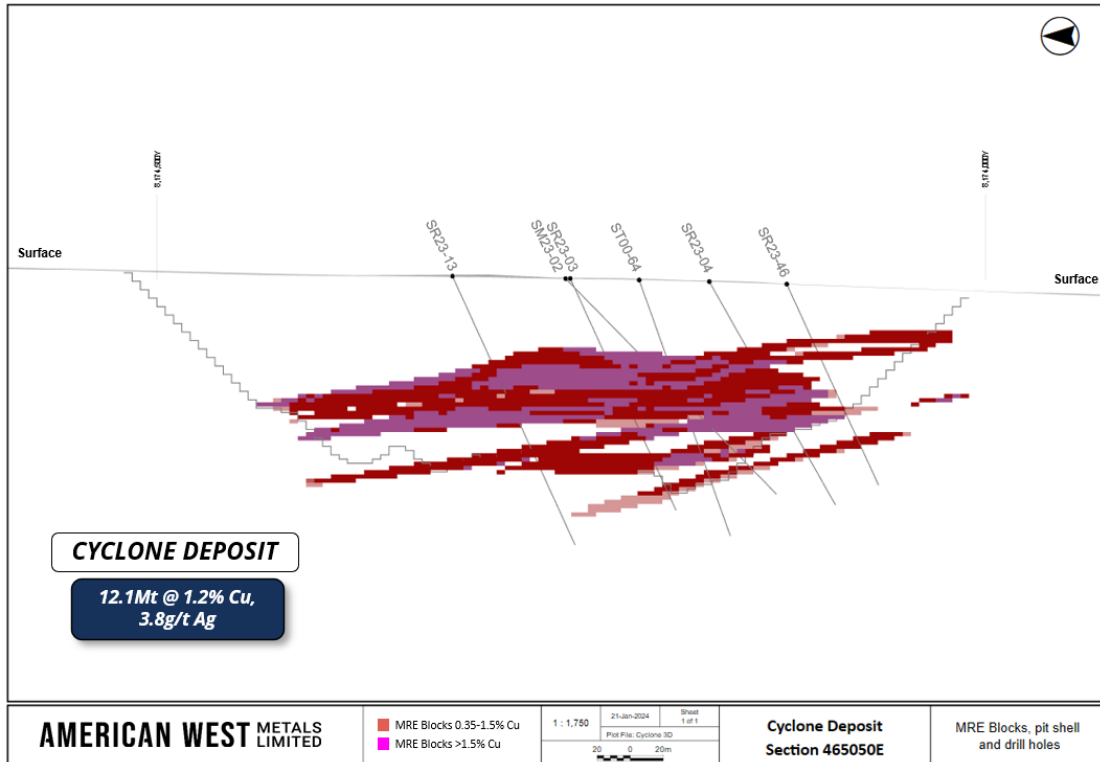


Figure 5: Cross section view (looking east at 465050E) of the Cyclone Deposit and conceptual pit shell.

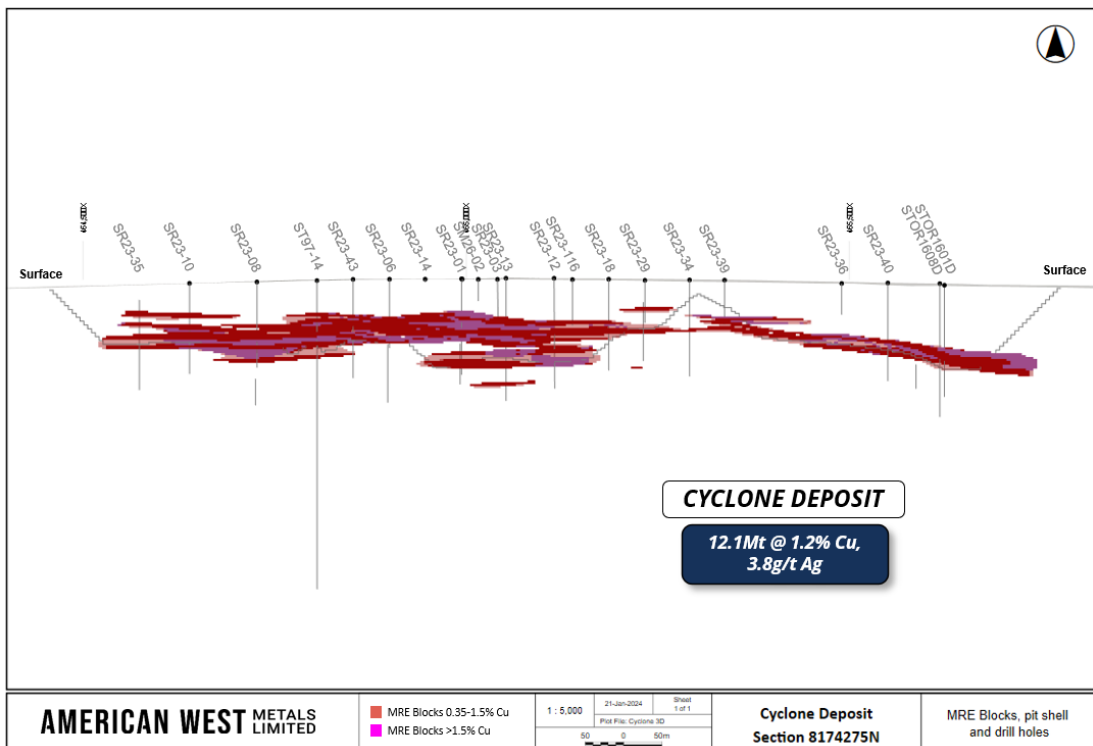


Figure 6: Long section view (looking north at 8174275N) of the Cyclone Deposit and conceptual pit shell.



**MRE – IMMEDIATE EXPANSION POTENTIAL**

The open mineralisation of the known Deposits, recent discoveries of high-grade copper mineralisation in the Storm area, and the largely untested 100km prospective copper horizon, highlight the outstanding potential for the discovery and definition of further resources within the Project area.

Four immediate opportunities have been defined for the expansion and addition of further resources at Storm, including the recently discovered high-grade Thunder and Lightning Ridge Zones, Cyclone North and The Gap Prospect.

**CYCLONE NORTH**

Exploration drilling to the north of the Cyclone Deposit (4100N Zone) during 2023 intersected a thick interval of copper sulphide. The drilling was designed to test a moderately conductive Fixed Loop Electromagnetic (FLEM) anomaly located to the north of Cyclone (Figure 7).

The 2021 FLEM survey highlighted two distinct, late time anomalies located approximately 200m and 500m respectively north of the known copper mineralisation at Cyclone. A single drill hole was designed to test the southern-most anomaly.

Drill hole SR23-55 intersected a 24.4m thick interval of breccia and vein copper sulphide mineralisation, which is interpreted to be hosted within the same prospective horizon as the Cyclone copper mineralisation. The mineralised zone contains a stronger sulphide breccia interval of 7.6m @ 1% Cu, which includes 1.5m @ 2% Cu. The >2% copper mineralisation is interpreted to be the source of the EM anomalism.

Significantly, the untested FLEM anomaly located over 300m to the north of drill hole SR23-55 has a higher conductivity and could represent larger volumes of >2% copper mineralisation. These two anomalies cover an area of approximately 16 hectares and have the potential to host significant volumes of additional resources.

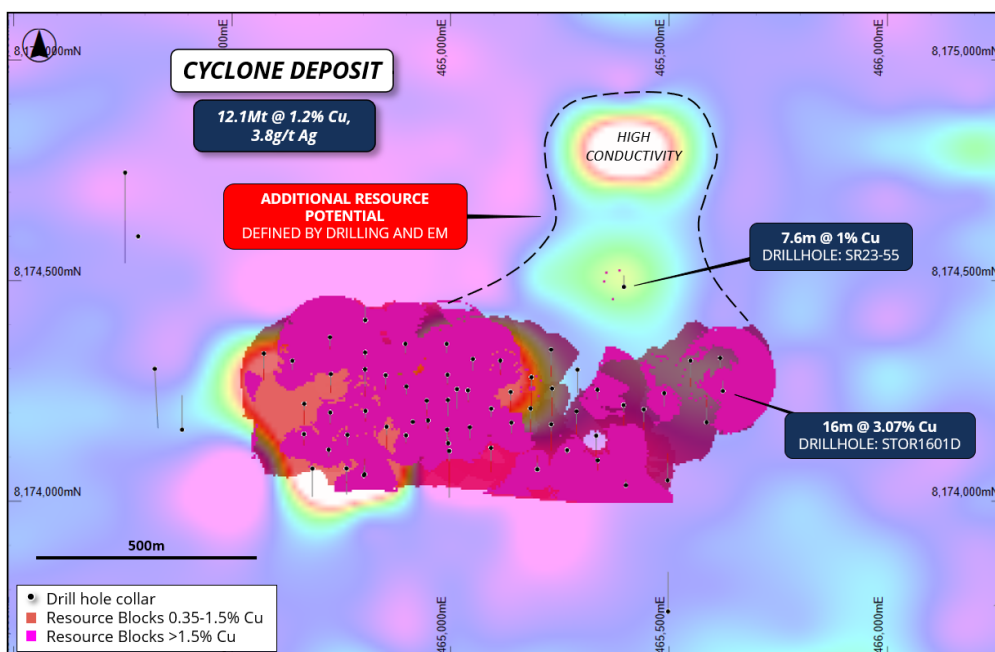


Figure 7: Plan view of the Cyclone Deposit showing the resource blocks and drilling, overlaying FLEM imagery (Late time conductivity – Channel 16. Hotter colours indicate higher conductivity).

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## THUNDER AND LIGHTNING RIDGE

Exploration drilling of high-priority EM anomalies and the large graben fault network during 2023 successfully expanded the footprint of the near-surface, high-grade copper mineralisation at Storm. This drilling resulted in the discovery of two exceptional copper discoveries at the Thunder and Lightning Ridge Prospects (ASX announcements dated 26 September 2023: *More High-Grade Copper Discoveries at Storm*, and 11 October 2023: *Emerging Camp-Scale Copper Opportunity at Storm*).

The Thunder Prospect is located approximately 1km to the west of the Chinook and Corona Copper Deposits (Figure 8). The discovery drill hole was designed to test a highly conductive Vertical Time Domain Electromagnetic (VTEM) and FLEM anomaly, and intersected a 48.6m thick interval of strong breccia and vein style copper sulphides grading 3% Cu, with broad zones of semi-massive to massive sulphide from 34.4m downhole. The massive sulphides are dominantly chalcocite, with lesser bornite and chalcopyrite and are interpreted to be fault related and the source of the strong EM anomalism.

Additionally, historical drilling in the vicinity of Thunder has intersected grades up to 20% Cu (0.75m @ 20.1% Cu from 102.45m downhole in ST00-66) and further highlights the potential for significant volumes of copper in the Thunder area.

The Lightning Ridge area is located to the south of the Chinook Copper Deposit and is characterised by a strong VTEM anomaly and an area of outcropping massive chalcocite on the slopes of a large E-W gully. Drilling successfully tested the VTEM target and resulted in the intersection of two main zones of high-grade copper mineralisation for a combined interval thickness of 30.4m (including 15.2m @ 2.3% Cu from 32m, and 15.2m @ 2.1% Cu from 77.7m downhole). The copper sulphide mineralisation consists of dense breccia and vein hosted chalcocite. Given its proximity to the gully and the style of mineralisation, it is strongly suggestive that the mineralisation is fault related and steeply dipping, as is seen at the nearby Chinook Copper Deposit.

The discoveries have continued to highlight the effectiveness of EM as a targeting tool at Storm, with a 100% correlation between EM anomalies and semi-massive/massive copper sulphides. Thunder and Lightning Ridge will become a focus for resource drilling during 2024, whilst further EM surveys will be employed to generate new targets for exploration drilling.

## THE GAP

The Gap Prospect is a 4km long zone located between the Corona and Cirrus Copper Deposits (Figure 8). The Prospect is centered on the large-scale, southern graben fault, and multiple drill holes in the area have intersected high-grade copper sulphides (including 1.5m @ 4.4% Cu, 9.8g/t Ag from 39m, and 2m @ 2.5% Cu from 74m downhole in AB18-09). The Thunder Prospect (described above) is located close to The Gap, and along a splay fault that is interpreted to be related to the southern graben fault.

The Gap area is characterised by broad zones of late time EM anomalism (VTEM and FLEM) and more localised, highly-conductive 'bullseye' style EM anomalies. A large and strong FLEM conductor at The Gap is interpreted to be flat lying, and approximately 900m x 600m in size. The EM anomalism, high-grade copper in drilling, and favourable geological setting, all indicate that The Gap Prospect is highly prospective for further copper discoveries.





**EXCEPTIONAL PIPELINE OF TARGETS**

Six significant, fault related copper deposits and prospects (Chinook, Corona, Cirrus, Thunder, Lightning Ridge, and The Gap) have now been identified in the southern graben area alone. All of these discoveries are located at, or close to surface, and have only been tested to a depth of approximately 100 vertical metres. Additionally, a number of EM anomalies in the southern graben area remain untested and have exceptional potential for the discovery of further high-grade copper mineralisation (Figure 8).

Exploration drilling during 2024 will look to expand the search space deeper and along strike within the vast fault network of the southern graben area, as well as test the existing high-priority EM targets in the area. Further EM surveys will be conducted during 2024 to extend the coverage outside of Storm and into the Blizzard and Tornado areas with the potential for discovery of additional targets, both in the near-surface and at depth.

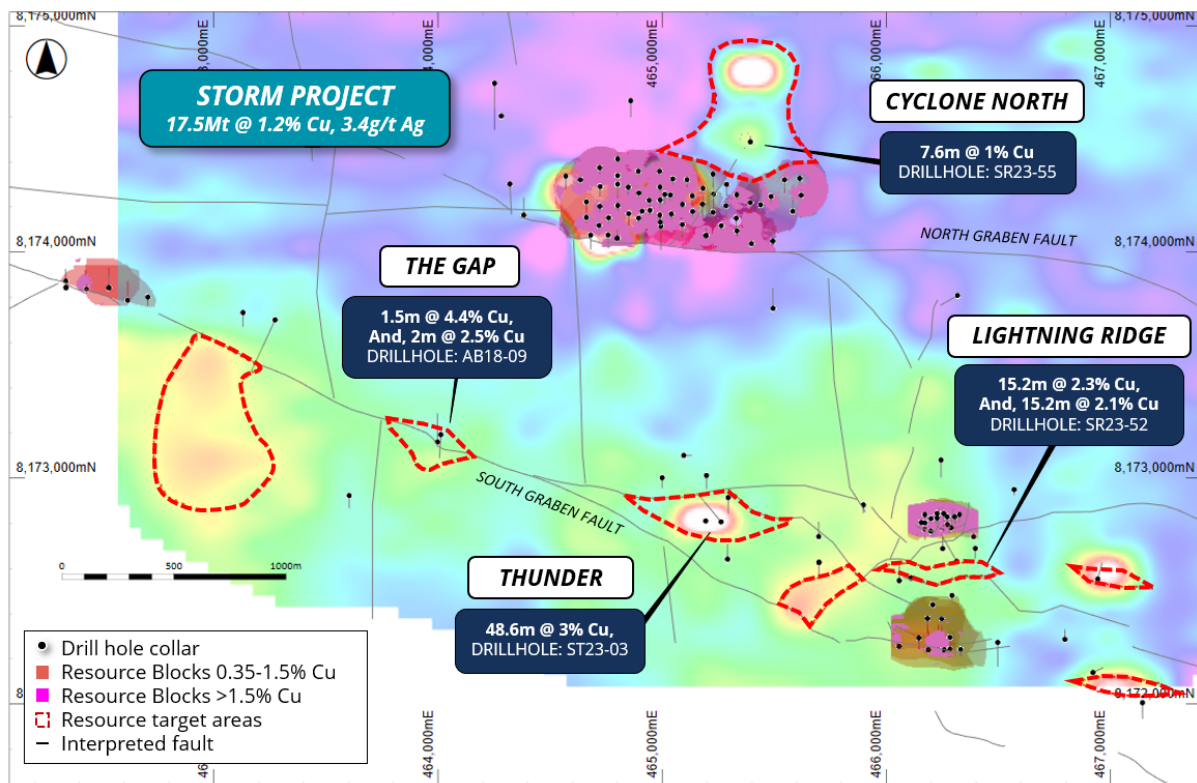


Figure 8: Plan view of Storm area showing the resource blocks of the known copper deposits, drilling, and major faults, overlaying FLEM geophysical imagery (Conductivity Ch16. Hotter colours and white indicate higher conductivity). Note the resource drilling target areas in red outline.



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This announcement has been approved for release by the Board of American West Metals Limited.

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**Forward looking statements**

Information included in this release constitutes forward-looking statements. Often, but not always, forward looking statements can generally be identified using forward-looking words such as “may,” “will,” “expect,” “intend,” “plan,” “estimate,” “anticipate,” “continue,” and “guidance,” or other similar words and may include, without limitation, statements regarding plans, strategies, and objectives of management.

Forward looking statements inherently involve known and unknown risks, uncertainties and other factors that may cause the Company’s actual results, performance, and achievements to differ materially from any future results, performance, or achievements. Relevant factors may include, but are not limited to, changes in commodity prices, foreign exchange fluctuations and general economic conditions, the speculative nature of exploration and project development, including the risks of obtaining necessary licenses and permits and diminishing quantities or grades of reserves, political and social risks, changes to the regulatory framework within which the Company operates or may in the future operate, environmental conditions including extreme weather conditions, recruitment and retention of personnel, industrial relations issues and litigation.

Forward looking statements are based on the Company and its management’s good faith assumptions relating to the financial, market, regulatory and other relevant environments that will exist and affect the Company’s business and operations in the future. The Company does not give any assurance that the assumptions on which forward looking statements are based will prove to be correct, or that the Company’s business or operations will not be affected in any material manner by these or other factors not foreseen or foreseeable by the Company or management or beyond the Company’s control.

Although the Company attempts and has attempted to identify factors that would cause actual actions, events, or results to differ materially from those disclosed in forward looking statements, there may be other factors that could cause actual results, performance, achievements, or events not to be as anticipated, estimated, or intended, and many events are beyond the reasonable control of the Company. Accordingly, readers are cautioned not to place undue reliance on forward looking statements. Forward looking statements in this announcement speak only at the date of issue. Subject to any continuing obligations under applicable law or any relevant stock exchange listing rules, in providing this information the Company does not undertake any obligation to publicly update or revise any of the forward-looking statements or to advise of any change in events, conditions or circumstances on which any such statement is based.



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### Competent Person's Statement

The information in this announcement that relates to the estimate of Mineral Resources for the Storm Project is based upon, and fairly represents, information and supporting documentation compiled and reviewed by Mr. Kevin Hon, P.Geo., Senior Geologist, Mr. Christopher Livingstone, P.Geo, Senior Geologist, Mr. Warren Black, P.Geo., Senior Geologist and Geostatistician, and Mr. Steve Nicholls, MAIG, Senior Resource Geologist, all employees of APEX Geoscience Ltd. and Competent Persons. Mr. Hon and Mr. Black are members of the Association of Professional Engineers and Geoscientists of Alberta (APEGA), Mr. Livingstone is a member of the Association of Professional Engineers and Geoscientist of British Columbia (EGBC), and Mr. Nicholls is a Member of the Australian Institute of Geologists (AIG).

Mr. Hon, Mr. Livingstone, Mr. Black, and Mr. Nicolls (the "APEX CPs") are Senior Consultants at APEX Geoscience Ltd., an independent consultancy engaged by American West Metals Limited for the Mineral Resource Estimate. The APEX CPs have sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". The APEX CPs consent to the inclusion in this announcement of matters based on his information in the form and context in which it appears.

All of the information in this announcement that relates to Exploration Results for the Storm Project is based on information compiled by Mr Dave O'Neill, a Competent Person who is a Member of The Australasian Institute of Mining and Metallurgy. Mr O'Neill is employed by American West Metals Limited as Managing Director, and is a substantial shareholder in the Company.

Mr O'Neill has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr O'Neill consents to the inclusion in this announcement of the matters based on his information in the form and context in which it appears.

### ASX Listing Rule 5.12

The Company has previously addressed the requirements of Listing Rule 5.12 in its Initial Public Offer prospectus dated 29 October 2021 (released to ASX on 9 December 2021) (Prospectus) in relation to the 2016 Foreign Seal MRE at the Storm Project. The Company is not in possession of any new information or data relating to the Seal Deposit that materially impacts on the reliability of the estimates or the Company's ability to verify the estimates as mineral resources or ore reserves in accordance with the JORC Code. The Company confirms that the supporting information provided in the Prospectus continues to apply and has not materially changed.

This ASX announcement contains information extracted from the following reports which are available on the Company's website at <https://www.americanwestmetals.com/site/content/>:

- 29 October 2021 Prospectus

The Company confirms that it is not aware of any new information or data that materially affects the exploration results included in the Prospectus. The Company confirms that the form and context in which the Competent Person's findings are presented have not been materially modified from the Prospectus.



## ABOUT AMERICAN WEST METALS

**AMERICAN WEST METALS LIMITED** (ASX: AW1) is an Australian clean energy mining company focused on growth through the discovery and development of major base metal mineral deposits in Tier 1 jurisdictions of North America. Our strategy is focused on developing mines that have a low-footprint and support the global energy transformation.

Our portfolio of copper and zinc projects in Utah and Canada include significant existing resource inventories and high-grade mineralisation that can generate robust mining proposals. Core to our approach is our commitment to the ethical extraction and processing of minerals and making a meaningful contribution to the communities where our projects are located.

Led by a highly experienced leadership team, our strategic initiatives lay the foundation for a sustainable business which aims to deliver high-multiplier returns on shareholder investment and economic benefits to all stakeholders.



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## Storm Mineral Resource Estimate – Supporting Information

### INTRODUCTION

The maiden JORC compliant Mineral Resource Estimation (MRE) for the Storm Copper Project (“Storm”, “Storm Copper” or the “Project”) was completed by APEX Geoscience Ltd. (“APEX”), an international geological consulting company, with geological modelling input from American West Metals Limited (“American West”).

The Storm Copper Project is located on northern Somerset Island, Nunavut in the Canadian Arctic Archipelago, within the Cornwallis Fold and Thrust Belt. The Project is part of the Aston Bay Property, which includes Storm Copper, the Seal Zinc Project, and numerous regional prospects and targets. The Aston Bay Property comprises 173 contiguous mineral claims covering a combined area of 219,256.7 hectares, and held 100% by Aston Bay Holdings Ltd. (“Aston Bay”).

On March 9, 2021, Aston Bay entered into an option agreement with American West Metals, and its wholly owned Canadian subsidiary Tornado Metals Ltd., pursuant to which American West was granted an option to earn an 80% undivided interest in the Project by spending a minimum of CAD\$10 million on qualifying exploration expenditures. The parties amended and restated the Option Agreement as of February 27, 2023 to facilitate American West potentially financing the expenditures through flow-through shares but did not change the commercial agreement between the parties. The expenditures were completed during 2023 and American West exercised the option. American West and Aston Bay will form an 80/20 unincorporated joint venture and enter into a joint venture agreement.

### GEOLOGY AND MINERALISATION

The Aston Bay Property, including the Storm Copper Project, lies within the Cornwallis Lead-Zinc District, which hosts the past producing Polaris Zn-Pb mine on Little Cornwallis Island. The Property covers a portion of the Cornwallis Fold and Thrust Belt, which affected sediments of the Arctic Platform deposited on a stable, passive continental margin that existed from Late Proterozoic to Late Silurian. Southward compression during the Ellesmerian Orogeny (Late Devonian to Early Carboniferous) produced a fold and thrust belt north and west of the former continental margin, effectively ending carbonate sedimentation throughout the region. This tectonic event is believed to have generated the ore-bearing fluids responsible for Zn-Pb deposits in the region.

Storm Copper is interpreted to be a sediment-hosted stratiform copper sulphide deposit, broadly comparable to Kupferschiefer and Kipushi type deposits. The Project comprises a collection of copper deposits (Cyclone, Chinook, Corona, and Cirrus) and other prospects and showings (including the Thunder and Lightning Ridge Zones, Cyclone North and Gap Prospects), surrounding a Central Graben. The Central Graben locally juxtaposes the conformable Late Ordovician to Early Silurian Allen Bay Formation, the Silurian Cape Storm Formation and the Silurian Douro Formation, and was likely a principal control on migration of mineralising fluids. The Storm Copper deposits are hosted within the upper 80 meters of the Allen Bay Formation and to a lesser extent in the basal Cape Storm Formation.



The Storm Copper sulphide mineralisation is most commonly hosted within structurally prepared ground, infilling fractures and a variety of breccias including crackle breccias, and lesser in-situ replacement and dissolution breccias, with a relatively impermeable “cap” of dolomicrite of the Silurian Cape Storm Formation.

Mineralisation at Storm Copper is dominated by chalcocite, with lesser chalcopyrite and bornite, and accessory cuprite, covellite, azurite, malachite, and native copper. Sulphides are hosted within porous, fossiliferous units and are typically disseminated, void-filling and net-textured as replacement of the host rock. Crackle, solution and fault breccias on the decametric to metric scale represent ground preparation at sites of copper deposition.

### **MINERAL RESOURCE ESTIMATION DATA**

The Maiden Storm Copper MRE was compiled using a database of a total of 115 surface diamond core and 56 surface reverse circulation (RC) drill holes (26,163 m of drilling for 1,756 samples), including data from 99 historical and modern diamond core drill holes (15,132 m) completed at the Aston Bay Property between 1995 and 2018 by previous operators Aston Bay Holdings Ltd., BHP Billiton, Cominco Ltd., and Noranda Inc. American West and Aston Bay completed drilling in 2022 and 2023 with 16 diamond core holes and 56 RC holes totaling 11,031 m. Of the 171 drillholes in the database, 103 intersected the mineralised estimation domains for 2,091 m. Unsampled material within the mineralised estimation domains accounts for 62 m (2%) of this material.

The historical (1997 to 2000) core was NQ or BQ diameter and modern (2016 to 2023) core was NQ2 diameter. The American West core was NQ2 diameter. All core was drilled using 3 metre rods. The RC drilling used a modern 3 ½ inch face sampling hammer with 5-foot rods, inner-tube assembly, and 3 ½ inch string diameter.

Appendix B lists the drill holes used in the MRE.

### **SAMPLING AND CORE RECOVERY**

Drill core samples ranged from 0.1 to 5.5 m in length, with average sample lengths of 1 to 1.5 m.

Exploration drilling at the Storm Copper Project (“Storm” or “Storm Copper”) in the 1990’s was conducted by Cominco Ltd. and Noranda Inc. In 1996 Cominco identified the Storm Copper mineralisation through prospecting and surficial sampling. Storm was first drilled with a single core hole in 1996. Subsequent core drilling programs were undertaken in 1997, 1999, and 2000. Not all aspects relating to the nature and quality of the historical drill sampling, including quality control and quality assurance (QAQC), can be confirmed; however, reports from re-logging of historical core by Aston Bay suggest that historical operators followed contemporary industry standard practices for half-core sampling. Samples were sent to at the Cominco Resource Laboratory in Vancouver, British Columbia, Canada, for analysis by ICP-AAS with 28-element return. Historical sample lengths ranged from 0.1 to 5.5 m in length and averaged 1.1 m. Holes were only sampled in areas of visible mineralisation.



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Modern core drilling was undertaken in 2016 by BHP Billiton and Aston Bay, in 2018 by Aston Bay, and in 2022 and 2023 by American West and Aston Bay. Modern diamond core sample intervals were based on visible copper sulphide mineralisation, structure, and geology, as identified by the logging geologist. Sample intervals were marked and recorded for cutting and sampling. Core samples consisted of half- or quarter-cut core submitted to ALS Minerals in North Vancouver, Canada for multi-element analysis by 4-acid digestion with ICP-MS and ICP-AES finish. Modern core sample lengths ranged from 0.3 to 3 m in length and averaged 1.4 m.

Modern RC drilling was undertaken in 2023 by American West and Aston Bay. RC holes were sampled in full on nominal 1.52 m intervals in conjunction with the 5-foot drill rod lengths. The assay samples were collected as 12.5% sub-sample splits from a riffle splitter used for homogenisation, and sent to ALS Minerals in North Vancouver, Canada for multi-element analysis by 4-acid digestion with ICP-MS and ICP-AES finish.

Modern core and RC sampling included a QAQC program comprising the insertion of certified reference materials (standards), blanks, and field duplicates. QAQC samples accounted for approximately 13% of total samples submitted.

Drill core logs in 1997 recorded diamond core recovery as a percentage per hole. Recovery was generally good (>95%). Drill core logs in 1999 and 2000 recorded diamond core recovery on three-metre intervals (a per-run basis), averaging 97% over the two programs. Modern diamond core recovery and rock quality designation (RQD) information was recorded by geological staff on three-metre intervals (a per-run basis) for the 2016, 2018, 2022, and 2023 programs. Recoveries were determined by measuring the length of core recovered in each three-metre run. Overall, the diamond core was competent, and recovery was very good, averaging 97%.

Sample recovery and condition was noted and recorded for all RC drilling. Recovery estimates were qualitative and based on the relative size of the returned sample. Due to pervasive and deep permafrost, virtually no wet samples were returned and preferential sampling of fine vs. coarse material is considered negligible.

## **GEOLOGICAL MODELLING**

The Storm Copper Project is interpreted to be a shallowly dipping sediment-hosted stratiform copper sulphide deposit. Shallow mineralisation associated with the Cyclone, Chinook, Corona, and Cirrus deposits is hosted within structurally prepared ground.

Geological models and estimation domains were used for the 2023 Storm Copper MRE and prepared by APEX Geoscience Ltd. with input from American West. Wireframe models were constructed in Micromine 2023.5 using the implicit modeler module and drilling data as input, with manual inputs as necessary. The geological model represents the geological interpretation of the Storm Copper Project backed by geological logs of drillholes. The primary data sources included the available drill hole data as well as surface geological mapping.



The estimation domains were constructed to honour the geological interpretation. Zones of mineralisation that were traced laterally through multiple drillholes defined the individual estimation domain wireframe shapes. Domains were constructed using the Micromine 2023.5 implicit modeler module, with manual inputs as necessary. A nominal visual cutoff of 0.3% copper was initially used to discriminate individual domains. The Project contains 22 estimation domains in the four deposit areas: Cyclone, Chinook, Corona, and Cirrus.

### MINERAL RESOURCE ESTIMATION

The 2023 Maiden Storm Copper MRE is reported in accordance with the Australian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves under JORC Code – 2012.

Relevant drilling data was composited to 1.5 m lengths prior to Mineral Resource Estimation for each individual domain. A balanced compositing approach was used which allowed composite lengths of +/- 40% in an effort to minimize orphans.

Composites within each domain were analyzed for extreme outliers and composite grade value was capped. Grade capping or top cutting restricts the influence of extreme values. Top-cut thresholds were determined using a combination of histograms, log probability and mean variance plots. Examination of the Cu and Ag populations per zone indicated some outlier samples exist. Capping was performed per zone to help limit overestimation. The Cyclone zone was capped at 11 % Cu and 28 g/t Ag leading to 3 copper and 7 silver composites being capped. The Chinook zone was capped at 10 % Cu and no capping for silver. Thirteen copper composites were capped. The Corona zone was capped at 9 % copper and no capping for silver leading to 2 copper composites being capped. The Cirrus zone was capped at 2% copper and 10 g/t silver leading to 6 copper and 1 silver composites being capped.

Variograms were modelled using estimation domain constrained composites, and the resulting parameters were used to estimate average block grades by the Ordinary Kriging (OK) method carried out by the python package Resource Modelling Solutions Platform (RMSP) version 1.10.2. Elements Cu (%) and Ag (g/t) were estimated separately using OK. The block model dimensions used are 5 m x 5 m x 2.5 m for the X, Y, and Z axes which is appropriate with the anticipated selective mining unit (SMU).

A dynamic search was used to more accurately represent the mineralisation trend at a given block location. A three-pass estimation was used with the maximum range determined by the variogram analysis. The maximum distance of extrapolation of data was 125 m away from the nearest drill hole. Volume-variance analysis was performed to ensure the model provided the expected tonnes and grade at a given cutoff which are calculated from declustered composites and the blank block model size.

There is a potential to obtain silver credits during extraction of copper. For this reason, silver was estimated separately from copper. There appears to be a low correlation between copper and silver from the samples in the current database. The estimation domains were constructed to capture the mineralised copper intervals while representing the geology. Silver was estimated inside the same estimation domains but separate from copper. Further geological and metallurgical testing is needed to better understand this relationship.





Estimation domains and block models were validated visually by APEX resource geologists and the CP upon completion.

### **BULK DENSITY**

The Storm density dataset comprises 256 samples from 18 different drill holes. Samples were measured on-site by weighing selected samples first in air, then submerged in water. The measurements were used to calculate the density ratio of the sample. Samples were grouped based on geological formation and the mean value was chosen as the appropriate density value. The block model was flagged with the geological formations and the corresponding density value was assigned. It was determined that a global bulk density of 2.79 g/cm<sup>3</sup> for all domains and formations was suitable at this stage.

### **MINERAL RESOURCE CLASSIFICATION**

The 2023 Maiden Storm Copper MRE has been classified as indicated and inferred based on geological confidence, drill hole spacing, sample density, data quality, and geostatistical analysis. The indicated classification category is defined for all blocks within an area of 75 m x 75 m x 10 m that contain a minimum of 3 drillholes. The inferred classification area is expanded to 125 m x 120 m x 10 m that contains a minimum of 2 drillholes.

Variogram models could not be obtained for the Corona, Chinook, and Cirrus deposits. As a result, these zones were capped at inferred classification only.

### **CUT-OFF GRADES**

The 2023 Maiden Storm Copper MRE is limited to material contained within the estimation domains and is reported above a copper cut-off grade of 0.35%. The Storm Copper MRE detailed herein is reported as undiluted and unconstrained by pit optimization. However, the reporting cut-off grade was based on assumptions regarding possible mining methods, metal prices, metal recoveries, mining costs, processing costs, and G&A costs. Open pit mining assumes a copper price of USD\$3.85 per pound (USD\$8,487.90/t) with 90% recovery of total copper. Cost assumptions were used to determine the reporting cut-off grade: open pit mining cost (USD\$5.00/t), processing (USD\$10.00/t), and G&A (USD\$12.00/t). Processing costs assume the use of ore sorting and jigging/dense medium separation techniques rather than traditional floatation. Cost assumptions were based on parameters used for comparable deposits.

The Storm Copper MRE is sensitive to the selection of a reporting cut-off value, as presented in the table below:



Deposit	Category	Cu Cutoff (%)	Ore Type	Tonnes	Cu (%)	Ag (g/t)	Cu (t)	Ag (Oz)
Cyclone (4100N Zone)	Indicated	0.2	Sulphide	5,270,000	1.19	3.32	62,700	562,800
		0.25	Sulphide	5,190,000	1.20	3.35	62,600	559,200
		0.3	Sulphide	5,090,000	1.22	3.38	62,300	553,400
		<b>0.35</b>	<b>Sulphide</b>	<b>4,880,000</b>	<b>1.26</b>	<b>3.45</b>	<b>61,600</b>	<b>541,100</b>
		0.4	Sulphide	4,690,000	1.30	3.51	60,900	528,200
		0.5	Sulphide	4,330,000	1.37	3.63	59,300	504,800
		0.6	Sulphide	4,000,000	1.44	3.76	57,400	483,700
		0.7	Sulphide	3,630,000	1.52	3.93	55,100	458,500
		0.8	Sulphide	3,250,000	1.61	4.07	52,200	425,400
		0.9	Sulphide	2,860,000	1.71	4.24	48,800	389,200
		1.0	Sulphide	2,500,000	1.82	4.45	45,500	357,200
	1.5	Sulphide	1,350,000	2.32	5.25	31,400	228,300	
	Inferred	0.2	Sulphide	7,930,000	1.12	3.81	88,800	971,900
		0.25	Sulphide	7,730,000	1.14	3.87	88,400	961,600
		0.3	Sulphide	7,520,000	1.17	3.93	87,800	950,900
		<b>0.35</b>	<b>Sulphide</b>	<b>7,210,000</b>	<b>1.20</b>	<b>4.03</b>	<b>86,800</b>	<b>934,700</b>
		0.4	Sulphide	6,930,000	1.24	4.13	85,700	919,700
		0.5	Sulphide	6,210,000	1.33	4.41	82,500	881,000
		0.6	Sulphide	5,440,000	1.44	4.74	78,200	829,300
		0.7	Sulphide	4,770,000	1.55	5.08	73,900	779,200
		0.8	Sulphide	4,250,000	1.65	5.36	70,000	733,600
		0.9	Sulphide	3,820,000	1.74	5.65	66,300	693,600
1.0		Sulphide	3,410,000	1.83	5.95	62,500	653,400	
1.5	Sulphide	1,780,000	2.38	7.56	42,200	431,700		
Chinook (2750N Zone)	Inferred	0.2	Sulphide	2,400,000	1.37	3.80	32,900	293,000
		0.25	Sulphide	2,340,000	1.40	3.85	32,800	290,400
		0.3	Sulphide	2,290,000	1.42	3.91	32,600	287,900
		<b>0.35</b>	<b>Sulphide</b>	<b>2,190,000</b>	<b>1.47</b>	<b>4.00</b>	<b>32,300</b>	<b>282,300</b>
		0.4	Sulphide	2,070,000	1.54	4.11	31,800	273,200
		0.5	Sulphide	1,910,000	1.63	4.31	31,100	263,700
		0.6	Sulphide	1,780,000	1.71	4.44	30,400	254,300
		0.7	Sulphide	1,640,000	1.80	4.57	29,500	240,700
		0.8	Sulphide	1,550,000	1.86	4.64	28,800	230,600
		0.9	Sulphide	1,460,000	1.93	4.73	28,000	221,500
		1.0	Sulphide	1,360,000	1.99	4.82	27,100	211,100
		1.5	Sulphide	880,000	2.40	4.88	21,200	138,600
	Inferred	0.2	Sulphide	2,070,000	0.77	1.38	15,900	91,600



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Deposit	Category	Cu Cutoff (%)	Ore Type	Tonnes	Cu (%)	Ag (g/t)	Cu (t)	Ag (Oz)
Corona (2200N Zone)		0.25	Sulphide	1,960,000	0.80	1.40	15,600	88,400
		0.3	Sulphide	1,810,000	0.84	1.43	15,200	83,400
		<b>0.35</b>	<b>Sulphide</b>	<b>1,640,000</b>	<b>0.89</b>	<b>1.48</b>	<b>14,700</b>	<b>77,700</b>
		0.4	Sulphide	1,450,000	0.96	1.54	14,000	71,700
		0.5	Sulphide	1,160,000	1.09	1.64	12,700	61,300
		0.6	Sulphide	930,000	1.22	1.73	11,400	51,700
		0.7	Sulphide	780,000	1.34	1.78	10,400	44,700
		0.8	Sulphide	650,000	1.46	1.85	9,400	38,600
		0.9	Sulphide	530,000	1.60	1.94	8,400	32,900
		1.0	Sulphide	370,000	1.87	2.16	6,900	25,600
		1.5	Sulphide	160,000	2.72	2.83	4,300	14,500
Cirrus (3500N Zone)	Inferred	0.2	Sulphide	1,860,000	0.57	1.28	10,500	76,300
		0.25	Sulphide	1,790,000	0.58	1.27	10,400	73,000
		0.3	Sulphide	1,700,000	0.60	1.29	10,100	70,500
		<b>0.35</b>	<b>Sulphide</b>	<b>1,550,000</b>	<b>0.62</b>	<b>1.29</b>	<b>9,700</b>	<b>64,400</b>
		0.4	Sulphide	1,460,000	0.64	1.29	9,300	60,500
		0.5	Sulphide	1,070,000	0.70	1.35	7,500	46,300
		0.6	Sulphide	690,000	0.79	1.35	5,500	30,200
		0.7	Sulphide	420,000	0.88	1.26	3,700	16,900
		0.8	Sulphide	250,000	0.97	1.16	2,500	9,500
		0.9	Sulphide	150,000	1.06	1.05	1,600	5,000
		1.0	Sulphide	80,000	1.15	0.99	900	2,600
		1.5	Sulphide	3,000	1.67	0.64	50	60
Global	Ind + Inf	0.2	Sulphide	19,520,000	1.08	3.18	210,900	1,995,500
		0.25	Sulphide	19,010,000	1.10	3.23	209,700	1,972,600
		0.3	Sulphide	18,410,000	1.13	3.29	208,000	1,946,100
		<b>0.35</b>	<b>Sulphide</b>	<b>17,480,000</b>	<b>1.17</b>	<b>3.38</b>	<b>205,000</b>	<b>1,900,200</b>
		0.4	Sulphide	16,590,000	1.22	3.47	201,700	1,853,500
		0.5	Sulphide	14,670,000	1.32	3.72	193,000	1,757,000
		0.6	Sulphide	12,850,000	1.42	3.99	183,000	1,649,200
		0.7	Sulphide	11,240,000	1.54	4.26	172,600	1,540,000
		0.8	Sulphide	9,950,000	1.64	4.49	162,900	1,437,700
		0.9	Sulphide	8,800,000	1.74	4.74	153,200	1,342,300
		1.0	Sulphide	7,720,000	1.85	5.03	142,900	1,249,900
				1.5	Sulphide	4,170,000	2.38	6.06



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Notes:

1. *The 2023 Maiden Storm Copper MRE is reported in accordance with the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (The Joint Ore Reserves Committee Code – JORC 2012 Edition).*
2. *The 2023 Maiden Storm Copper MRE was prepared and reviewed by Mr. Kevin Hon, P.Geo., Mr. Christopher Livingstone, P.Geo., Mr. Warren Black, P.Geo., and Mr. Steve Nicholls, MAIG, all Senior Consultants at APEX Geoscience Ltd. and Competent Persons.*
3. *Mineral resources which are not mineral reserves do not have demonstrated economic viability. No mineral reserves have been calculated for the Storm Project. There is no guarantee that any part of mineral resources discussed herein will be converted to a mineral reserve in the future.*
4. *The quantity and grade of the reported Inferred Resources are uncertain in nature and there has not been sufficient work to define these Inferred Resources as Indicated or Measured Resources. It is reasonably expected that most of the Inferred Mineral Resources could be upgraded to Indicated Mineral Resources with continued exploration.*
5. *All figures are rounded to reflect the relative accuracy of the estimates. Tonnes have been rounded to the nearest 10,000 and contained metals have been rounded to the nearest 100 copper tonnes or silver ounces. Totals may not sum due to rounding.*
6. *A global bulk density of 2.79 was used for the Storm Project MRE.*
7. *The 2023 Maiden Storm Copper MRE is limited to material contained within the estimation domains at a nominal 0.3% copper mineralised envelope and is reported at a lower cut-off grade of 0.35% copper. The Storm Copper MRE detailed herein is reported as undiluted and unconstrained by pit optimization. The reporting cut-off grade was based on assumptions regarding possible mining methods, metal prices, metal recoveries, mining costs, processing costs, and G&A costs.*
8. *Open pit mining assumes a copper price of USD\$3.85 per pound (USD\$8,487.90/t) with 90% recovery of total copper.*
9. *Costs are USD\$5/t for mining, USD\$10/t for processing, and USD\$12/t for G&A, leading to a cut-off grade of 0.35% copper.*

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**COST ASSUMPTIONS**

Given the shallow depth of mineralisation at the Storm Copper deposits the assumed mining method is open pit. A selective mining unit size of 5 m x 5 m x 2.5 m was chosen. Pit slopes were assumed to be 44 degrees. No geotechnical studies have been completed to date to support this assumption. A requirement for shallower pit slopes may result in a material change to the open pit resources.

Open pit mining assumes a copper price of USD\$3.85 per pound (USD\$8,487.90/t) with 90% recovery of total copper. Cost assumptions were used to determine the reporting cut-off grade: open pit mining cost (USD\$5.00/t), processing (USD\$10.00/t), and G&A (USD\$12.00/t). Processing costs assume the use of ore sorting and jigging/dense medium separation techniques rather than traditional floatation. Cost assumptions were based on parameters used for comparable deposits.



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## METALLURGY AND PROCESSING ASSUMPTIONS

The assumed processing method is by ore sorting and jigging/dense medium separation techniques rather than traditional flotation. Preliminary ore sorting work was completed during 2022 and 2023, indicating that the Storm mineralisation is highly amenable to ore sorting techniques.

Preliminary ore sorting test work was carried out at the STEINERT Australia Perth test facility in 2022. The test work was completed on a 5.5 kg of drill core sample sourced from remaining half core from 2016 hole STOR1601D, drilled at the Cyclone Deposit with an average grade of 4.16%. The sample was crushed and screened to a -25.0 +10.0 mm size fraction, removing fines (~0.03 kg). The 2022 test work was completed using a full-scale STEINERT KSS CLI XT combination sensor sorter. A combination of X-ray transmission, 3D laser, laser brightness, induction, and colour were used in the 2022 sorting algorithms. A substantial upgrade in Cu was achieved, with the concentrate fraction reporting a grade of 53.1% Cu in 10.2% of the mass yield, from an initial calculated feed grade of 6.52% Cu and a Cu recovery of 83.4%. If combined with the middling fraction, a 32.17% Cu product is produced in 19.76% of the mass yield, with a total Cu recovery of 96.5%. Given the small sample size, additional test work was recommended.

Additional ore sorting test work was carried out at the STEINERT Australia Perth test facility in 2023. The test work was completed on two composite samples sourced from 2022 holes drilled at the Chinook Deposit. Composite 1 had a feed mass of 66.46 kg and a head grade of 2.72% Cu. Composite 2 had a feed mass of 87.78 kg and a head grade of 0.70% Cu. The samples were crushed and screened to a -25.0 +10.0 mm size fraction, removing fines (~48.92 kg total). The 2023 test work was completed using a full-scale STEINERT KSS CLI XT combination sensor sorter. A combination of X-ray transmission and induction were used in the 2023 sorting algorithms, to avoid the need to wash the feed material for 3D laser, as a consideration for the Arctic climate. Three passes were completed, producing three concentrates for each composite (Con 1, Con 2, Con 3). Both samples were amenable to ore sorting, with Con 1 fractions alone producing grades of 14.88% Cu and 13.15% in mass yields of 11.1% and 1.8% for Composites 1 and 2, respectively. Utilizing all three passes, Cu recoveries of 94.7% and 84.2% were achieved in mass yields of 34.7% and 16.6%.

Preliminary floatation testing of the concentrates produced from the 2023 ore sorting work showed that the Storm material is highly amenable to flotation, with strong upgrade potential.

The test work completed to date is preliminary and may not be representative of the expected grades and recoveries that could be achieved through additional ore sorting and traditional metallurgical processes. American West is currently undertaking additional ore sorting, dry and wet jigging (closed circuit), dense material separation, and flotation test work. The results from these tests will be used in future MRE updates.



## Mineral Resource Estimate – Drill Hole Information

The table below lists all drill holes completed at the Storm Copper Project to date. Those holes with **bolded** IDs do not intersect the MRE.

Hole ID	Prospect	Easting (m)	Northing (m)	RL (m)	Total Depth (m)	Azimuth	Dip	Type
<b>AB18-02</b>	Exploration	462,932	8,175,741	256	167.0	180	-80	Core
<b>AB18-02B</b>	Exploration	462,932	8,175,741	256	185.0	180	-85	Core
<b>AB18-02C</b>	Exploration	462,932	8,175,741	256	157.9	180	-85	Core
<b>AB18-04</b>	Exploration	459,521	8,176,877	201	473.0	179	-80	Core
<b>AB18-05</b>	Exploration	462,699	8,175,133	268	321.9	180	-80	Core
<b>AB18-09</b>	The Gap	464,016	8,173,190	239	199.9	183	-58	Core
SM23-01	Chinook	466,203	8,172,819	250	101.0	180	-50	Core
SM23-02	Cyclone	465,016	8,174,253	301	152.0	180	-45	Core
SM23-03	Cyclone	464,949	8,174,182	300	95.0	180	-75	Core
SR23-01	Cyclone	464,994	8,174,286	301	137.2	180	-65	RC
SR23-02	Cyclone	464,993	8,174,161	299	140.2	180	-59	RC
SR23-03	Cyclone	465,041	8,174,251	301	150.9	178	-65	RC
SR23-04	Cyclone	465,045	8,174,167	299	152.4	179	-60	RC
SR23-05	Cyclone	464,899	8,174,148	298	131.1	180	-66	RC
SR23-06	Cyclone	464,900	8,174,259	301	166.1	180	-69	RC
SR23-07	Cyclone	464,806	8,174,204	299	137.2	180	-71	RC
SR23-08	Cyclone	464,727	8,174,287	297	118.9	180	-69	RC
SR23-09	Cyclone	464,726	8,174,200	298	164.6	180	-69	RC
SR23-10	Cyclone	464,639	8,174,318	295	125.0	180	-70	RC
SR23-11	Cyclone	464,666	8,174,220	296	140.2	180	-70	RC
SR23-12	Cyclone	465,115	8,174,318	302	149.4	179	-73	RC
SR23-13	Cyclone	465,052	8,174,322	302	175.3	180	-65	RC
SR23-14	Cyclone	464,946	8,174,227	301	160.0	180	-65	RC
SR23-15	Cyclone	464,855	8,174,168	299	121.9	180	-65	RC
SR23-16	Cyclone	465,139	8,174,247	300	132.6	180	-70	RC
SR23-17	Cyclone	465,140	8,174,177	299	129.5	180	-66	RC
SR23-18	Cyclone	465,186	8,174,280	301	182.9	180	-65	RC
SR23-19	Chinook	466,176	8,172,771	245	70.1	180	-55	RC
SR23-20	Chinook	466,231	8,172,821	251	97.5	196	-45	RC
SR23-21	Chinook	466,277	8,172,792	249	59.4	180	-55	RC
SR23-22	Chinook	466,230	8,172,820	251	114.3	150	-72	RC
SR23-23	Chinook	466,276	8,172,791	249	79.2	90	-78	RC



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Hole ID	Prospect	Easting (m)	Northing (m)	RL (m)	Total Depth (m)	Azimuth	Dip	Type
SR23-24	Corona	466,188	8,172,376	240	132.6	180	-61	RC
SR23-25	Corona	466,289	8,172,241	232	70.1	181	-61	RC
SR23-26	Corona	466,289	8,172,293	238	94.5	180	-60	RC
SR23-27	Corona	466,150	8,172,291	233	100.6	180	-60	RC
SR23-28	Cyclone	465,184	8,174,210	299	149.4	180	-65	RC
SR23-29	Cyclone	465,233	8,174,255	299	132.6	180	-62	RC
SR23-30	Cyclone	465,231	8,174,174	297	120.4	180	-60	RC
SR23-31	Cyclone	465,268	8,174,115	296	125.0	182	-61	RC
<b>SR23-32</b>	Cyclone	465,334	8,174,148	295	179.8	180	-65	RC
SR23-33	Cyclone	465,289	8,174,203	297	125.0	180	-65	RC
<b>SR23-34</b>	Cyclone	465,291	8,174,297	300	135.6	180	-67	RC
SR23-35	Cyclone	464,574	8,174,334	294	149.4	180	-66	RC
SR23-36	Cyclone	465,490	8,174,244	295	129.5	180	-65	RC
SR23-37	Cyclone	465,443	8,174,207	295	125.0	180	-65	RC
SR23-38	Cyclone	465,338	8,174,092	295	125.0	180	-65	RC
SR23-39	Cyclone	465,337	8,174,252	300	125.0	180	-65	RC
SR23-40	Cyclone	465,550	8,174,318	296	140.2	180	-65	RC
SR23-41	Cyclone	464,763	8,174,073	296	140.2	180	-65	RC
SR23-42	Cyclone	464,898	8,174,356	301	170.7	180	-70	RC
SR23-43	Cyclone	464,852	8,174,285	301	182.9	180	-65	RC
<b>SR23-44</b>	Cyclone	464,685	8,174,073	296	152.4	180	-65	RC
SR23-45	Cyclone	464,765	8,174,150	297	150.9	180	-65	RC
SR23-46	Cyclone	465,093	8,174,120	297	131.1	180	-65	RC
<b>SR23-47</b>	Cyclone North	464,863	8,174,668	307	170.7	180	-65	RC
SR23-48	Corona	466,191	8,172,237	227	120.4	0	-45	RC
SR23-49	Corona	466,192	8,172,237	227	120.4	0	-70	RC
SR23-50	Corona	466,263	8,172,237	230	120.4	0	-50	RC
SR23-51	Corona	466,263	8,172,237	230	120.4	0	-70	RC
<b>SR23-52</b>	Lightning Ridge	466,062	8,172,544	230	118.9	0	-45	RC
<b>SR23-53</b>	Exploration	466,927	8,172,137	227	100.6	65	-60	RC
SR23-54	Cyclone	465,587	8,174,178	292	146.3	0	-65	RC
SR23-55	Cyclone North	465,398	8,174,485	303	150.9	0	-80	RC
SR23-56	Cyclone	464,665	8,174,151	296	121.9	180	-65	RC
ST00-60	Cyclone	464,915	8,174,179	299	160.9	0	-90	Core
ST00-61	Cyclone	464,722	8,174,116	296	128.0	180	-70	Core
ST00-62	Cyclone	464,725	8,174,371	298	170.4	180	-70	Core
ST00-63	Cyclone	464,992	8,174,356	302	146.0	180	-70	Core



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Hole ID	Prospect	Easting (m)	Northing (m)	RL (m)	Total Depth (m)	Azimuth	Dip	Type
ST00-64	Cyclone	465,094	8,174,209	300	160.9	180	-70	Core
ST00-65	Cyclone	465,397	8,174,217	296	227.1	180	-70	Core
<b>ST00-66</b>	Thunder	465,198	8,172,808	243	149.0	0	-90	Core
<b>ST00-67</b>	Thunder	465,100	8,173,098	259	206.0	90	-80	Core
ST22-01	Chinook	466,231	8,172,841	252	128.0	180	-50	Core
ST22-02	Chinook	466,202	8,172,763	245	155.1	0	-66	Core
ST22-03	Chinook	466,294	8,172,778	248	118.9	359	-69	Core
ST22-04	Chinook	466,276	8,172,827	253	146.0	182	-60	Core
ST22-05	Chinook	466,276	8,172,827	253	89.0	180	-46	Core
ST22-06	Chinook	466,176	8,172,836	249	152.1	181	-51	Core
ST22-07	Chinook	466,160	8,172,802	244	100.9	197	-50	Core
ST22-08	Chinook	466,331	8,172,836	254	107.0	182	-50	Core
<b>ST22-09</b>	Exploration	466,948	8,172,551	258	155.1	15	-61	Core
<b>ST22-10</b>	Cyclone	464,324	8,174,299	287	382.6	177	-69	Core
ST23-01	Cyclone	464,805	8,174,337	300	416.0	180	-75	Core
<b>ST23-02</b>	Cyclone	464,256	8,174,745	298	602.0	180	-70	Core
<b>ST23-03</b>	Thunder	465,267	8,172,804	244	395.0	320	-65	Core
<b>ST23-04</b>	Exploration	463,276	8,173,698	231	476.0	205	-60	Core
<b>ST96-01</b>	Chinook	466,318	8,172,629	252	328.9	330	-55	Core
ST97-02	Corona	466,236	8,172,237	229	103.9	0	-90	Core
ST97-03	Corona	466,236	8,172,237	229	174.3	0	-50	Core
ST97-04	Corona	466,061	8,172,254	224	110.0	0	-90	Core
ST97-05	Corona	466,061	8,172,254	224	188.1	335	-50	Core
<b>ST97-06</b>	Lightning Ridge	466,115	8,172,556	234	38.1	285	-55	Core
<b>ST97-07</b>	Lightning Ridge	466,115	8,172,556	234	173.1	285	-70	Core
ST97-08	Chinook	466,255	8,172,776	247	217.9	0	-60	Core
ST97-09	Chinook	466,261	8,172,841	253	150.9	180	-53	Core
ST97-10	Chinook	466,258	8,172,842	253	163.1	180	-80	Core
ST97-11	Corona	466,252	8,172,376	238	196.9	180	-50	Core
<b>ST97-12</b>	Exploration	465,499	8,173,749	285	263.0	0	-70	Core
ST97-13	Cyclone	464,995	8,174,229	301	190.5	180	-50	Core
ST97-14	Cyclone	464,805	8,174,298	299	192.9	180	-50	Core
<b>ST97-15</b>	The Gap	464,001	8,173,158	238	196.9	0	-50	Core
<b>ST97-16</b>	Exploration	463,607	8,172,921	230	113.1	180	-60	Core
ST97-17	Corona	466,501	8,172,271	236	167.9	180	-50	Core
<b>ST97-18</b>	Exploration	467,148	8,172,004	175	143.9	180	-60	Core
ST99-19	Chinook	466,177	8,172,799	247	116.1	180	-50	Core



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Hole ID	Prospect	Easting (m)	Northing (m)	RL (m)	Total Depth (m)	Azimuth	Dip	Type
ST99-20	Chinook	466,402	8,172,686	254	71.0	180	-50	Core
ST99-21	Corona	466,212	8,172,437	242	109.1	180	-80	Core
ST99-22	Chinook	466,309	8,172,827	253	100.9	180	-45	Core
ST99-23	Corona	466,336	8,172,239	234	60.0	180	-60	Core
ST99-24	Exploration	466,249	8,173,078	255	182.9	180	-65	Core
ST99-25	Corona	466,297	8,172,479	249	75.6	180	-65	Core
ST99-26	Exploration	466,801	8,172,284	239	128.0	0	-70	Core
ST99-27	Exploration	465,703	8,172,739	244	131.1	0	-60	Core
ST99-28	Cirrus	462,343	8,173,841	212	81.4	0	-65	Core
ST99-29	Exploration	465,704	8,172,625	236	89.0	180	-50	Core
ST99-30	Cirrus	462,343	8,173,841	212	31.1	0	-45	Core
ST99-31	Cirrus	462,534	8,173,840	215	125.9	0	-45	Core
ST99-32	Exploration	465,704	8,172,625	236	157.9	180	-65	Core
ST99-33	Cirrus	462,534	8,173,840	215	118.0	0	-75	Core
ST99-34	Thunder	465,299	8,172,912	253	143.0	180	-60	Core
ST99-35	Thunder	465,004	8,172,999	255	107.0	180	-65	Core
ST99-36	Cirrus	462,342	8,173,870	214	82.9	0	-50	Core
ST99-37	Thunder	465,201	8,173,009	255	143.0	180	-65	Core
ST99-38	Cirrus	462,708	8,173,798	219	146.0	180	-75	Core
ST99-39	Thunder	465,296	8,172,639	245	157.9	0	-65	Core
ST99-40	Exploration	465,902	8,172,879	247	28.3	180	-50	Core
ST99-41	Cirrus	462,619	8,173,784	215	131.1	0	-50	Core
ST99-42	Exploration	465,902	8,172,876	247	79.9	180	-65	Core
ST99-43	Cirrus	462,435	8,173,833	213	125.0	0	-50	Core
ST99-44	Chinook	466,256	8,172,686	243	77.1	0	-50	Core
ST99-45	Exploration	462,403	8,175,704	242	157.9	180	-60	Core
ST99-46	Chinook	466,394	8,172,739	249	125.0	0	-50	Core
ST99-47	Cyclone	464,996	8,174,130	298	139.9	0	-70	Core
ST99-48	Exploration	462,801	8,175,487	263	146.0	180	-80	Core
ST99-49	Cyclone	465,200	8,174,071	295	98.1	0	-90	Core
ST99-50	Exploration	460,374	8,175,168	211	128.0	180	-80	Core
ST99-51	Cyclone	465,200	8,174,071	295	50.0	0	-50	Core
ST99-52	Exploration	463,786	8,174,647	275	116.1	180	-70	Core
ST99-53	Cyclone	465,402	8,174,035	293	143.0	0	-55	Core
ST99-54	Cyclone	464,803	8,174,058	296	100.9	0	-65	Core
ST99-55	Cyclone	464,386	8,174,161	289	121.9	0	-50	Core
ST99-56	Cyclone	464,804	8,174,060	296	125.0	0	-45	Core

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Hole ID	Prospect	Easting (m)	Northing (m)	RL (m)	Total Depth (m)	Azimuth	Dip	Type
<b>ST99-57</b>	Cyclone	464,806	8,174,410	300	50.0	0	-50	Core
ST99-58	Cyclone	464,998	8,174,113	297	185.0	180	-55	Core
ST99-59	Cyclone	465,498	8,174,046	291	107.0	0	-55	Core
STOR1601D	Cyclone	465,624	8,174,249	293	149.7	0	-75	Core
STOR1602D	Cyclone	465,231	8,174,343	302	123.4	180	-60	Core
<b>STOR1603D</b>	Exploration	466,322	8,173,806	272	179.0	240	-60	Core
<b>STOR1604D</b>	Cyclone	464,286	8,174,600	293	122.0	180	-90	Core
STOR1608D	Cyclone	465,618	8,174,324	295	178.9	180	-75	Core
<b>STOR1609D</b>	Exploration	463,133	8,173,730	230	125.0	180	-60	Core
<b>STOR1612D</b>	Chinook	466,575	8,172,947	264	147.0	180	-80	Core



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# American West Metals Ltd. – 2023 Maiden Storm Copper MRE

## JORC Code, 2012 Edition – Table 1

### Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> <li>• Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</li> <li>• Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</li> <li>• Aspects of the determination of mineralisation that are Material to the Public Report.</li> <li>• In cases where ‘industry standard’ work has been done this would be relatively simple (eg ‘reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay’). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</li> </ul>	<ul style="list-style-type: none"> <li>• Drilling included in the current reported 2023 Maiden Storm Copper MRE (“Storm Copper MRE”) includes historical diamond core drilling (1997, 1999 and 2000), and modern diamond core and reverse circulation (RC) drilling and sampling (2012-2023).</li> <li>• Exploration drilling at the Storm Copper Project (“Storm” or “Storm Copper”) in the 1990’s was conducted by Cominco Ltd. and Noranda Inc. In 1996 Cominco identified the Storm Copper mineralisation through prospecting and surficial sampling. Storm was first drilled with a single core hole in 1996. Subsequent programs were undertaken in 1997, 1999, and 2000.</li> <li>• Geophysical surveys, surficial sampling, and further drilling through to 2001 identified four prospects at Storm Copper, known as the 4100N, 2750N, 2200N, and 3500N zones (now known as Cyclone, Chinook, Corona, and Cirrus deposits, respectively).</li> <li>• Historical diamond sampling consisted of half-cut core submitted to Cominco Resource Laboratory in Vancouver, Canada for multi-element ICP analysis.</li> <li>• Not all aspects relating to the nature and quality of the historical drill sampling can be confirmed. Available details pertaining to historical exploration methods are outlined in the appropriate sections below.</li> <li>• Modern exploration at the Storm Copper Project was re-ignited with drill core resampling programs in 2008, 2012 and 2013 by Commander Resources Ltd. (“Commander”) and Aston Bay Holdings Ltd. (“Aston Bay”). Drilling was undertaken in 2016 by BHP Billiton and Aston Bay, in 2018 by Aston Bay, and in 2022 and 2023 by American West Metals Ltd. (“American West Metals” or “American West”) and Aston Bay.</li> <li>• Modern diamond core sample intervals were based on visible copper sulphide mineralisation, structure, and geology, as identified by the logging</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>geologist. Sample intervals were marked and recorded for cutting and sampling. Core samples consisted of half- or quarter-cut core submitted to ALS Minerals in North Vancouver, Canada for multi-element ICP analysis.</p> <ul style="list-style-type: none"> <li>• Modern RC drill holes were sampled in their entirety. RC samples were collected from a riffle splitter in 1.52 m (5-foot) intervals and sent to ALS Minerals for multi-element ICP analysis.</li> </ul>
<p><i>Drilling techniques</i></p>	<ul style="list-style-type: none"> <li>• <i>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</i></li> </ul>	<ul style="list-style-type: none"> <li>• Historical diamond drilling was conducted using a Cominco Ltd. owned, heli-portable Boyles 25A rig with standard NQ diameter core tubing, or a Boyles 18A rig with standard BQ diameter core tubing. Drill core was not oriented.</li> <li>• Modern diamond drilling was conducted with heli-portable rigs. The 2016 program was completed by Geotech Drilling Services Ltd. using a Hydracore 2000 rig with standard NQ diameter core tubing. The 2018, 2022, and 2023 programs were completed by Top Rank Diamond Drilling Ltd. using an Aston Bay owned Zinex A5 rig with standard NQ2 diameter core tubing (2018, 2022), and a Top Rank Discovery II rig with standard NQ2 diameter core tubing (2018, 2022, 2023). The modern drill core was not oriented.</li> <li>• Modern RC drilling was completed by Northspan Explorations Ltd. with a heli-portable Multi-Power Products “Super Hornet” RC rig utilizing two external compressors, each providing 300 cfm/200 psi air. The rig used a modern 3 ½ inch face sampling hammer with 5-foot rod lengths, inner-tube assembly, and 3 ½ inch string diameter.</li> </ul>
<p><i>Drill sample recovery</i></p>	<ul style="list-style-type: none"> <li>• <i>Method of recording and assessing core and chip sample recoveries and results assessed.</i></li> <li>• <i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i></li> <li>• <i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Drill core logs in 1997 recorded diamond core recovery as a percentage per hole. Recovery was generally good (&gt;95%).</li> <li>• Drill core logs in 1999 and 2000 recorded diamond core recovery on three-metre intervals (a per-run basis), averaging 97% over the two programs.</li> <li>• Modern diamond core recovery and rock quality designation (RQD) information was recorded by geological staff on three-metre intervals (a per-run basis) for the 2016, 2018, 2022, and 2023 programs. Recoveries were determined by measuring the length of core recovered in each three-metre run. Overall, the diamond core was competent, and recovery was very good, averaging 97%.</li> <li>• Sample recovery and sample condition was noted and recorded for all RC drilling. Recovery estimates were qualitative and based on the relative size of the returned sample. Due to pervasive and deep permafrost, virtually no wet samples were returned and preferential sampling of fine vs. coarse material is considered negligible.</li> </ul>

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Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>No relationship has been identified between sample recovery and grade in modern drilling and no sample bias is believed to exist. Good recoveries are generally maintained in areas of high-grade mineralisation.</li> </ul>
Logging	<ul style="list-style-type: none"> <li>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> <li>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</li> <li>The total length and percentage of the relevant intersections logged.</li> </ul>	<ul style="list-style-type: none"> <li>Historical and modern logging was both qualitative and quantitative, and all holes were logged in full.</li> <li>Historical core logging comprised detailed geological descriptions including geological formation, lithology, texture, structure, and mineralisation. This data was transcribed and standardized to conform with modern logging codes for import into the Storm Copper geological database.</li> <li>During the 2012-2013 resampling programs, select drillholes were re-logged with reference to the historical drilling records to establish continuity and conformity of geological assignment.</li> <li>Modern diamond core logging was completed on-site and in detail for lithology, oxidation, texture, structure, mineralisation, and geotechnical data.</li> <li>Modern RC holes were logged on a 5-foot basis (1.52 m) for lithology, oxidation, texture, structure and mineralisation.</li> <li>All modern drillholes were logged in full by geologists from BHP Billiton, Aston Bay, or APEX Geoscience Ltd. ("APEX"), an independent geological consultancy.</li> <li>High resolution wet and dry core and RC chip photos are available for all modern drillholes in full. Lower resolution core photos are available for some historical holes.</li> </ul>
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> <li>If core, whether cut or sawn and whether quarter, half or all core taken.</li> <li>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</li> <li>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> <li>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</li> <li>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</li> <li>Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul>	<ul style="list-style-type: none"> <li>Details relating to sampling techniques employed by historical explorers, including quality control procedures, have not been preserved. It has been noted from examination of the historical core that half-core samples were taken. Samples were between 0.1 and 5.5 m in length and averaged 1.1 m. Holes were only sampled in areas of visible mineralisation.</li> <li>The 2012-2013 resampling program included samples 0.5-2.8 m in length (average 1.4 m) and included the insertion of QAQC samples such as standards and blanks. Where core was re-sampled from the historical assay intervals, quarter core was taken from the remaining half core. Where new samples were taken, half core was sampled.</li> <li>Modern core drilling samples were 0.3 to 3 m in length (average 1.4 m) and included the insertion of QAQC samples (~13%) including certified reference materials (standards), blanks, and field duplicates. Half core was sampled</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>for most laboratory analyses, with quarter core used for duplicate samples. Quarter core was sampled for laboratory analysis in holes designated for metallurgical testing. The remaining three-quarter core was set aside for metallurgical testing. Drill core sample intervals were selected based on geological and/or mineralogical boundaries. Holes were sampled in areas of visible mineralisation, with modest shoulder samples above, below, and between mineralised zones.</p> <ul style="list-style-type: none"> <li>• RC holes were sampled in full on nominal 1.52 m intervals in conjunction with the 5-foot drill rod lengths. The assay samples were collected as 12.5% sub-sample splits from a riffle splitter used for homogenisation. QAQC samples (~13%) were inserted using the same procedures as the modern core drilling.</li> <li>• Sample sizes are considered to be appropriate to correctly represent base metal sulphide mineralisation and associated geology based on the style and consistency of mineralisation, and sampling method.</li> </ul>
<p><i>Quality of assay data and laboratory tests</i></p>	<ul style="list-style-type: none"> <li>• <i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i></li> <li>• <i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i></li> <li>• <i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Historical core assays (1997 to 2000) were conducted at the Cominco Resource Laboratory in Vancouver, British Columbia, Canada. The samples were analysed by ICP-AAS with 28-element return. QAQC procedures including the use of blank, standard, or duplicate samples were either not used or not available and have not been subsequently located.</li> <li>• Modern core (2016 to 2023) and RC (2023) analyses were conducted by ALS Geochemistry, an independent, accredited analytical laboratory. Most of the sample preparation was completed at the ALS laboratory in Yellowknife, Northwest Territories, Canada, and the analytical procedures were completed at the ALS laboratory in North Vancouver, British Columbia, Canada.</li> <li>• Modern core and RC samples were weighted, dried and crushed to &gt;70% passing 2 mm mesh, followed by a split pulverized to 85% passing 75 µm mesh. The samples were sent to ALS for multi-element analysis by 4-acid digestion with ICP-MS and ICP-AES finish. Samples with values for elements of interest (Cu or Zn) exceeding the upper detection limits of the applied method were further analyzed by ore-grade acid digestion and ICP-AES, as needed.</li> <li>• In addition to the field QAQC procedures described above, ALS Geochemistry inserts their own standards and blanks at set intervals and monitor the precision of the analyses.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>The assay method and laboratory procedures are within industry standards and are considered appropriate for the commodities of interest and style of mineralisation. The four-acid ICP techniques are designed to report precise elemental returns.</li> </ul>
Verification of sampling and assaying	<ul style="list-style-type: none"> <li>The verification of significant intersections by either independent or alternative company personnel.</li> <li>The use of twinned holes.</li> <li>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</li> <li>Discuss any adjustment to assay data.</li> </ul>	<ul style="list-style-type: none"> <li>Significant intersections are verified by the Company's technical staff and a suitably qualified Competent Person.</li> <li>Drill hole logs are inspected to verify the correlation of mineralised zones between assay results and pertinent lithology/alteration/mineralisation.</li> <li>Drillhole data is logged into locked Excel logging templates and imported into the Storm Copper Project database for validation.</li> <li>No twin holes were used, however, resampling of select historical holes was conducted in 2008 by Commander Resources Ltd. Six samples from five holes at Storm Copper were re-analysed, showing good agreement with copper results from the original analyses. The 2008 Commander results were not substituted for the historical results in the current MRE.</li> <li>Further resampling was conducted in 2012 and 2013 to confirm the historical reported mineralisation and fill sampling gaps in select holes. The resampled intervals were not directly replicated with certainty as there were no sample markers on the core; however, the 2012 results (grade over width) were found to be comparable to the reported historical data. In addition to re-sampling of mineralised core, previously unsampled core was sampled over select intervals to fill sampling gaps between mineralised zones, and in some cases as shoulder samples. The 2012 re-assay results were used in some places instead of historical results because of irregular gaps in the historical sampling sequences. Several of these intervals were included in the Storm Copper Project database used in the MRE.</li> <li>No adjustments were made to the historical assay data, other than described above with respect to the re-assay program.</li> </ul>
Location of data points	<ul style="list-style-type: none"> <li>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</li> <li>Specification of the grid system used.</li> <li>Quality and adequacy of topographic control.</li> </ul>	<ul style="list-style-type: none"> <li>Historical drill collars were recorded via handheld GPS in Universal Transverse Mercator ("UTM") coordinates referenced to NAD83 Zone 15N.</li> <li>No downhole survey data is available for the historical drilling.</li> <li>In 2012, over 60 historical Storm Copper drillhole collars were confirmed on the ground and recaptured via handheld Garmin GPS considered accurate to +/- 5 m.</li> <li>Modern drillhole locations were located using handheld Garmin GPS considered accurate to +/- 5 m. All coordinates were recorded in UTM</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>coordinates referenced to WGS84 Zone 15N.</p> <ul style="list-style-type: none"> <li>• Topographic elevation control is provided by a digital terrain model included as a deliverable from an Airborne Gravity and Gradiometry survey flown in 2017.</li> <li>• Modern drilling collected downhole multi-shot surveys with station captures at 100 m nominal intervals (2018) or continuous surveys with station captures at 5 m intervals (2022/2023). Core surveys were collected by north-seeking gyroscopic downhole tools (Reflex EZ Gyro or Gyro Sprint IQ). RC downhole surveys were collected using a referential downhole gyroscopic tool (SlimGyro) in conjunction with a north-seeking collar setup tool (Reflex TN14 Gyrocompass). The holes were largely straight with some expected minor deviation in the slim-line RC drillholes.</li> </ul>
<p><i>Data spacing and distribution</i></p>	<ul style="list-style-type: none"> <li>• <i>Data spacing for reporting of Exploration Results.</i></li> <li>• <i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i></li> <li>• <i>Whether sample compositing has been applied.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Recent drilling at the Storm Copper Project has generally conformed with historical drilling section lines. Drilling is spaced up to 50 m at Cyclone, up to 30 m at Chinook, and up to 100 m at Corona and Cirrus. The data distribution is considered sufficient to establish geological and grade continuity for estimation of Mineral Resources at Cyclone, Chinook, Corona, and Cirrus, in accordance with the 2012 JORC Code.</li> <li>• Developing prospects at Storm Copper (e.g. Cyclone North, Thunder, Lightning Ridge, The Gap) require additional drilling to produce the data spacing required to establish sufficient geological and grade continuity for a JORC compliant Mineral Resource Estimation. No Mineral Resources are estimated for these targets at this time.</li> <li>• Relevant drilling data was composited to 1.5 m lengths prior to Mineral Resource Estimation. A balanced compositing approach was used which allowed composite lengths of +/- 40% in an effort to minimize orphans.</li> </ul>
<p><i>Orientation of data in relation to geological structure</i></p>	<ul style="list-style-type: none"> <li>• <i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i></li> <li>• <i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Mineralisation at Storm strikes east-west and dips to the north at Cyclone, Chinook, Corona and Cirrus.</li> <li>• Historical and modern drilling was primarily oriented to the north (000) or south (090) and designed to intersect approximately perpendicular to the mineralised trends. Holes were angled to achieve (where possible) a true-width intercept through the mineralised zones. Holes at Cyclone, Chinook and Corona were angled between -45 and -90 degrees. Holes at Cirrus were angled between -45 and -75 degrees. The orientation of key structures may be locally variable.</li> <li>• Structural or mineralised geometries have not been confirmed at</li> </ul>



Criteria	JORC Code explanation	Commentary
		<p>developing prospects (Thunder, Lightning Ridge, The Gap, Cyclone North), though exploration holes are angled based on estimations of stratigraphic orientation.</p> <ul style="list-style-type: none"> <li>No orientation-based sampling bias has been identified in the data to date.</li> </ul>
Sample security	<ul style="list-style-type: none"> <li>The measures taken to ensure sample security.</li> </ul>	<ul style="list-style-type: none"> <li>No details of measures to ensure sample security are available for the historical work.</li> <li>During the modern drilling and sampling programs, samples were placed directly into a labelled plastic sample bag and sealed along with a sample tag inscribed with the unique sample number. The plastic bags were placed in woven rice (poly) bags which were secured with numbered security cable ties for shipment to the laboratory. Chain of custody was tracked and maintained throughout the shipping process.</li> <li>Sample submissions with complete list of the included samples were emailed to the laboratory, where the sample counts and numbers were checked by laboratory staff.</li> </ul>
Audits or reviews	<ul style="list-style-type: none"> <li>The results of any audits or reviews of sampling techniques and data.</li> </ul>	<ul style="list-style-type: none"> <li>No formal reviews or audits of the core sampling techniques or data were reported during the exploration by Cominco or Noranda.</li> <li>American West Metals, APEX, and the CP reviewed all available modern and historical data and sampling techniques to determine suitability for inclusion in the Mineral Resource Estimation.</li> <li>The work pertaining to this report has been carried out by reputable companies and laboratories using industry best practice and is considered suitable for use in the Mineral Resource Estimation.</li> </ul>

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> <li>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</li> <li>The security of the tenure held at the time of reporting along with any</li> </ul>	<ul style="list-style-type: none"> <li>The Aston Bay Property is located on northern Somerset Island, Nunavut, in the Canadian Arctic Archipelago. The Property comprises 173 contiguous mineral claims covering a combined area of 219,256.7 hectares. The mineral claims are located on Crown land.</li> <li>The Aston Bay Property includes the Storm Copper Project, Seal Zinc</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p><i>known impediments to obtaining a licence to operate in the area.</i></p>	<p>Project, and numerous regional prospects and targets.</p> <ul style="list-style-type: none"> <li>• The information in this release relates to mineral claims 100085, 100086, 100089 and 100090 within the Aston Bay Property.</li> <li>• All mineral claims are in good standing and held 100% by Aston Bay Holdings Ltd.</li> <li>• A portion of the Aston Bay Property, including the Storm Copper deposits, is subject to a 0.875% Gross Overriding Royalty held by Commander Resources Ltd. Aston Bay retains the option to buy down the royalty to 0.4% by making a one-time payment of CAD\$4 million to Commander.</li> <li>• On March 9, 2021, Aston Bay entered into an option agreement with American West Metals, and its wholly owned Canadian subsidiary Tornado Metals Ltd., pursuant to which American West was granted an option to earn an 80% undivided interest in the Aston Bay Property by spending a minimum of CAD\$10 million on qualifying exploration expenditures. The parties amended and restated the Option Agreement as of February 27, 2023, to facilitate American West potentially financing the expenditures through flow-through shares but did not change the commercial agreement between the parties. The expenditure requirements were completed during 2023 and American West exercised the option. American West and Aston Bay will form an 80/20 unincorporated joint venture and enter into a joint venture agreement. Under such agreement, Aston Bay shall have a free carried interest until American West has made a decision to mine upon completion of a bankable feasibility study, meaning American West will be solely responsible for funding the joint venture until such decision is made. After such decision is made, Aston Bay will be diluted in the event it does not elect to contribute its proportionate share and its interest in the Project will be converted into a 2% net smelter returns royalty if its interest is diluted to below 10%.</li> </ul>
<p><i>Exploration done by other parties</i></p>	<ul style="list-style-type: none"> <li>• <i>Acknowledgment and appraisal of exploration by other parties.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Exploration work in the areas around the Aston Bay Property and the Storm Copper Project has been carried out intermittently since the 1960's. Most of the historical work at Storm was undertaken by, or on behalf of, Cominco Ltd. ("Cominco").</li> <li>• From 1966 to 1993, exploration by Cominco, J.C. Sproule and Associates Ltd, and Esso Minerals consisted largely of geochemical sampling, prospecting, mapping and a radiometric survey for uranium mineralisation.</li> <li>• In 1994-1996 Cominco conducted geological mapping, geochemical</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>sampling, ground IP and gravity surveys, and drilling at the Seal Zinc Project.</p> <ul style="list-style-type: none"> <li>• In 1996 Cominco geologists discovered large chalcocite boulders in Ivor Creek, about 20 km east of Aston Bay, subsequently named the 2750N zone (Chinook Deposit). Copper mineralisation identified over a 7 km structural trend in the Paleozoic dolostones were named the Storm Copper showings (4100N, 2750N, 2200N, and 3500N zones).</li> <li>• In 1997, Sander Geophysics Ltd, on behalf of Cominco, conducted a high-resolution aeromagnetic survey over a 5,000 km<sup>2</sup> area of northern Somerset Island. A total of 89 line-km of IP and 71.75 line-km of HLEM surveys were completed, and 536 soil samples were collected at Storm Copper. Additionally, 17 diamond core holes totaling 2,784.5 m were completed at Storm Copper.</li> <li>• In 1998 Cominco completed 44.5 line-km of IP and collected 2,054 surface samples (soil and base-of-slope samples) at Storm Copper.</li> <li>• In 1999 Cominco completed 57.7 line-km of IP at Storm Copper. A total of 750 soil samples were collected on a grid in the Storm central graben area. Cominco also drilled 41 diamond core holes totaling 4,593 m at Storm Copper.</li> <li>• In 2000, under an option agreement with Cominco, Noranda Inc flew a 3,260 line-km GEOTEM electromagnetic and magnetic airborne geophysical survey over the property, with follow-up ground UTEM, HLEM, magnetics and gravity surveys. Eleven diamond core holes, totaling 1,886 m were completed; eight of which were drilled at the current Storm Copper Project.</li> <li>• In 2001 Noranda Inc. completed drilling at the Seal Zinc Project.</li> <li>• In 2008 Commander Resources Ltd. completed ground truthing of the Cominco geological maps along with limited confirmation resampling at Storm and Seal.</li> <li>• In 2011 Geotech Ltd, on behalf of Commander, conducted a heli-borne VTEM and aeromagnetic survey over the Storm Copper Project and Central Graben area.</li> <li>• In 2012-2013, Aston Bay Holdings completed desktop studies and review of the Commander and Cominco databases, along with ground truthing, re-sampling and re-logging operations.</li> <li>• In 2016, Aston Bay completed 12 diamond core holes totaling 1,951 m, which included the collection of downhole time domain EM surveys on five of the drillholes. Additionally, 2,026 surface geochemical samples were collected.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>• In 2017, Aston Bay contracted CGG Multi-Physics to fly a property-wide Falcon Plus airborne gravity gradiometry survey for 14,672 line-km.</li> <li>• In 2018 Aston Bay completed 13 diamond core holes totaling 3,138 m at the Storm and Seal Projects.</li> <li>• In 2021 Aston Bay entered into an option agreement with American West Metals Ltd. whereby American West could earn an 80% interest in the Aston Bay Property.</li> <li>• In 2021 Aston Bay and American West Metals completed a 94.4 line-km fixed loop, time domain EM ground survey at the Seal Zinc and Storm Copper Projects.</li> </ul>
<p><i>Geology</i></p>	<ul style="list-style-type: none"> <li>• <i>Deposit type, geological setting and style of mineralisation.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The Aston Bay Property covers a portion of the Cornwallis Fold and Thrust Belt, which affected sediments of the Arctic Platform deposited on a stable, passive continental margin that existed from Late Proterozoic to Late Silurian.</li> <li>• The Storm Copper Project, a collection of copper deposits (Cyclone, Chinook, Corona, and Cirrus) and other prospects/showings, is centered around faults that define an east-west trending Central Graben. The Central Graben locally juxtaposes the conformable Ordovician-Silurian Allen Bay Formation, the Silurian Cape Storm Formation and the Silurian Douro Formation.</li> <li>• The Allen Bay Formation consists of buff dolostone with common chert nodules and vuggy crinoidal dolowackestone. The Cape Storm Formation consists of light grey platy dolostone with argillaceous interbeds. The Douro Formation consists of dark green nodular argillaceous fossiliferous limestone.</li> <li>• The Storm Copper deposits all lie within the upper 80 m of the Allen Bay Formation and to a lesser extent in the basal Cape Storm Formation. The development of the Central Graben was likely a principal control on the migration of mineralising fluids, and the relatively impermeable and ductile Cape Storm Formation acted as a footwall “cap” for the fluids.</li> <li>• The Storm Copper deposit sulphide mineralisation is most commonly hosted within structurally prepared ground, infilling fractures and a variety of breccias including crackle breccias, and lesser in-situ replacement and dissolution breccias. Chalcocite is the most common copper mineral, with lesser chalcopyrite, and bornite, and accessory cuprite, covellite, azurite, malachite, and native copper.</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Storm Copper is interpreted to be a sediment-hosted stratiform copper sulphide deposit and can be broadly compared to Kupferschiefer and Kipushi type deposits.</li> </ul>
Drill hole Information	<ul style="list-style-type: none"> <li>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> <li>easting and northing of the drill hole collar</li> <li>elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</li> <li>dip and azimuth of the hole</li> <li>down hole length and interception depth</li> <li>hole length.</li> </ul> </li> <li>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</li> </ul>	<ul style="list-style-type: none"> <li>All historical and modern drill holes and significant intercepts were independently compiled by APEX for use in the MRE.</li> <li>Supporting drill hole information (easting, northing, elevation, dip, azimuth, hole length, significant intercepts) are included in Appendix B of the release.</li> <li>Significant intercepts relating to the Storm Copper Project have been described in previous publicly available announcements, releases, and reports.</li> </ul>
Data aggregation methods	<ul style="list-style-type: none"> <li>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.</li> <li>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</li> <li>The assumptions used for any reporting of metal equivalent values should be clearly stated.</li> </ul>	<ul style="list-style-type: none"> <li>Length weighted averaging was applied to the reported drillhole intersection grades.</li> <li>All drill assay results used in the calculation of this MRE are understood to have been previously reported and published in relevant announcements, releases, and reports. No new drilling results are being reported with this release.</li> <li>No metal equivalent values are used.</li> </ul>
Relationship between mineralisation widths and intercept lengths	<ul style="list-style-type: none"> <li>These relationships are particularly important in the reporting of Exploration Results.</li> <li>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> <li>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').</li> </ul>	<ul style="list-style-type: none"> <li>Based on extensive drilling at the Storm Copper Project, mineralisation strikes roughly east-west at all prospects, and dips shallowly to the north (&lt;10°) at Cyclone, Corona, and Cirrus. Mineralisation at Chinook is vertically plumbed, showing multiple fault structures, and has a steeper dip (~40°).</li> <li>Historical and modern drilling was oriented to the north or south, designed to intersect approximately perpendicular to the trends described above. Holes were angled to achieve (where possible) a true-width intercept through the mineralised zones.</li> <li>Structural or mineralised geometries have not been confirmed at developing prospects (Thunder, Lightning Ridge, the Gap, Cyclone North),</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>though exploration holes are angled based on estimations of stratigraphic orientation.</p> <ul style="list-style-type: none"> <li>Any drillhole intersections are reported as downhole lengths and are not necessarily considered to be representative of true widths. Significant intercepts relating to the Storm Copper Project have been described in previous announcements, releases, and reports. These documents present detailed information related to mineralised intercepts and include representative drill hole cross sections and related maps showing the distribution of significant mineralisation.</li> </ul>
<i>Diagrams</i>	<ul style="list-style-type: none"> <li>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</li> </ul>	<ul style="list-style-type: none"> <li>Significant intercepts relating to the Storm Copper Project have been described in previous announcements, releases, and reports.</li> <li>Appropriate location and layout maps, along with cross sections and diagrams illustrating the mineralisation wireframes are included in the body of the release.</li> </ul>
<i>Balanced reporting</i>	<ul style="list-style-type: none"> <li>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</li> </ul>	<ul style="list-style-type: none"> <li>All drill assay results used in the estimation of this Mineral Resource have been sourced from data compiled by the previous explorers listed above, or from information published in previous announcements, releases, and reports.</li> <li>All material exploration results have been reported.</li> </ul>
<i>Other substantive exploration data</i>	<ul style="list-style-type: none"> <li>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</li> </ul>	<ul style="list-style-type: none"> <li>All material data has been reported.</li> </ul>
<i>Further work</i>	<ul style="list-style-type: none"> <li>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</li> <li>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</li> </ul>	<ul style="list-style-type: none"> <li>Additional drilling is planned to extend mineralisation beyond the major zones outlined by the current Mineral Resource Estimation, including work at Thunder, Lightning Ridge, the Gap, and Cyclone North.</li> <li>Technical reporting on the resource modelling and estimation using recent and historical drill hole data is currently underway.</li> <li>Further activities are being planned to explore for and identify new targets and high-priority exploration areas within the Storm Copper Project.</li> </ul>

### Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	<ul style="list-style-type: none"> <li>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</li> <li>Data validation procedures used.</li> </ul>	<ul style="list-style-type: none"> <li>Modern drill logging data were collected in Excel format and verified by a geologist prior to importing to the project database. All modern logging and analytical data were imported into a Micromine database and validated using the Micromine drillhole database validation tool.</li> <li>Historical drilling data were sourced from original paper logs in publicly available Nunavut assessment reports detailing historical drilling programs, and from original Cominco digital data acquired from Cominco's successor, Teck Resources Ltd., in 2012. Paper logs were transcribed to Excel format for use in the project database. The Cominco digital data were compiled, reviewed, and verified against the original sources by Aston Bay in conjunction with the 2012-2013 re-logging and re-sampling campaigns. The verified historical data in digital format was incorporated into the Storm Copper Project database. Data was again reviewed during the resource modeling stage to ensure any transcription errors were corrected.</li> <li>All modern assays were reported by the laboratory in digital format reducing transcription errors.</li> <li>The Storm Copper Project database is maintained by APEX Geoscience Ltd.</li> <li>An APEX CP independently reviewed the drill hole database for: <ul style="list-style-type: none"> <li>drill collar errors</li> <li>duplicate samples</li> <li>overlapping intervals</li> <li>interval sequence</li> <li>geological inaccuracies</li> <li>statistical review of raw assay samples</li> </ul> </li> </ul>
Site visits	<ul style="list-style-type: none"> <li>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</li> <li>If no site visits have been undertaken indicate why this is the case.</li> </ul>	<ul style="list-style-type: none"> <li>Mr. Christopher Livingstone, P.Geo., Senior Geologist of APEX and a Competent Person, conducted site visits during the 2018, 2022, and 2023 drill programs, and included the following: <ul style="list-style-type: none"> <li>A tour of the Aston Bay Property to verify the reported geology and mineralisation at the Storm Copper Project, including the Cyclone, Chinook, Corona, and Cirrus deposits, as well as the Seal Zinc Project, and several other targets and prospects.</li> <li>An inspection of the core logging facility and review of logging and sampling procedures for each program, including internal QAQC procedures.</li> <li>Drill site and rig inspections, and collar verification.</li> <li>A review of modern drill core from each program and select historical drill intercepts.</li> </ul> </li> <li>The Mineral Resource Estimation was prepared and reviewed by Mr. Kevin Hon, P.Geo.,</li> </ul>

Criteria	JORC Code explanation	Commentary
		Senior Geologist, Mr. Warren Black, P.Geo., Senior Geologist and Geostatistician, and Mr. Steve Nicholls, MAIG, Senior Resource Geologist, all of APEX and Competent Persons. Mr. Hon, Mr. Black, and Mr. Nicholls did not conduct a site visit as Mr. Livingstone's visit was deemed sufficient by the CPs.
<i>Geological interpretation</i>	<ul style="list-style-type: none"> <li>• <i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i></li> <li>• <i>Nature of the data used and of any assumptions made.</i></li> <li>• <i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i></li> <li>• <i>The use of geology in guiding and controlling Mineral Resource estimation.</i></li> <li>• <i>The factors affecting continuity both of grade and geology.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The Storm Copper Project is interpreted to be a shallowly dipping sediment-hosted stratiform copper sulphide deposit. Shallow mineralisation associated with the Cyclone, Chinook, Corona, and Cirrus deposits is hosted within structurally prepared ground.</li> <li>• Individual geological interpretations for the Cyclone, Chinook, Corona, and Cirrus deposits were developed by APEX and American West Metals, building on previous work completed by APEX and Aston Bay. Wireframe models were constructed in Micromine 2023.5 using the implicit modeler module and drilling data as input, with manual inputs as necessary. The geological model represents the geological interpretation of the Storm Copper Project backed by geological logs of drillholes. The primary data sources included the available drill hole data as well as surface geological mapping.</li> <li>• New (2022-2023) drill holes confirmed the existence of mineralised material at the expected horizons in the Cyclone, Chinook, and Corona deposit areas. Mineralised zones were traced across different drilling generations and confirmed to be the same geological horizons.</li> <li>• Estimation domains created for the Mineral Resource Estimate adhere to the interpreted geological boundaries. Mineralised intervals were grouped together by the same geological features.</li> </ul>
<i>Dimensions</i>	<ul style="list-style-type: none"> <li>• <i>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The 2023 Maiden Storm Copper MRE area extends over an east-west length of 4.3 km (462,290 – 466,600 mE) and north-south length 2.5 km (8,172,130 - 8,174,620 mN) and spans a vertical distance of 220 m (62.5 – 282.5 mRL).</li> <li>• The Cyclone deposit area extends over an east-west length of 1.45 km (464,295 – 465,745 mE) and north-south length of 625 m (8,173,995 – 8,174,620 mN) and spans a vertical distance of 125 m (157.5 – 282.5 mRL).</li> <li>• The Chinook deposit area extends over an east-west length of 315 m (466,100 – 466,415 mE) and north-south length of 205 m (8,172,720 – 8,172,925 mN) and spans a vertical distance of 190 m (62.5 – 252.5 mRL).</li> <li>• The Corona deposit area extends over an east-west length of 575 m (466,025 – 466,600 mE) and north-south length of 345 m (8,172,130 – 8,172,475 mN) and spans a vertical distance of 82.5 m (152.5 – 235 mRL).</li> <li>• The Cirrus deposit area extends over an east-west length of 470 m (462,290 – 462,760 mE) and north-south length of 215 m (8,173,755 – 8,173,970 mN) and a vertical distance of 112.5</li> </ul>



Criteria	JORC Code explanation	Commentary
Estimation and modelling techniques	<ul style="list-style-type: none"> <li>• <i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i></li> <li>• <i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i></li> <li>• <i>The assumptions made regarding recovery of by-products.</i></li> <li>• <i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i></li> <li>• <i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i></li> <li>• <i>Any assumptions behind modelling of selective mining units.</i></li> <li>• <i>Any assumptions about correlation between variables.</i></li> <li>• <i>Description of how the geological interpretation was used to control the resource estimates.</i></li> <li>• <i>Discussion of basis for using or not using grade cutting or capping.</i></li> <li>• <i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i></li> </ul>	<p>m (107.5 – 220 mRL).</p> <ul style="list-style-type: none"> <li>• Estimation domains were constructed to honour the geological interpretation. Zones of mineralisation that were traced laterally through multiple drillholes defined the individual estimation domain wireframe shapes. Domains were constructed using the Micromine 2023.5 implicit modeler module with manual inputs as necessary.</li> <li>• Composites within each domain were analyzed for extreme outliers and composite grade value was capped. Grade capping or top cutting restricts the influence of extreme values. Examination of the Cu and Ag populations per zone indicated some outlier samples exist. Capping was performed per zone to help limit overestimation. The Cyclone zone was capped at 11 % Cu and 28 g/t Ag leading to 3 copper and 7 silver composites being capped. The Chinook zone was capped at 10 % Cu and no capping for silver. Thirteen copper composites were capped. The Corona zone was capped at 9 % copper and no capping for silver leading to 2 copper composites being capped. The Cirrus zone was capped at 2% copper and 10 g/t silver leading to 6 copper and 1 silver composites being capped.</li> <li>• Variograms were modelled using estimation domain constrained composites, and the resulting parameters were used to estimate average block grades by the Ordinary Kriging (OK) method carried out by the python package Resource Modelling Solutions Platform (RMSP) version 1.10.2. Elements Cu (%) and Ag (g/t) were estimated separately using OK.</li> <li>• The block model dimensions used are 5 m x 5 m x 2.5 m for the X, Y, and Z axes which is appropriate with the anticipated selective mining unit (SMU).</li> <li>• A dynamic search was used to more accurately represent the mineralisation trend at a given block location. A three-pass estimation was used with the maximum range determined by the variogram analysis. The maximum distance of extrapolation of data was 125 m away from the nearest drillhole.</li> <li>• Volume-variance analysis was performed to ensure the model provided the expected tonnes and grade at a given cutoff which are calculated from declustered composites and the blank block model size.</li> <li>• There is a potential to obtain silver credits during extraction of copper. For this reason, silver was estimated separately from copper.</li> <li>• There appears to be a low correlation between copper and silver from the samples in the current database. The estimation domains were constructed to capture the mineralized copper intervals while representing the geology. Silver was estimated inside the same estimation domains but separate from copper. Further geological and metallurgical testing is needed to better understand this relationship.</li> <li>• Estimation domains and block models were validated visually by APEX resource geologists and the CP upon completion.</li> </ul>

Criteria	JORC Code explanation	Commentary																																																																																								
		<ul style="list-style-type: none"> <li>No check estimates were performed as this was the Maiden Mineral Resource Estimation for the Storm Copper Project.</li> </ul>																																																																																								
Moisture	<ul style="list-style-type: none"> <li>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</li> </ul>	<ul style="list-style-type: none"> <li>Dry samples were used to estimate the 2023 Maiden Storm Copper MRE. No determinations of moisture content have been made.</li> </ul>																																																																																								
Cut-off parameters	<ul style="list-style-type: none"> <li>The basis of the adopted cut-off grade(s) or quality parameters applied.</li> </ul>	<ul style="list-style-type: none"> <li>The 2023 Maiden Storm Copper MRE is limited to material contained within the estimation domains at a nominal 0.3% mineralised envelope and is reported at a lower cut-off grade of 0.35% copper. The Storm Copper MRE detailed herein is reported as undiluted and unconstrained by pit optimization. However, the reporting cut-off grade was based on assumptions regarding possible mining methods, metal prices, metal recoveries, mining costs, processing costs, and G&amp;A costs presented below.</li> <li>Open pit mining assumes a copper price of USD\$3.85 per pound (USD\$8,487.90/t) with 90% recovery of total copper.</li> <li>Cost assumptions were used to determine the reporting cut-off grade: open pit mining cost (USD\$5.00/t), processing (USD\$10.00/t), and G&amp;A (USD\$12.00/t). Processing costs assume the use of ore sorting and jigging/dense medium separation techniques rather than traditional floatation. Cost assumptions were based on parameters used for comparable deposits.</li> <li>The Storm Copper MRE is sensitive to the selection of a reporting cut-off value, as presented in the table below:</li> </ul>																																																																																								
<table border="1"> <thead> <tr> <th>Deposit</th> <th>Category</th> <th>Cu Cutoff (%)</th> <th>Ore Type</th> <th>Tonnes</th> <th>Cu (%)</th> <th>Ag (g/t)</th> <th>Cu (t)</th> <th>Ag (Oz)</th> </tr> </thead> <tbody> <tr> <td rowspan="10">Cyclone (4100N Zone)</td> <td rowspan="10">Indicated</td> <td>0.2</td> <td>Sulphide</td> <td>5,270,000</td> <td>1.19</td> <td>3.32</td> <td>62,700</td> <td>562,800</td> </tr> <tr> <td>0.25</td> <td>Sulphide</td> <td>5,190,000</td> <td>1.20</td> <td>3.35</td> <td>62,600</td> <td>559,200</td> </tr> <tr> <td>0.3</td> <td>Sulphide</td> <td>5,090,000</td> <td>1.22</td> <td>3.38</td> <td>62,300</td> <td>553,400</td> </tr> <tr> <td><b>0.35</b></td> <td><b>Sulphide</b></td> <td><b>4,880,000</b></td> <td><b>1.26</b></td> <td><b>3.45</b></td> <td><b>61,600</b></td> <td><b>541,100</b></td> </tr> <tr> <td>0.4</td> <td>Sulphide</td> <td>4,690,000</td> <td>1.30</td> <td>3.51</td> <td>60,900</td> <td>528,200</td> </tr> <tr> <td>0.5</td> <td>Sulphide</td> <td>4,330,000</td> <td>1.37</td> <td>3.63</td> <td>59,300</td> <td>504,800</td> </tr> <tr> <td>0.6</td> <td>Sulphide</td> <td>4,000,000</td> <td>1.44</td> <td>3.76</td> <td>57,400</td> <td>483,700</td> </tr> <tr> <td>0.7</td> <td>Sulphide</td> <td>3,630,000</td> <td>1.52</td> <td>3.93</td> <td>55,100</td> <td>458,500</td> </tr> <tr> <td>0.8</td> <td>Sulphide</td> <td>3,250,000</td> <td>1.61</td> <td>4.07</td> <td>52,200</td> <td>425,400</td> </tr> <tr> <td>0.9</td> <td>Sulphide</td> <td>2,860,000</td> <td>1.71</td> <td>4.24</td> <td>48,800</td> <td>389,200</td> </tr> <tr> <td>1.0</td> <td>Sulphide</td> <td>2,500,000</td> <td>1.82</td> <td>4.45</td> <td>45,500</td> <td>357,200</td> </tr> </tbody> </table>			Deposit	Category	Cu Cutoff (%)	Ore Type	Tonnes	Cu (%)	Ag (g/t)	Cu (t)	Ag (Oz)	Cyclone (4100N Zone)	Indicated	0.2	Sulphide	5,270,000	1.19	3.32	62,700	562,800	0.25	Sulphide	5,190,000	1.20	3.35	62,600	559,200	0.3	Sulphide	5,090,000	1.22	3.38	62,300	553,400	<b>0.35</b>	<b>Sulphide</b>	<b>4,880,000</b>	<b>1.26</b>	<b>3.45</b>	<b>61,600</b>	<b>541,100</b>	0.4	Sulphide	4,690,000	1.30	3.51	60,900	528,200	0.5	Sulphide	4,330,000	1.37	3.63	59,300	504,800	0.6	Sulphide	4,000,000	1.44	3.76	57,400	483,700	0.7	Sulphide	3,630,000	1.52	3.93	55,100	458,500	0.8	Sulphide	3,250,000	1.61	4.07	52,200	425,400	0.9	Sulphide	2,860,000	1.71	4.24	48,800	389,200	1.0	Sulphide	2,500,000	1.82	4.45	45,500	357,200
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		Inferred	1.5	Sulphide	1,350,000	2.32	5.25	31,400	228,300
			0.2	Sulphide	7,930,000	1.12	3.81	88,800	971,900
			0.25	Sulphide	7,730,000	1.14	3.87	88,400	961,600
			0.3	Sulphide	7,520,000	1.17	3.93	87,800	950,900
			<b>0.35</b>	<b>Sulphide</b>	<b>7,210,000</b>	<b>1.20</b>	<b>4.03</b>	<b>86,800</b>	<b>934,700</b>
			0.4	Sulphide	6,930,000	1.24	4.13	85,700	919,700
			0.5	Sulphide	6,210,000	1.33	4.41	82,500	881,000
			0.6	Sulphide	5,440,000	1.44	4.74	78,200	829,300
			0.7	Sulphide	4,770,000	1.55	5.08	73,900	779,200
			0.8	Sulphide	4,250,000	1.65	5.36	70,000	733,600
			0.9	Sulphide	3,820,000	1.74	5.65	66,300	693,600
			1.0	Sulphide	3,410,000	1.83	5.95	62,500	653,400
			1.5	Sulphide	1,780,000	2.38	7.56	42,200	431,700
			Chinook (2750N Zone)	Inferred	0.2	Sulphide	2,400,000	1.37	3.80
	0.25	Sulphide			2,340,000	1.40	3.85	32,800	290,400
	0.3	Sulphide			2,290,000	1.42	3.91	32,600	287,900
	<b>0.35</b>	<b>Sulphide</b>			<b>2,190,000</b>	<b>1.47</b>	<b>4.00</b>	<b>32,300</b>	<b>282,300</b>
	0.4	Sulphide			2,070,000	1.54	4.11	31,800	273,200
	0.5	Sulphide			1,910,000	1.63	4.31	31,100	263,700
	0.6	Sulphide			1,780,000	1.71	4.44	30,400	254,300
	0.7	Sulphide			1,640,000	1.80	4.57	29,500	240,700
	0.8	Sulphide			1,550,000	1.86	4.64	28,800	230,600
	0.9	Sulphide			1,460,000	1.93	4.73	28,000	221,500
	1.0	Sulphide			1,360,000	1.99	4.82	27,100	211,100
	1.5	Sulphide			880,000	2.40	4.88	21,200	138,600
	Corona (2200N Zone)	Inferred	0.2	Sulphide	2,070,000	0.77	1.38	15,900	91,600
			0.25	Sulphide	1,960,000	0.80	1.40	15,600	88,400
			0.3	Sulphide	1,810,000	0.84	1.43	15,200	83,400
			<b>0.35</b>	<b>Sulphide</b>	<b>1,640,000</b>	<b>0.89</b>	<b>1.48</b>	<b>14,700</b>	<b>77,700</b>
			0.4	Sulphide	1,450,000	0.96	1.54	14,000	71,700

Criteria	JORC Code explanation	Commentary							
			0.5	Sulphide	1,160,000	1.09	1.64	12,700	61,300
			0.6	Sulphide	930,000	1.22	1.73	11,400	51,700
			0.7	Sulphide	780,000	1.34	1.78	10,400	44,700
			0.8	Sulphide	650,000	1.46	1.85	9,400	38,600
			0.9	Sulphide	530,000	1.60	1.94	8,400	32,900
			1.0	Sulphide	370,000	1.87	2.16	6,900	25,600
			1.5	Sulphide	160,000	2.72	2.83	4,300	14,500
	Cirrus (3500N Zone)	Inferred	0.2	Sulphide	1,860,000	0.57	1.28	10,500	76,300
			0.25	Sulphide	1,790,000	0.58	1.27	10,400	73,000
			0.3	Sulphide	1,700,000	0.60	1.29	10,100	70,500
			<b>0.35</b>	<b>Sulphide</b>	<b>1,550,000</b>	<b>0.62</b>	<b>1.29</b>	<b>9,700</b>	<b>64,400</b>
			0.4	Sulphide	1,460,000	0.64	1.29	9,300	60,500
			0.5	Sulphide	1,070,000	0.70	1.35	7,500	46,300
			0.6	Sulphide	690,000	0.79	1.35	5,500	30,200
			0.7	Sulphide	420,000	0.88	1.26	3,700	16,900
			0.8	Sulphide	250,000	0.97	1.16	2,500	9,500
			0.9	Sulphide	150,000	1.06	1.05	1,600	5,000
			1.0	Sulphide	80,000	1.15	0.99	900	2,600
			1.5	Sulphide	3,000	1.67	0.64	50	60
	Global	Ind + Inf	0.2	Sulphide	19,520,000	1.08	3.18	210,900	1,995,500
			0.25	Sulphide	19,010,000	1.10	3.23	209,700	1,972,600
			0.3	Sulphide	18,410,000	1.13	3.29	208,000	1,946,100
			<b>0.35</b>	<b>Sulphide</b>	<b>17,480,000</b>	<b>1.17</b>	<b>3.38</b>	<b>205,000</b>	<b>1,900,200</b>
			0.4	Sulphide	16,590,000	1.22	3.47	201,700	1,853,500
			0.5	Sulphide	14,670,000	1.32	3.72	193,000	1,757,000
			0.6	Sulphide	12,850,000	1.42	3.99	183,000	1,649,200
			0.7	Sulphide	11,240,000	1.54	4.26	172,600	1,540,000
			0.8	Sulphide	9,950,000	1.64	4.49	162,900	1,437,700
			0.9	Sulphide	8,800,000	1.74	4.74	153,200	1,342,300
			1.0	Sulphide	7,720,000	1.85	5.03	142,900	1,249,900

Criteria	JORC Code explanation	Commentary						
		1.5	Sulphide	4,170,000	2.38	6.06	99,200	813,200
		<p><i>Notes:</i></p> <ol style="list-style-type: none"> <li>1. <i>The 2023 Maiden Storm Copper MRE is reported in accordance with the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (The Joint Ore Reserves Committee Code – JORC 2012 Edition).</i></li> <li>2. <i>The 2023 Maiden Storm Copper MRE was prepared and reviewed by Mr. Kevin Hon, P.Geo., Mr. Christopher Livingstone, P.Geo., Mr. Warren Black, P.Geo., and Mr. Steve Nicholls, MAIG, all Senior Consultants at APEX Geoscience Ltd. and Competent Persons.</i></li> <li>3. <i>Mineral resources which are not mineral reserves do not have demonstrated economic viability. No mineral reserves have been calculated for the Storm Project. There is no guarantee that any part of mineral resources discussed herein will be converted to a mineral reserve in the future.</i></li> <li>4. <i>The quantity and grade of the reported Inferred Resources are uncertain in nature and there has not been sufficient work to define these Inferred Resources as Indicated or Measured Resources. It is reasonably expected that most of the Inferred Mineral Resources could be upgraded to Indicated Mineral Resources with continued exploration.</i></li> <li>5. <i>All figures are rounded to reflect the relative accuracy of the estimates. Tonnes have been rounded to the nearest 10,000 and contained metals have been rounded to the nearest 100 copper tonnes or silver ounces. Totals may not sum due to rounding.</i></li> <li>6. <i>A global bulk density of 2.79 was used for the Storm Project MRE.</i></li> <li>7. <i>The 2023 Maiden Storm Copper MRE is limited to material contained within the estimation domains at a nominal 0.3% copper mineralised envelope and is reported at a lower cut-off grade of 0.35% copper. The Storm Copper MRE detailed herein is reported as undiluted and unconstrained by pit optimization. The reporting cut-off grade was based on assumptions regarding possible mining methods, metal prices, metal recoveries, mining costs, processing costs, and G&amp;A costs.</i></li> <li>8. <i>Open pit mining assumes a copper price of USD\$3.85 per pound (USD\$8,487.90/t) with 90% recovery of total copper.</i></li> <li>9. <i>Costs are USD\$5/t for mining, USD\$10/t for processing, and USD\$12/t for G&amp;A, leading to a cut-off grade of 0.35% copper.</i></li> </ol>						

Criteria	JORC Code explanation	Commentary
Mining factors or assumptions	<ul style="list-style-type: none"> <li>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>Given the shallow depth of mineralisation at the Storm Copper deposits the assumed mining method is open pit.</li> <li>A selective mining unit size of 5 m x 5 m x 2.5 m was chosen.</li> <li>Pit slopes were assumed to be 44 degrees. No geotechnical studies have been completed to date to support this assumption. A requirement for shallower pit slopes may result in a material change to the open pit resources.</li> <li>Open pit mining assumes a copper price of USD\$3.85 per pound (USD\$8,487.90/t) with 90% recovery of total copper.</li> <li>Cost assumptions were used to determine the reporting cut-off grade: open pit mining cost (USD\$5.00/t), processing (USD\$10.00/t), and G&amp;A (USD\$12.00/t). Processing costs assume the use of ore sorting and jigging/dense medium separation techniques rather than traditional floatation. Cost assumptions were based on parameters used for comparable deposits.</li> <li>No further assumptions have been made about details of the mining methods.</li> </ul>
Metallurgical factors or assumptions	<ul style="list-style-type: none"> <li>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>Preliminary ore sorting test work was carried out at the STEINERT Australia Perth test facility in 2022. The test work was completed on a 5.5 kg of drill core sample sourced from remaining half core from 2016 hole STOR1601D, drilled at the Cyclone Deposit with an average grade of 4.16%. The sample was crushed and screened to a -25.0 +10.0 mm size fraction, removing fines (~0.03 kg). The 2022 test work was completed using a full-scale STEINERT KSS CLI XT combination sensor sorter. A combination of X-ray transmission, 3D laser, laser brightness, induction, and colour were used in the 2022 sorting algorithms. A substantial upgrade in Cu was achieved, with the concentrate fraction reporting a grade of 53.1% Cu in 10.2% of the mass yield, from an initial calculated feed grade of 6.52% Cu and a Cu recovery of 83.4%. If combined with the middling fraction, a 32.17% Cu product is produced in 19.76 of the mass yield, with a total Cu recovery of 96.5%. Given the small sample size, additional test work was recommended.</li> <li>Additional ore sorting test work was carried out at the STEINERT Australia Perth test facility in</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>2023. The test work was completed on two composite samples sourced from 2022 holes drilled at the Chinook Deposit. Composite 1 had a feed mass of 66.46 kg and a head grade of 2.72% Cu. Composite 2 had a feed mass of 87.78 kg and a head grade of 0.70% Cu. Storm Copper drill core. The samples were crushed and screened to a -25.0 +10.0 mm size fraction, removing fines (~48.92 kg total). The 2023 test work was completed using a full-scale STEINERT KSS CLI XT combination sensor sorter. A combination of X-ray transmission and induction were used in the 2023 sorting algorithms, to avoid the need to wash the feed material for 3D laser, as a consideration for the Arctic climate. Three passes were completed, producing three concentrates for each composite (Con 1, Con 2, Con 3). Both samples were amenable to ore sorting, with Con 1 fractions alone producing grades of 14.88% Cu and 13.15% in mass yields of 11.1% and 1.8% for Composites 1 and 2, respectively. Utilizing all three passes, Cu recoveries of 94.7% and 84.2% were achieved in mass yields of 34.7% and 16.6%.</p> <ul style="list-style-type: none"> <li>• Preliminary floatation testing of the concentrates produced from the 2023 ore sorting work showed that the Storm material is highly amenable to flotation, with strong upgrade potential.</li> <li>• The test work completed to date is preliminary and may not be representative of the expected grades and recoveries that could be achieved through additional ore sorting and traditional metallurgical processes. American West is currently undertaking additional ore sorting, dry and wet jigging (closed circuit), dense material separation, and flotation test work. The results from these tests will be used in future MRE updates.</li> </ul>
<p><i>Environmental factors or assumptions</i></p>	<ul style="list-style-type: none"> <li>• <i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i></li> </ul>	<ul style="list-style-type: none"> <li>• No restricting environmental assumptions have been applied.</li> </ul>
<p><i>Bulk density</i></p>	<ul style="list-style-type: none"> <li>• <i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether</i></li> </ul>	<ul style="list-style-type: none"> <li>• Bulk density (specific gravity) measurements for historical drilling are not available.</li> <li>• Resampling in 2012-2013 included the collection of bulk density data from several historical</li> </ul>

Criteria	JORC Code explanation	Commentary
	<p>wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</p> <ul style="list-style-type: none"> <li>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</li> <li>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</li> </ul>	<p>holes. A total of 41 bulk density measurements were collected from the historical core at the Storm Project.</p> <ul style="list-style-type: none"> <li>The Storm density dataset comprises 256 samples from 18 different drill holes. Samples were measured on-site by weighing selected samples first in air, then submerged in water. The measurements were used to calculate the density ratio of the sample. Samples were grouped based on geological formation and the mean value was chosen as the appropriate density value. The block model was flagged with the geological formations and the corresponding density value was assigned. It was determined that a global bulk density of 2.79 g/cm<sup>3</sup> for all domains and formations was suitable at this stage.</li> </ul>
Classification	<ul style="list-style-type: none"> <li>The basis for the classification of the Mineral Resources into varying confidence categories.</li> <li>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</li> <li>Whether the result appropriately reflects the Competent Person's view of the deposit.</li> </ul>	<ul style="list-style-type: none"> <li>The 2023 Maiden Storm Copper MRE classification of indicated and inferred is based on geological confidence, data quality, data density, and data continuity. <ul style="list-style-type: none"> <li>The indicated classification category is defined for all blocks within an area of 75 m x 75 m x 10 m that contain a minimum of 3 drillholes.</li> <li>The inferred classification area is expanded to 125 m x 120 m x 10 m that contains a minimum of 2 drillholes.</li> </ul> </li> <li>Variogram models could not be obtained for the Corona, Chinook, and Cirrus deposits. As a result, these zones were capped at inferred classification only.</li> <li>The CP considers the classification to be appropriate for the Storm Copper deposits at this stage.</li> </ul>
Audits or reviews	<ul style="list-style-type: none"> <li>The results of any audits or reviews of Mineral Resource estimates.</li> </ul>	<ul style="list-style-type: none"> <li>Currently, no audits have been performed on the MRE.</li> </ul>
Discussion of relative accuracy/ confidence	<ul style="list-style-type: none"> <li>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</li> <li>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include</li> </ul>	<ul style="list-style-type: none"> <li>The CP is confident that the 2023 Maiden Storm Copper MRE accurately reflects the geology of the Project. Detailed geological logs completed by qualified geologists were used to construct the model.</li> <li>Model validation shows good correlation between input data and the resulting estimated model. The largest source of uncertainty is the grade continuity from zones Corona, Chinook, and Cirrus. No variogram models could be obtained for these zones. More data is required to more accurately resolve the continuity of these zones.</li> </ul>



Criteria	JORC Code explanation	Commentary
	<p><i>assumptions made and the procedures used.</i></p> <ul style="list-style-type: none"><li>• <i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i></li></ul>	