

SUBSTANTIAL MINERAL RESOURCE UPGRADE AT GOVERNOR BROOME MINERAL SANDS PROJECT, WA

Updated Mineral Resources to underpin Scoping Study due in Q1 2024



Key Highlights

- Substantial 18% upgrade in Governor Broome Project Measured and Indicated resource tonnes following successful in-fill drill programs.
- Combined 93.4Mt of Resources now in the highconfidence Measured (28.4Mt) and Indicated (65Mt) Resource Categories
- Latest Mineral Assemblage results demonstrate high-value mineralogy at the Jack Track Deposit, including:
 - Combined Jack Track-Jack Track East assemblage of 68% Primary Ilmenite, 14% Secondary Ilmenite, 4.5% Rutile, 10% Zircon, and 0.8% Monazite, for a 97% VHM content
- Updated Mineral Resource Estimate and Mineral Assemblages to be incorporated in Governor Broome Project Scoping Study

Astute Metals NL (ASX: ASE) ("ASE", "Astute" or "the Company") is pleased to announce a significant upgrade of the Mineral Resources at its 100%-owned **Governor Broome Heavy Mineral Sands Project** in the South West of Western Australia.

Astute Executive Chairman, Tony Leibowitz, said:

"The completion of this Resource upgrade marks another key step forward in our value-realisation strategy for Governor Broome. Successful in-fill drilling programs completed earlier this year have resulted in a substantial uplift of the higher confidence Indicated and Measured categories. This means these Resources can be included in the upcoming Scoping Study and will ultimately be available for conversion to Ore Reserves. With this key resource upgrade now finalized, the data will be handed over to our consultants for inclusion in the Scoping Study – which remains on track for completion in QI 2024."

Background

The 100%-owned Governor Broome Heavy Mineral Sands Project is located in the mineral sands-rich coastal areas of the South West of WA. The Project is, by sealed road, located about 95km south of Busselton, 105km south of Iluka's processing plant at Capel, and 135km from Bunbury Port and from Picton, where Doral Australia has a heavy mineral separation plant. The area is well serviced by electrical infrastructure with a 132kV line located just 5km to the north and a three-phase power line passing through the Project.

Resource Development

The Governor Broome Project has been systematically de-risked by Astute over a number of years. Recent work includes the successful separation of marketable zircon, ilmenite, zircon and monazite products from bulk sample testwork for the Jack Track (eastern) part of the Project¹. This updated Mineral Resource Estimate (MRE) has resulted in a substantial 18% upgrade in higher-confidence Measured and Indicated resources from a previous 79Mt of Indicated Resources to 28.4Mt of Measured and 65Mt of Indicated Resources. This update in Mineral Resources incorporates the results of Astute's 502-hole aircore drilling programme that was carried out earlier this year, designed specifically to upgrade the category of Mineral Resources.

The upgraded resources are being included in the current Scoping Study, which is scheduled for completion in QI 2024. The locations of the various Project deposits are shown on Figure I, and a summary of the Project's Mineral Resources is shown in Table I. The deposits within R70/58, for which these revised resources are reported, are shown in Figure 2. Details of the various resources are given in Table 3.



Figure 1. Governor Broome Project tenements and Mineral Resources.



Figure 2. Resources within and adjacent to R70/58.

Tenement	Category	Tonnage (Mt)	HM (%)	Slimes
R70/58 - Jack Track	Measured	20.4	4.2	8.4
-	Indicated	21	3.5	7.9
	Total	41	3.8	8.2
	-			1
R70/53 - Governor Broome	Measured	8.0	5.0	13
	Indicated	44	5.0	13
	Inferred	7	3.5	12
	Total	59	4.8	12.5
R70/22 - Fouracres	Indicated	0.72	11.4	6.5
	Inferred	0.2	4	9
	Total	0.93	9.4	7.1
Project	Measured	28.4	4.4	9.7
	Indicated	65	4.5	11
	Inferred	8.5	3.6	11
	Total	102	4.4	11
	Resources			

 Table 1. Governor Broome Project Resources – at 2% HM lower block-cut-off grade²

Note that the above figures have been appropriately rounded. The Fouracres Resources estimated at a 3% Heavy Mineral (HM) lower block-cut-off grade

Governor Broome and Jack Track Resources estimated at a 2% HM lower block-cut-off grade

Geology and Mineralisation

The Governor Broome Project mineralisation is hosted in unconsolidated beach sands occurring on the Scott River Coastal Plain. The geological character of the mineralisation is like that of other heavy mineral deposits occurring along the Swan Coastal Plain, which have a long history of mining and processing. The mineralisation is hosted in beach placer facies sediments of the Pleistocene aged Barlee Shore-line on the southward facing Scott Coastal Plain.

The host unit to the Jack Track Deposit mineralisation, and that of the other deposits in the eastern section of R70/58, is the Warren Sands, which do not contain significant clay.

A sub-surface Bunbury Basalt headland is present to the west of the Jack Track Deposit (see Figures 1 and 2). The characteristics of both the Warren Sands-hosted mineralisation and of the underlying Beenup Beds, are markedly different on either side of the headland. To its east, both the Warren Sands and the immediately unconformably underlying Beenup Beds of the Cretaceous Warnbro Group are very fine grained, as are the heavy minerals.

To the west the grain sizes are larger, with most of the mineralisation within R70/58 also being within the Warren Sands, but its lower portions are hosted within the Beenup Beds. The Beenup Beds sediments are of two main facies in the area: clayey sands and organic clays. The clayey sands contain medium - to coarse-grained, angular to sub-angular, unconsolidated quartz and minor feldspar grains. The clay content, which is variable, tends to increase downward. Generally, it contains between 1% and 8% of valuable HM. Common accessory minerals are garnet, pyrite, and fine coal fragments.

The mineralisation that has been reported as Mineral Resources is based upon a minimum heavy mineral content of 2% over a thickness of 2m and a maximum Slimes content of 20% in any one intersection.

Exploration

The Jack Track Tenement, R70/58, has been explored with air-core drilling by Metal Sands in 2007, Astro in 2012, by Iluka in 2015, and by Astro in 2022 and 2023. Those holes within R70/58, or marginal to it and within the vicinity of the modelled mineralisation, are summarised in Table 1. The holes used in these revised Jack Track Deposit resource estimations are listed in Appendix 2.

Company	Year	Air-core	Metres
		Holes	Drilled
Metal Sands	2007	265	2,600
Astro Resources	2012	176	3,208
lluka	2015	159	2,409
Astro Resources	2022	314	3,520
Astro Resources	2023	502	5,351
Total		1,416	17,088

Table 2. S	Significant exp	loration	drill holes
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2007, 2012, and 2015 Drilling and Sampling

The Metal Sands and the 2012 Astro holes were predominantly drilled on 45° oriented lines that were up to 480m apart, with the holes mostly 80m apart along the lines. All drilling was by NQ air-core. Samples were taken at one-metre intervals, after which they were selected for HM separation on the basis of the presence of visual HM.

The Iluka holes were drilled on five near north-south lines, with holes mostly 50m apart. Along strike, however, the lines were spaced between 800m and 1700m apart. All drilling was by NQ air-core.

2022 and 2023 Drilling and Sampling

The 2022 and 2023 drilling was designed to in-fill the earlier broad-spaced lines with holes mostly spaced 80m apart on lines spaced up to 160m apart and holes. As most of the 2022 drilling and some of the 2023 drilling was within blue-gum plantations, the orientation of those lines was dependent upon the orientations of the tree rows. The orientation of remainder of the 2023 drilling lines, which were within farmland was dependent upon access.

Sample Analytical Techniques

The Metal Sands analyses (Samples GB0991 to GB1310 in Appendix 2) were analysed by Western Geolabs Pty Ltd using its standard HM analytical procedure: Split ~100g sub-sample; remove -45µ slimes and +1mm oversize; obtain HM concentrate from sub-sample using Tetrabromoethane ("TBE") separation (SG = 2.97g/cc); report HM%, slimes%, and oversize%.

The Iluka samples (Samples W00161 to W00303 in Appendix 2) were analysed at its Hamilton laboratory, where they were separated using Iluka's standard heavy media technique (Lithium Heteropolytungstate; SG = 2.85g/cc). Clay and oversize fractions were screened at sizes of -53µ and plus 710µ respectively.

The Company's 2022 and 2023 samples (Samples GB2295 to GB3110 in Appendix 2) were analysed by Western Geolabs Pty Ltd using its revised standard procedure, except that the clay and oversize fractions were screened at sizes of -53μ and plus 710 μ respectively so that the results would be comparable to those from the Iluka holes: Remove and weigh >3.3mm fraction; split 100g sub-sample; remove -53μ slimes and plus 710 μ oversize; obtain HM concentrate from remaining sub-sample TBE separation; report HM%, slimes%, and total oversize%.

Although the three methods differ, the differences have had no significant effect on the HM and the slimes contents. The Oversize percentages, however, are not comparable between all programmes.

Jack Track Deposit Mineral Assemblages – Iluka and 2022

luka carried out mineralogical testwork on 12 composite samples of HM sinks from its 2015 drilling to determine the mineral assemblage and indicative mineral quality. It reported that the assemblage of the Jack Track Deposit is ilmenite dominated and high in zircon; containing 75% ilmenite, 10.8% zircon, 6.8% leucoxene, and 2.4% rutile; for a 94% VHM content and 59.4% TiO₂.

The Company also carried out mineralogical testwork on composite samples of HM sinks from its 2022 drilling of the Jack Track Deposit². It reported that the deposit contains approximately 66.5% primary ilmenite (58% TiO₂), 14.5% secondary ilmenite (including approximately 8.5% leucoxene), 4.5% rutile, 10.5% zircon, and 0.8% monazite – for an overall 96.5% valuable heavy mineral ("VHM") content. The titanium minerals have an average composition of 63% TiO₂.

Jack Track Deposit Mineral Assemblages – 2023

Composite samples of heavy mineral concentrate ("HMC") from Astro's 2023 drilling of the JT E (Jack Track East), JT E U (Jack Track East Upper), JT SW E (Jack Track Southwest East), JT SW S (Jack track Southwest South), JT NW (Jack Track Northwest), and JT W (Jack Track West) Deposits were processed by Allied Mineral Laboratories, Perth, to assess their heavy mineral assemblages.

Five JT E composites averaged 69.2% Primary Ilmenite (57% TiO2), 14.0% Secondary Ilmenite (63% TiO2), 9.2% zircon, 4.5% Rutile (95% TiO2), and 0.7% Monazite, for a 97.5% VHM content.

The JT EU composite contained 70.9% Primary Ilmenite (57% TiO2), 12.3% Secondary ilmenite (63% TiO2), 10.2% zircon, 4.6% Rutile (95% TiO2), and 0.8% Monazite, for a 98.7% VHM content.

The JT SW E composite contained 71.2% Primary Ilmenite (57% TiO2), 10.8% Secondary ilmenite (63% TiO2), 9.3% zircon, 4.0% Rutile (95% TiO2), and 0.7% Monazite, for a 96.1% VHM content.

The JT SW S composite contained 68.7% Primary Ilmenite (57% TiO2), 11.8% Secondary ilmenite (63% TiO2), 9.7% zircon, 3.2% Rutile (95% TiO2), and 0.6% Monazite, for a 93.9% VHM content.

Two JT NW composites averaged 72.6% Primary Ilmenite (54% TiO2), 6.3% Secondary ilmenite (60% TiO2), 5.6% zircon, 2.4% Rutile (95% TiO2), 0.3% Monazite, and 8.7% Garnet, for a 95.9% VHM content.

The JT W composite contained 67.0% Primary Ilmenite (54% TiO2), 8.3% Secondary Ilmenite (60% TiO2), 8.5% zircon, 3.4% Rutile (95% TiO2), 0.4% Monazite, and 12.4% Garnet, for a 100% VHM content.

The combined results for the Jack Track and Jack Track East deposits give an average assemblage of 68% Primary Ilmenite, 14% Secondary Ilmenite, 4.5% Rutile, 10% Zircon, and 0.8% Monazite, for a 97% VHM content.

Resource Estimates

Estimate Methodology

The estimates employed Inverse Distance Squared ("ID2") modelling to produce ore block models ("OBMs") of the HM mineralisation.

HM and slimes grades were used to form wireframed hard upper and lower boundaries to the mineralisation. The grade boundaries were based on a minimum 2% HM content; and a maximum slimes limit of 35% for individual samples and 20% for intersections.

No upper cut was used for the HM grades, as virtually no outlying high values were present. The 2% lower cut-off was selected as this grade allowed grade continuity to be established between drill-holes. Grade interpolation was within 25m East-West x 25m North-South x 0.5m vertical blocks.

The wireframed bodies of mineralisation were restricted to areas that contained drill-holes with significant ratios of contained mineralisation to depth of overburden. The ratio used was "sum of 1m HM grades within intersection to depth of base of mineralisation" (e.g., 4m @ 4% HM from 6m to 10m would give a ratio of 16:10 or 1.6:1).

The wireframed areas contained drill-holes returning ratios of 1 or greater. A minimum intersection length of 2m was used.

Ore Block Models

The resulting Ore Block Models (OBMs) are shown in plan-view in Figure 2 and in sectional view in Figures 3 to 13.

Apparent gaps along the northern and southern margins of the Jack Track resource, between the Jack Track and Jack Track East resources, in the north of the JT SW E resource, and in the southeast of the SW N resource are areas of wetland containing native vegetation. Although mineralisation is present in these areas, the Competent Person considers it unlikely that regulatory permission would be obtained to mine these areas. Consequently, they are not included in the Mineral Resources.





Figure 6. Jack Track East Deposit OBM; 364400E Cross-section; V.E. 10:1



Figure 8 JT SW N Deposit OBM Cross-section; V.E. 10:1



Figure 9. JT SW E Deposit OBM and indicated cross-section location





Figure 10 JT SW S Deposit OBM Cross-section; V.E. 10:1





Figure 12. JT NW Deposit OBM Cross-section; V.E. 10:1



Figure 13. JT W Deposit OBM Cross-section; V.E. 10:1

Specific Gravities

The Specific Gravity (SG) was calculated for each ore block based on its interpolated HM content, according to the standard formula SG = 1.686 + (0.0108 x HM%).

Mineral Resources

The newly estimated mineral resources for the various deposits within and adjacent to R70/58 Jack Track Deposit are set out in Table 3.

Deposit	Category	Tonnage (Mt)	нм (%)	Slimes (%)
Jack Track	Measured	20.4	4.2	8.4
Jack Track East	Indicated	11	3.6	7.4
	Total	31.5	4.0	8.0
Jack Track Southwest North	Indicated	2.6	2.8	9.5
Jack Track Southwest East	Indicated	1.4	3.4	8.3
Jack Track Southwest South	Indicated	0.9	2.5	8.6
Jack Track Northwest	Indicated	2.3	4.2	9.5
Jack Track West	Indicated	2.5	3.4	6.7
	Total	9.6	3.3	8.5
Southeast	Inferred	1.3	3.5	8
Totals	Measured	20.4	4.2	8.4
	Indicated	21	3.5	7.9
	Inferred	1.3	3.5	8
	Total	42.5	3.8	8.1
	Resources			

Note that the above figures have been appropriately rounded. **Table 3.** R70/58 Resources – at 2% HM lower block-cut-off grade

Resource Classification

The estimated resource within the infill-drilled portion of the Jack Track Deposit to the west of 363800E is classified as Measured, as the quantity, grade, density, shape, and mineral assemblage are estimated

with sufficient confidence to support detailed mine planning and final evaluation of its economic viability. In addition, Bulk Testwork carried out indicated that its mineralisation is amenable to processing using conventional wet and dry plant techniques¹.

The other estimated Jack Track resources are classified as Indicated, as the drilling has shown both geological and mineralisation continuity throughout the area and the drilling density has been such to enable the verification of grade continuity.

The estimated resource within the Southeast Deposit is classified as Inferred, as, although the drilling has shown both geological and mineralisation continuity throughout the area, the drilling density has not been such to enable the verification of grade continuity.

The drill-hole locations are shown on Figure 2. Appendix 2 lists the air-core drill-holes drilled into the deposits for which updated resource estimates are reported. HM intercepts are provided for each hole.

Cut-off Grade

CRM selected the lower block-cut-off grade of 2% as:

- 1. This grade has been used for the estimation of the Governor Broome Resources to the west within R70/53 and consistency will be necessary for planned study of the economics of the entire Governor Broome Project; and
- 2. TZ Minerals International Pty Ltd's ("TZMI's") study in 2019 demonstrated the possibility of economic viability of mining 22.9Mt from the North Deposit and 7.9Mt from the South Deposit in R70/53. The study was based upon the resources that had been estimated using a 2% lower block-cut-off grade³. As the mineral assemblage of the Jack Track Deposit is more valuable than that of the North and South Deposits, it is reasonable to conclude that the 2% cut-off grade is also potentially economic within R70/58; and
- 3. A 2% cut-off grade allows grade continuity to be established between drill-holes.

Previous Resource Estimates

The Jack Track Deposit was estimated by Iluka and reported by the Company in 2016 as an Inferred Mineral Resource of 18.8 Mt @ 4.7% HM containing 890 thousand tonnes of HM at a 3.0% HM lower cut-off grade⁴.

The Company reported a revised Inferred Resource for the deposit of 28Mt @ 4.1% HM containing 1.15Mt of HM⁵. The larger tonnage was the result of the use of a lower block-cut-off grade of 2% HM and the extension of the resource about 800m to the west by the inclusion of two lines of holes drilled by Metal Sands in 2007.

Following infill drilling of the western portion of the Jack Track Deposit in 2022, Astro reported revised resources for mineralisation within R70/58⁶. The resources comprised an Indicated Resource of 22Mt @ 4.5% HM for the western portion of the Jack Track Deposit, an Inferred Resource of 12Mt @ 3.5% HM for the eastern portion of the Jack Track Deposit, and Inferred Resources for the Jack Track, Southwest, Northwest, and West Deposits of 22Mt @ 3.8% HM, 3.8Mt @ 4.5% HM, and 5Mt @ 3.9% HM respectively.

Overburden

The Jack Track Measured Resource's overburden has an average depth of 5.1m. The mineralisation has an average thickness of 4.0m, for an overburden to mineralisation ratio of 1.25 : 1. The Jack Track Indicated Resource's overburden has an average depth to the mineralisation of 6.7m. Its mineralisation has an average thickness is 3.4m for an overburden to mineralisation ratio of 1.95 : 1.

The JT SW N Deposit overburden has an average depth of 6.1m. The mineralisation has an average thickness of 4.7m, for an overburden to mineralisation ratio of 1.3 : 1.

The JT SW E Deposit overburden has an average depth of 10.4m. The mineralisation has an average thickness of 5.3m, for an overburden to mineralisation ratio of 2.0 : 1.

The JT SW S Deposit overburden has an average depth of 6.4m. The mineralisation has an average thickness of 6.6m, for an overburden to mineralisation ratio of 1.0 : 1.

The JT NW Deposit overburden has an average depth of 4.4m. The mineralisation has an average thickness of 2.2m, for an overburden to mineralisation ratio of 2.0 : 1.

The JT W Deposit overburden has an average depth of 4.3m. The mineralisation has an average thickness of 3.6m, for an overburden to mineralisation ratio of 1.2 : 1.

The Southeast Deposit overburden has an average depth of 7.8m. The mineralisation has an average thickness of 4.6m, for an overburden to mineralisation ratio of 1.7 : 1.

Mining Method

It has been assumed that, for potential mining of the deposits, topsoil and overburden would be removed by scrapers and the mineralisation would be mined by bulldozer feeding an in-pit slurry unit. The slurry would be pumped to a wet concentrator to produce an HM concentrate. The waste would be returned to the mine void and covered with stored topsoil.

The deposits are within farmland and blue-gum plantations and suitable agreements for compensation would need to be addressed with the owners and occupiers before mining was carried out.

Proposed Work Program

Governor Broome Project Scoping Study

TZ Minerals International (TZMI) has been engaged by Astute to carry out a Scoping Study on the Project⁷. The study, scheduled for completion in QI 2024, will include the review and assessment of mining and processing options, and a mineral products market review. It will be guided by the results of recent Project bulk testwork studies and HMC mineralogical studies. Results from the review will be used to generate the capital cost and operating cost estimates, and an economic evaluation.

Extensional Exploration Drilling

Exploratory drilling is recommended for two areas within E70/5872 that are along strike to the south-east of the Jack Track Deposits, with a view to eventual addition of further tonnes to mineral resource inventory. The drilling has regulatory approval.

Exploration of the first area would consist of the follow-up of previous air-core drilling conducted in 2012 along Fouracres Road. This drilling intersected heavy mineral mineralisation within eight holes that were located down-dip of a radiometric thorium anomaly. Unfortunately, the drill samples were not analysed.

The second area is located 4km further south-east within farmland.

ASX: ASE 23 August 2023 'Jack Track Bulk Testwork Produces Marketable Heavy Mineral Products'

Authorisation

This announcement has been authorised for release by the Board of Astute.

More Information

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² ASX: ARO 21 November 2022 'High Value Mineral Content for Jack Track Deposit'

³ ASX: ARO 16 October 2019 'Review of the Governor Broome Project Preliminary Study'

RASX: ARO 26 April 2016 'Jack Track Maiden Inferred Heavy Mineral Resource'

⁵ ASX: ARO 8 November 2021 'Re-estimation of Jack Track Tenement Resource'

⁶ ASX: ARO 19 September 2022 'Substantial increase in Mineral Resource for Governor Broome'

⁷ ASX: ASE 14 September 2023 'Commencement of Scoping Study at Governor Broome'

Competent Persons

The information in this report as it relates to Mineral Resources and Exploration Results for the Governor Broome Project is based on information compiled by John Doepel, a Director of Continental Resource Management Pty Ltd (CRM), who is a member of the Australasian Institute of Mining and Metallurgy. Mr Doepel has sufficient experience in mineral resource estimation relevant to the style of mineralisation and type of deposit under consideration to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Doepel consents to the inclusion in this announcement of the information in the form and context in which it appears.



Section 1 – Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (eg cut channels, random chips, or specific specialisedindustry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheldXRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.	Air-core drilling was used to obtain 1m samples from target horizons; Approximately 1 to 1.5 kg sub-samples were split by scoop from 1m samples
	 Include reference to measures taken to ensuresample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, suchas where there is coarse gold that has inherentsampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information 	
Drilling techniques	Drill type (eg core, reverse circulation, open- holehammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core isoriented and if so, by what method, etc).	Vertical NQ Air-core
Drill sample recovery	Method of recording and assessing core andchip sample recoveries and results assessed. Measures taken to maximise sample recoveryand ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gainof fine/coarse material.	Good recovery and retention of all size fractions; Holes cleaned at completion of each two- metre rod; Cyclone cleaned after each hole
Logging	 Whether core and chip samples have been geologically and geotechnically logged to alevel of detail to support appropriate MineralResource estimation, mining studies and metallurgical studies. Whether logging is qualitative or quantitative innature. Core (or costean, channel, etc) photography. The total length and percentage of the relevantintersections logged. 	All intervals geologically logged by Competent Person during drilling

APPENDIX 1 - JORC Code, 2012 Edition – Table 1



Sub- sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotarysplit, etc and whether sampled wet or dry. For all sample types, the nature, quality and appropriateness of the sample preparationtechnique. Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. Measures taken to ensure that the sampling isrepresentative of the in situ material	Sample preparation via drying and manual pulverisation before removal of +3.3mm material; 100g sub- samples riffle split from remaining sample
	collected,including for instance results for field duplicate/second-half sampling.	
Quality of assay data and laboratory tests	 Whether sample sizes are appropriate to thegrain size of the material being sampled. The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial ortotal. For geophysical tools, spectrometers, handheldXRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bigs) and precisionhave been established 	Analysis by Western Geolabs Pty Ltd by its standard HM analytical procedures for HM%, Slimes % (-53µ), and Oversize % (+710µ); Repeat laboratory sub-sample splits analysed at 1:12 ratio. Western Geolabs Pty Ltd re-analysed 10% of samples from within the mineralised wireframes at -45µ, +710µ
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes. Documentation of primary data, data	Sampling and logging carried out by or under supervision of Competent Person. Assay entry by digital capture of laboratory files, with later verification of significant intervals against geological logging
	entryprocedures, data verification, data storage (physical and electronic) protocols. Discuss any adjustment to assay data.	
Location of data points	Accuracy and quality of surveys used to locatedrill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Holes located by hand-held GPS for Astro holes. Grid MGA_GDA94, Zone 50;
	Specification of the grid system used. Quality and adequacy of topographic control.	Elevation data interpolated from elevation data on Google Earth



Data spacing and distribution	Data spacing for reporting of Exploration Results.	Im samples collected and analysed throughout mineralized horizons.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the MineralResource and Ore Reserve estimation procedure(s) and classifications applied.	Holes drilled on approximate 80m spacing along lines approximately 160m apart. Duplicate samples collected at 1:20 ratio. Twinned holes drilled at 1:20 ratio.
	Whether sample compositing has been applied.	No sample compositing applied
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering thedeposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	Vertical drilling through horizontal stratigraphy resulted in intersected thickness equivalent to true thickness.
Sample Security	The measures taken to ensure sample security.	Samples transported from site to laboratory by drill company personnel
Audits or Reviews	The results of any audits or reviews of samplingtechniques and data.	Review will be carried out by Competent Person



Section 2 - Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	The Jack Track Deposits are within Retention Licence R70/58, held by Governor Broome Sands Pty Ltd, a wholly owned subsidiary of Astute Metals NL. R70/58 has an expiry date of 24/07/24 and is in good standing.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	The Southeast Deposit is within Retention Licence R70/53, held by Governor Broome Sands Pty Ltd, a wholly owned subsidiary of Astute Metals NL. R70/53 has an expiry date of 03/07/26 and is in good standing.
		A small portion of the Jack Track West Deposit is within Exploration Licence E70/5200, held by Governor Broome Sands Pty Ltd, a wholly owned subsidiary of Astute Metals NL. E70/5200 has an expiry date of 25/02/24 and is in good standing.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	Metals Sands Australia Ltd carried out an air- core drilling campaign over the ground in 2007 within E70/1583, 1584, and 2464. Iluka carried out an air-core drilling campaign over the ground in 2015 within E70/2464. The recent drilling infills and extends that coverage.
Geology	Deposit type, geological setting and style of mineralisation.	The deposits are located in the Scott Coastal Plain, within the Perth Basin. They consist of beach deposited HM strands. The main host beach sand unit (Warren Sands) is overlain by surficial sand and soil. It unconformably overlies the Beenup Beds. The heavy mineral assemblage of the Jack Track and Jack Track East deposits comprises approximately 68% primary ilmenite (58% TiO ₂), 14% secondary ilmenite, 4.5% rutile, 10% zircon, and 0.8% monazite – for an overall 97% valuable heavy mineral content. The TiO ₂ minerals have an average composition of 63% TiO ₂ .
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: • easting and northing of the drill hole collar • elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar • dip and azimuth of the hole • down hole length and interception depth • hole length. If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	See Appendix 2, which lists the air-core drill-holes drilled into the deposits for which updated resource estimates are reported. HM intercepts are provided for each hole.

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APPENDIX 1 - JORC Code, 2012 Edition – Table 1



Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shownin detail. The assumptions used for any reporting of metal equivalent values should be clearly stated.	No grade cutting carried out; No metal equivalents employed.
Relationship between mineralisatio n widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width notknown').	Vertical drilling through virtually horizontal stratigraphy resulted in intersected thickness equivalent to true thickness
Diagrams	Appropriate maps and sections (with scales) andtabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	See figures in announcement body
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	Report gives balanced view of the deposits



Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	 2015: Iluka carried out mineralogical testwork on 12 composite samples of HM sinks from its 2015 drilling of the Jack Track Deposit. Its results were similar to those reported here. Iluka reported that the HM assemblage of the deposit was 75% ilmenite, 10.8% zircon, 6.8% leucoxene, and 2.4% rutile – for an overall 94% VHM content and 59.4% TiO₂. 2023: 2t Jack Track Deposit bulk sample test- work completed. 4t bulk sample composited from 960 Im samples within mineralisation. 4t sample split into two 2t samples. 2t sample processed through the feed preparation circuit with no indication of potential issues with slimes within the mineralisation. Remaining 2t bulk sample split retained at AML. Heavy mineral concentrate successfully produced in wet concentrator using conventional mineral sands processing equipment. Ilmenite, rutile, zircon, and monazite products successfully produced from HMC using conventional dry plant mineral separation equipment.
Further work	The nature and scale of planned further work (egtests for lateral extensions or depth extensions orlarge-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drillingareas, provided this information is not commercially sensitive.	Scoping study to be completed. Exploratory air-core drilling of two areas within E70/5872 along struke to the southeast of the Jack Track Deposits. Areas shown on figure 1.



Section 3 – Estimation and Reporting of Mineral Resources

Criteria	JORC Code explanation	Commentary
Database integrity	Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation Data validation procedures used	Assay and drill-hole data entered by Competent Person. Assay data copied digitally from Astro database and from files obtained from Iluka. Micromine drill-hole verification performed. Anomalous intersections checked. Drill-hole collar elevations checked, and if necessary, adjusted.
(D)		
Site visits	Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is the case	The Competent Person drilled the various Jack Track Deposits in 2022 and 2023.
Geological interpretation	Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.	High degree of confidence in geological interpretation as stratigraphy is both visually and analytically distinct and continuous.
	Nature of the data used and of any assumptions made. The effect, if any, of alternative interpretations on Mineral Resource estimation. The use of geology in guiding and controlling Mineral Resource estimation. The factors affecting continuity both of grade and geology	Mineralisation >2% HM and <20% Slimes wireframed. Area limited by ratio >1 for "mineralisation thickness times HM% divided by depth of base of mineralisation".
Dimensions	The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.	The Jack Track and Jack Track East Resources have a combined strike length of 5.2km and a maximum across-strike width of 1.25km. The Jack Track Measured Resource overburden is between 1m and 12m thick, with an average depth of 5.2m; the mineralisation is between 2m and 10m thick, with an average of 4.0m, for an overburden to mineralisation ratio of 1.25:1. The Jack Track East overburden is also between 1m and 12m thick, with an average depth of 6.7m; the mineralisation is between 2m and 8m thick, with an average of 3.4m, for an overburden to mineralisation ratio of 1.95:1. The JT SW N Deposit has a strike length of 1.5km and a maximum across-strike width of 0.5km. It has an average overburden thickness of 6.2m and an average mineralisation thickness of 4.7m; for an overburden to mineralisation ratio of 1.3:1. The JT SW E Deposit has a strike length of 0.25km. It has an average overburden thickness of 10.4m and a maximum across-strike width of 0.25km. It has an average overburden thickness of 10.4m and a maximum across-strike width of 0.25km. It has an average mineralisation thickness of 5.3m; for an overburden to mineralisation ratio of 2.0:1. The JT SW S Deposit has a strike length of 0.5km and a maximum across-strike width of 0.25km. It has an average overburden thickness of 5.3m; for an overburden to mineralisation ratio of 2.0:1.



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			and an average mineralisation thickness of 6.6m; for an overburden to mineralisation ratio of 1.0:1.
			The JT NW Deposit has a strike length of 1.8km and a maximum across-strike width of 0.6km. It has an average overburden thickness of 4.4m and an average mineralisation thickness of 2.2m; for an overburden to mineralisation ratio of 2.0:1.
0			The JT W Deposit has a strike length of 2.0km and a maximum across-strike width of 0.3km. It has an average overburden thickness of 4.3m and an average mineralisation thickness of 3.6m; for an overburden to mineralisation ratio of 1.2:1.
0	D N		The Southeast Deposit has a strike length of 0.8km and a maximum across-strike width of 0.25km. It has an average overburden thickness of 7.8m and an average mineralisation thickness of 4.6m; for an overburden to mineralisation ratio of 1.7:1.
	Estimation and	The nature and appropriateness of the	Estimation of HM and Slimes ore block grades by
	techniques	estimation technique(s) applied and key assumptions, including treatment of extreme	isz witnin >2% dajustea HM and <20% Silmes wireframes using Micromine software.
		grade values, aomaining, interpolation parameters and maximum distance of outproperties from data points. If a computer	Block size 25m E-W x 25m N-S x 0.5m vertical.
C	\square	assisted estimation method was chosen include a description of computer software and parameters used.	For areas drilled in 2022 and 2023 average hole spacing along lines 80m and average line spacing 160m.
2		The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate	For Iluka holes drilled in 2015, average hole spacing along lines 50m and line spacing but up to 1700m along strike.
((takes appropriate account of such data.	Grade boundaries form hard upper and lower boundaries.
6	\bigcirc	The assumptions made regarding recovery of by-products.	No assumptions made re correlation between
ğ		Estimation of deleterious elements or other non-grade variables of economic significance	No upper cuts, as virtually no outlying values.
((15	(eg sulphur for acid mine drainage characterisation).	No estimation of deleterious elements, as no
		In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.	No assumptions made re recovery of by- products.
		Any assumptions behind modelling of selective mining units	OBM grades validated by comparison with assays.
8		Any assumptions about correlation between variables.	
		Description of how the geological interpretation was used to control the resource estimates.	
-		Discussion of basis for using or not using grade cutting or capping.	
		The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available	
	Moisture	Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content	Tonnages estimated on dry basis.

APPENDIX 1 - JORC Code, 2012 Edition – Table 1



Cupc	ut-off arameters	The basis of the adopted cut-off grade(s) or quality parameters applied	Estimates initially reported above a range of grades. Final report grade of above 2% HM selected on basis of grade continuity of mineralisation.
	ining factors or ssumptions	Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made	Topsoil and overburden to be removed by scrapers and mineralisation to be mined by bulldozer feeding in-pit slurry unit.
	etallurgical ctors or ssumptions	The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made	Slurry pumped to wet concentrator to produce HM concentrate.
	vironmental ctors or sumptions	Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made	Waste to be returned to mine void and covered with stored topsoil. Only for the Jack Track Northwest and West Deposits and for the Southeast Deposit, is there potential for the creation of acidic soils that would need to be managed
Bu	Ilk density	Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.	SG calculated for each ore block on the basis of its interpolated HM content according to the standard formula SG = 1.686 + (0.0108 x HM%) Average SG = 1.73;
	2	The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit. Discuss assumptions for bulk density	
Cl	assification	estimates used in the evaluation process of the different material The basis for the classification of the Mineral	The estimated resource within the infill-drilled portion of the Jack Track Deposit to the west of
		Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and	363800E is classified as Measured, as the quantity, grade, density, shape, and mineral assemblage are estimated with sufficient confidence to support detailed mine planning and final evaluation of its economic viability. In

APPENDIX 1 - JORC Code, 2012 Edition – Table 1



	metal values, quality, quantity and distribution of the data). Whether the result appropriately reflects the Competent Person's view of the deposit	addition, Bulk Testwork carried out indicated that its mineralisation is amenable to processing using conventional wet and dry plant techniques. The other estimated Jack Track resources are classified as Indicated, as the drilling has shown both geological and mineralisation continuity throughout the area and the drilling density has been such to enable the verification of grade continuity. The estimated resource within the Southeast Deposit is classified as Inferred, as, although the drilling has shown both geological and mineralisation continuity throughout the area, the drilling density has not been such to enable the verification of grade continuity. The resource estimates appropriately reflect the Competent Person's impression of the deposits.
Audits or reviews	The results of any audits or reviews of Mineral Resource estimates	No audit or review has been carried out on these resource estimates.
Discussion of relative accuracy / confidence	Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.	The relative accuracy of the Mineral Resource estimates are reflected in the reporting of the Mineral Resources as per the guidelines of the 2012 JORC Code. The global resources reported are the total of the local estimates reported for each of the areas.
	The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation.	
	Documentation should include assumptions made and the procedures used. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available	



			East	North	RL	Depth	From	Interval	нм
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	(%)
			Z50)	Z50)	((/	()	(''')	(70)
	JT 1 M	GB2298	362193	6206896	46.1	8.0	2	5	5.3
(JT 1 M	GB2299	362185	6206969	46.9	7.0	3	3	3.8
27	JT 1 M	GB2300	362007	6206865	45.7	10.0	5	2	3.3
6	JT 1 M	GB2301	361867	6206862	45.7	10.0	5	3	4
9	JT 1 M	GB2303	362534	6206565	42.4	10.0	7	2	2.4
	JT 1 M	GB2304	362534	6206645	43.3	10.0	4	5	5.3
	JT 1 M	GB2305	362531	6206725	44.2	10.0	2	5	3.4
((JT 1 M	GB2306	362530	6206805	45.1	10.0	3	3	3.6
7	JT 1 M	GB2307	362539	6206884	45.9	9.0	2	4	3.1
((JT 1 M	GB2309	362019	6206934	46.5	10.0	4	2	3.4
	JT 1 M	GB2310	362011	6207005	47.3	9.0	3	3	3.9
	JT 1 M	GB2311	362002	6207080	48.2	10.0	3	2	2.7
	JT 1 M	GB2312	361704	6206882	45.9	10.0	4	2	3.9
	JT 1 M	GB2318	362365	6206559	42.3	10.0	7	2	6.4
	JT 1 M	GB2319	362362	6206637	43.2	10.0	6	2	3.9
A	JT 1 M	GB2320	362358	6206717	44.1	10.0	4	4	3.3
9	JT 1 M	GB2321	362356	6206797	45.0	10.0	5	2	3.6
C	JT 1 M	GB2322	362353	6206875	45.8	10.0	3	3	3.8
\mathcal{Q}	JT 1 M	GB2323	362346	6206953	46.7	8.0	3	2	2.4
7	JT 1 M	GB2366	362350	6206480	41.4	10.0	8	2	4.2
((JT 1 M	GB2367	362350	6206481	41.4	12.0	8	2	3.6
7	JT 1 M	GB2368	362344	6206398	40.5	12.0	9	3	3.3
A	JT 1 M	GB2369	362348	6206317	39.6	10.5	7	2	2.5
2	JT 1 M	GB2377	362544	6206490	41.5	10.0	6	3	4.1
29	JT 1 M	GB2378	362544	6206415	40.7	12.0	6	4	5.3
C	JT 1 M	GB2379	362545	6206340	39.8	12.0	7	4	5.9
(() JT 1 M	GB2380	362546	6206265	39.0	12.0	9	2	5
	JT 1 M	GB2381	362546	6206190	38.1	12.0	9	3	2.3
((JT 1 M	GB2382	362549	6206115	37.3	12.0	9	2	1.7
	JT 1 M	GB2383	362550	6206040	36.5	12.0	9	2	1.4
~	JT 1 M	GB2384	362551	6205965	36.0	12.0	10	1	1.7
29	JT 1 M	GB2385	362553	6205890	35.8	12.0	11	1	2.3
	JT 1 M	GB2409	363300	6205204	34.9	14.0	12	2	4.8
((JT 1 M	GB2410	363255	6205137	34.8	16.0	12	2	4.1
	JT 1 M	GB2411	363407	6205251	34.9	14.0	11	3	3.9
	JT 1 M	GB2417	363650	6204899	34.4	16.0	12	4	4.6
_	JT 1 M	GB2418	363803	6204887	34.4	16.0	10	5	5.8
	JT 1 M	GB2420	363803	6205248	34.9	16.0	9	3	4.6
	JT 1 M	GB2421	363803	6205247	34.9	14.0	9	3	4.9
	JT 1 M	GB2422	363227	6205303	35.0	14.0	8	5	5.5
	JT 1 M	GB2424	363177	6205247	34.9	14.0	9	5	6
	JT 1 M	GB2427	363392	6205119	34.7	16.0	9	5	4.4
	JT 1 M	GB2428	363618	6205271	35.0	14.0	10	4	3.3
	JT 1 M	GB2429	363635	6205198	34.9	16.0	10	5	4



			East	North	RL	Depth	From	Interval	ШМ
	Wireframe	Hole ID	(GDA94 Z50)	(GDA94 Z50)	(m ASL)	(m)	(m)	(m)	(%)
C	JT 1 M	GB2430	363456	6205184	34.8	14.0	8	6	4.2
2	JT 1 M	GB2431	363650	6205086	34.7	16.0	10	3	4.1
	JT 1 M	GB2432	363513	6205072	34.7	16.0	10	3	4.1
	JT 1 M	GB2433	363674	6205037	34.6	14.0	11	3	3.6
7	JT 1 M	GB2448	362697	6206561	42.3	10.0	3	5	5.9
	JT 1 M	GB2449	362698	6206485	41.5	10.0	2	7	5.2
((JT 1 M	GB2450	362702	6206405	40.6	10.0	4	5	7
6	JT 1 M	GB2451	362703	6206327	39.7	12.0	3	7	4.9
P	JT 1 M	GB2452	362705	6206250	38.8	12.0	5	6	4.4
C	JT 1 M	GB2453	362705	6206164	37.8	10.0	7	2	5.5
	JT 1 M	GB2454	362709	6206084	36.9	10.0	7.3	2	2.8
	JT 1 M	GB2455	362709	6206085	37.0	10.0	8	2	5.1
	JT 1 M	GB2456	362710	6206000	36.0	12.0	8	2	2.8
	JT 1 M	GB2457	362711	6205925	35.9	12.0	9	2	2.3
6	JT 1 M	GB2458	362712	6205828	35.8	12.0	10	2	2.2
	JT 1 M	GB2459	362706	6205750	35.6	12.0	10	2	2.2
Z	JT 1 M	GB2465	362825	6206562	42.3	12.0	3	7	4.1
((JT 1 M	GB2466	362826	6206490	41.5	10.0	3	6	5.5
2	JT 1 M	GB2467	362825	6206406	40.6	10.0	4.2	5.8	3.8
6	JT 1 M	GB2468	362835	6206331	39.7	10.0	5	5	4
6	JT 1 M	GB2469	362835	6206332	39.7	10.0	5	5	4.9
0	JT 1 M	GB2470	362833	6206242	38.7	12.0	6	5	3.8
U	JT 1 M	GB2471	362832	6206170	37.9	12.0	4	7	4.6
2	JT 1 M	GB2472	362834	6206091	37.0	10.0	6	4	3.8
	JT 1 M	GB2473	362836	6206006	36.1	12.0	8	3	3.6
	JT 1 M	GB2474	362836	6205930	35.9	12.0	9	2	3.8
7	JT 1 M	GB2475	362838	6205854	35.8	10.9	8.9	2	2.8
(JT 1 M	GB2476	362837	6205762	35.7	12.0	9	3	2.2
2	JT_1 M	GB2506	363031	6206565	42.4	8.0	2	5	3.5
	JT 1 M	GB2507	363186	6206562	42.3	8.0	1	3	3.3
2	JT 1 M	GB2510	363473	6206377	40.2	8.0	2	3	2.6
	JT 1 M	GB2511	363421	6206318	39.6	8.0	1	4	3.9
$\left(\left(\right) \right)$	JI1M	GB2512	363361	6206246	38.8	8.0	1	5	4.5
7	JI 1 M	GB2513	363305	6206186	38.1	8.0	2	5	4./
	JIIM	GB2514	363258	6206126	37.4	10.0	3.1	4.9	5.6
	JI 1 M	GB2515	363205	6206065	36.7	10.0	5	3	6.7
	JI 1 M	GB2516	363147	6206003	36.0	10.0	5	4	5.9
		GB2517	363091	6205941	35.9	10.0	6	4	5.2
		GB2518	303043	6205892	35.8	10.0	6	4	4.2
		GB2520	363596	6206323	39.6	8.0	2	2	2.2
		GB2521	303531	6206249	38.8	8.0	1	5	3.0
		GB2522	363480	6206189	38.1	8.0	1	5	4.6
		GB2523	303429	6206132	37.5	8.U	1 4	b Г С	4.1
		GB2524	262225	6206072	36.1	0.0 10.0	5	3.0 2	7.7



JT 1 M	GB2526	363280	6205955	35.9	10.0	3	6	5.9
JT 1 M	GB2527	363220	6205894	35.8	10.0	4	5	5
JT 1 M	GB2528	363163	6205830	35.8	12.0	5	4	3.4
JT 1 M	GB2529	363109	6205772	35.7	12.0	7	3	4.9

=		East	North	RL	Depth	From	Interval	ЦМ
Wireframe	Hole ID	(GDA94	(GDA94	(m ASI)	(m)	(m)	(m)	(%)
		Z50)	Z50)			(iii)		(%)
JT 1 M	GB2530	363792	6205791	35.7	10.0	4	4	4.7
JT 1 M	GB2531	363791.5	6205792	35.7	10.0	3	5	4.5
JT 1 M	GB2532	363809	6204993	34.6	16.0	7	7	4.4
JT 1 M	GB2533	363669	6204958	34.5	16.0	10	6	4.8
	GB2526	363280	6205955	35.9	10.0	3	6	5.9
JT 1 M	GB2527	363220	6205894	35.8	10.0	4	5	5
JT 1 M	GB2528	363163	6205830	35.8	12.0	5	4	3.4
JT 1 M	GB2529	363109	6205772	35.7	12.0	7	3	4.9
JT 1 M	GB2534	363461	6204999	34.6	16.0	11	4	6.1
JT 1 M	GB2535	363027	6205712	35.6	14.0	9	2	3.6
JT 1 M	GB2536	363023	6205759	35.7	12.0	8	2	5.3
JT 1 M	GB2537	363006	6205861	35.8	12.0	7	3	5.2
JT 1 M	GB2538	362833	6205700	35.6	14.0	10	2	2.7
JT 1 M	GB2539	362833	6205622	35.5	14.0	11	2	2.3
JT 1 M	GB2540	362833	6205542	35.3	14.0	10	2	2.3
JT 1 M	GB2541	363329	6206503	41.7	8.0	1	2	2.9
JT 1 M	GB2542	363269	6206427	40.8	8.0	1	5	2.9
JT 1 M	GB2543	363208	6206356	40.0	8.0	2	4	3.4
JT 1 M	GB2544	363156	6206293	39.3	10.0	3	5	6.1
JT 1 M	GB2545	363091	6206226	38.5	10.0	2	7	5.3
JT 1 M	GB2546	363045	6206171	37.9	10.0	5	4	4.2
JT 1 M	GB2547	363018	6206132	37.5	10.0	5	5	5.4
JT 1 M	GB2548	363124	6206496	41.6	8.0	1	5	3.5
JT 1 M	GB2549	363074	6206432	40.9	8.0	1	6	4.8
JT 1 M	GB2550	363032	6206379	40.3	8.0	2	5	7.8
ЛТ 1 М	GB2551	362981	6206327	39.7	10.0	2	6	6.8
JT 1 M	GB2552	362961	6206438	40.9	8.0	3	4	5.9
JT 1 M	GB2553	362976	6206491	41.5	8.0	2	5	4.2
JT 1 M	GB2554	362975.3	6206490	41.5	8.0	2	6	4.9
JT 1 M	GB2555	362840	6206735	44.3	8.0	3	3	3.4
JT 1 M	GB2557	362830	6206643	43.2	8.0	3	4	3.7
JT 1 M	GB2558	362710	6206643	43.2	8.0	2	6	4.4
JT 1 M	GB2561	363032	6206626	43.0	8.0	2	5	2.8
JT 1 M	GB2562	363139	6206615	42.9	8.0	2	3	2.6
JT 1 M	GB2563	363734	6206162	37.8	8.0	2	2	5.2
JT 1 M	GB2564	363685	6206104	37.2	8.0	3	4	3.2
JT 1 M	GB2565	363626	6206033	36.4	8.0	2.1	4.9	4
JT 1 M	GB2566	363570	6205968	36.0	10.0	3	5	4.1
JT 1 M	GB2567	363570.7	6205969	36.0	10.0	3	6	3.8
JT 1 M	GB2568	363515	6205906	35.9	10.0	6	2	4.4
JT 1 M	GB2569	363458	6205845	35.8	10.0	6	3	5.5
JT 1 M	GB2570	363403	6205782	35.7	10.0	2.3	7.7	5.3



			East	North	RL	Depth	From	Interval	ым
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	(%)
			Z50)	Z50)	(()	("")	(70)
2	JT 1 M	GB2571	363345	6205720	35.6	12.0	5	5	4.6
	JT 1 M	GB2572	363280	6205658	35.5	12.0	8	3	4.9
((JT 1 M	GB2573	363223	6205594	35.4	12.0	9	2	3.6
	JT 1 M	GB2574	363165	6205536	35.3	12.0	10	2	3
((JT 1 M	GB2575	363118	6205474	35.2	12.0	9	3	3.7
9	JT 1 M	GB2576	363752	6205640	35.5	10.0	4	6	2.7
	JT 1 M	GB2577	363699	6205578	35.4	12.0	5	6	3.7
	JT 1 M	GB2578	363647	6205520	35.3	14.0	8	4	4.9
((JT 1 M	GB2579	363590	6205456	35.2	14.0	9	3	6.4
7	JT 1 M	GB2580	363533	6205390	35.1	14.0	9	4	3.7
((JT 1 M	GB2581	363479	6205328	35.0	14.0	10	4	3.65
	JT 1 M	GB2582	363760	6205863	35.8	8.0	3	4	4.6
	JT 1 M	GB2583	363706	6205806	35.7	10.0	4	5	5.1
-	JT 1 M	GB2584	363652	6205749	35.6	10.0	4	5	3.1
	JT 1 M	GB2585	363595	6205686	35.6	10.0	5	5	5.8
	JT 1 M	GB2586	363595.7	6205687	35.6	12.0	5	5	5
((JT 1 M	GB2587	363519	6205653	35.5	12.0	6	4	6.1
9	JT 1 M	GB2588	363465	6205596	35.4	12.0	7	5	5.2
A	JT 1 M	GB2589	363408	6205536	35.3	14.0	7	5	2.1
2	JT 1 M	GB2590	363355	6205471	35.2	14.0	10	3	4
	JT 1 M	GB2591	363298	6205409	35.2	14.0	8	4	3.8
((JT 1 M	GB2592	363253	6205353	35.1	14.0	9	3	4.2
7	JT 1 M	GB2593	363775	6205467	35.2	12.0	8	3	3.2
((JT 1 M	GB2594	363716	6205404	35.1	14.0	8	4	5.1
G	JT 1 M	GB2595	363661	6205342	35.1	14.0	9	4	3.8
2	JT 1 M	GB2596	363001	6205376	35.1	14.0	11	2	3.6
6	JT 1 M	GB2597	362961	6205315	35.0	14.0	11	2	3.3
6	JT 1 M	W00161	363787.3	6206191	38.2	18.0	1	2	2.3
	JT 1 M	W00162	363787.6	6206141	37.6	18.0	2	2	3.7
((JT 1 M	W00163	363789.4	6206091	37.0	18.0	1	4	2.6
_	JT 1 M	W00164	363789	6206040	36.5	18.0	2	3	3.6
	JT 1 M	W00165	363789.8	6205991	36.0	18.0	2	3	3.6
2	JT 1 M	W00166	363791.3	6205940	35.9	18.0	1	4	3.7
6	JT 1 M	W00167	363792	6205891	35.8	18.0	2	4	4.4
Q	JТ 1 М	W00168	363792.6	6205841	35.8	18.0	3	4	5.3
	JT 1 M	W00169	363793.6	6205791	35.7	18.0	3	5	3.9
	JT 1 M	W00170	363793.9	6205741	35.6	18.0	3	5	4.9
-	JT 1 M	W00171	363795.1	6205691	35.6	18.0	4	5	4.6
	JT 1 M	W00172	363796.1	6205640	35.5	18.0	5	5	4.3
	JT 1 M	W00173	363796.3	6205591	35.4	18.0	5	4	4.2
	JT 1 M	W00174	363795.7	6205540	35.3	18.0	5	5	3.4
	JT 1 M	W00175	363796.1	6205537	35.3	18.0	5	5	4
	JT 1 M	W00176	363797.5	6205491	35.3	18.0	4	6	4.8
	JT 1 M	W00177	363798.3	6205440	35.2	18.0	5	5	4.6
	JT 1 M	W00178	363799.9	6205390	35.1	18.0	6	5	4.2
	JT 1 M	W00179	363800.4	6205340	35.1	18.0	7	5	4.2



			East	North	RL	Depth	From	Interval	НМ
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	(%)
A			Z50)	Z50)		()	(11)	(11)	(10)
24	JT 1 M	W00180	363801.3	6205291	35.0	18.0	8	5	4.7
2	JT 1 M	W00181	363802.4	6205241	34.9	18.0	9	4	3.6
	JT 1 M	W00182	363802.3	6205205	34.9	18.0	9	3	4.1
7	JT 1 M	W00183	363803	6205140	34.8	18.0	10	3	3
	JT 1 M	W00184	363802.7	6205091	34.7	18.0	10	3	3
6	JT 1 M	W00185	363803.9	6205041	34.6	18.0	6	8	3
9	JT 1 M	W00186	363805.3	6204993	34.6	18.0	7	7	3.8
0	JT 1 M	W00187	363807.3	6204788	34.3	18.0	12	3	6.2
U	JT 1 M	W00197	362951.6	6206757	44.5	15.0	3	2	2.4
	JT 1 M	W00198	362938.6	6206705	43.9	15.0	3	3	2.9
	JT 1 M	W00199	362926.5	6206657	43.4	15.0	2	5	2.6
	JT 1 M	W00200	362915.5	6206607	42.8	15.0	3	4	4.1
	JT 1 M	W00201	362908.9	6206559	42.3	15.0	5	3	3.4
	JT 1 M	W00202	362914	6206511	41.8	15.0	3	3	4.4
$(\square$	JT 1 M	W00203	362922.5	6206459	41.2	15.0	3	4	5.8
0	JT 1 M	W00204	362931	6206410	40.6	15.0	4	3	6.4
C	JT 1 M	W00205	362936	6206359	40.0	15.0	3	5	5
\mathbb{Z}	IT 1 M	W00206	362945.8	6206309	39.5	15.0	5	4	5.7
	IT 1 M	W00207	362952.3	6206264	39.0	15.0	4	5	6
Q	IT 1 M	W00208	362959.7	6206211	38.4	15.0	4	5	6.4
A		W00209	362968.1	6206161	37.8	15.0	4	5	4.8
(C	IT 1 M	W00210	362971.2	6206114	37.3	15.0	4	5	5
2	JT 1 M	W00211	362981.3	6206063	36.7	15.0	4	5	5.6
	JT 1 M	W00212	362988.8	6206015	36.2	15.0	5	4	6.1
(JT 1 M	W00213	362987	6206014	36.2	15.0	4	5	4.4
9	JT 1 M	W00214	362994.7	6205965	36.0	15.0	6	3	4.9
	JT 1 M	W00215	363002.8	6205914	35.9	15.0	6	4	3.8
29	T 1 M	W00216	363010.6	6205860	35.8	15.0	7	3	4.9
	JT 1 M	W00217	363018.5	6205807	35.7	15.0	, 7	3	3.3
$\overline{\Omega}$	JT 1 M	W00218	363024.3	6205758	35.7	15.0	8	2	3.3
	JT 1 M	W00219	363029.7	6205711	35.6	15.0	8	3	2.9
A	JT 1 M	W00220	363036.9	6205659	35.5	15.0	9	2	3.6
9	JT 1 M	W00221	363044	6205609	35.4	15.0	9	3	2.9
	JT 1 M	W00222	363049.6	6205565	35.4	15.0	8	3	2.4
	JT 1 M	W00223	363055.6	6205513	35.3	15.0	9	5	2.6
	JT 1 M	W00225	363070.8	6205412	35.2	15.0	9	3	4.9
	JT 1 M	W00226	363071.8	6205336	35.1	15.0	9	4	5.6
	JT 1 M	W00227	363027.4	6205282	35.0	18.0	10	3	5.7
	JT 1 M	W00229	363116.8	6205348	35.1	15.0	8	5	4.2
	JT 1 M	W00230	362189.4	6207061	47.9	15.0	3	5	6.2
	JT 1 M	W00233	362218.8	6206756	44.5	15.0	3	5	3.8
	JT 1 M	W00234	362219.8	6206707	44.0	15.0	6	2	4.5
	JT 1 M	W00235	362220.6	6206656	43.4	15.0	5	3	5.7
	JT 1 M	W00236	362222.4	6206608	42.8	15.0	6	2	6.1



			East	North	RL	Depth	From	Intorval	
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	(%)
			Z50)	Z50)	((/	()	()	(10)
\leq	JT 1 M	W00237	362224.1	6206545	42.1	15.0	6	2	3.2
	JT 1 M	W00238	362224.1	6206508	41.7	15.0	6	2	2.1
	JT 1 V M	GB1147	361952	6206811	45.1	15.0	5.0	2.0	5.0
	JT 1 V M	GB1148	361926	6206751	44.4	9.0	5.0	2.0	3.7
(JT 1 V M	GB1149	361865	6206691	43.8	12.0	5.0	2.0	1.3
5	JT 1 V M	GB1167	361919	6206371	40.2	12.0	8.0	1.0	2.1
	JT 1 V M	GB2295	362223	6205968	36.0	12.0	8.0	4.0	4.5
1	JT 1 V M	GB2296	362216	6206313	39.5	12.0	7.0	4.0	2.3
Ĺ	JT 1 V M	GB2297	362209	6206707	44.0	8.2	6.0	2.0	5.1
0	JT 1 V M	GB2298	362193	6206896	46.1	8.0	2.0	5.0	5.3
(JT 1 V M	GB2299	362185	6206969	46.9	7.0	3.0	3.0	3.8
	JT 1 V M	GB2300	362007	6206865	45.7	10.0	4.0	2.0	3.1
	JT 1 V M	GB2301	361867	6206862	45.7	10.0	4.0	4.0	3.4
	JT 1 V M	GB2302	361517	6206860	45.7	10.0	3.0	2.0	2.1
	JT 1 V M	GB2309	362019	6206934	46.5	10.0	4.0	2.0	3.4
	JT 1 V M	GB2310	362011	6207005	47.3	9.0	3.0	3.0	3.9
7	JT 1 V M	GB2311	362002	6207080	48.2	10.0	3.0	2.0	2.7
5	JT 1 V M	GB2312	361704	6206882	45.9	10.0	4.0	2.0	3.9
	JT 1 V M	GB2313	361772	6206938	46.6	10.0	4.0	2.0	1.8
7	JT 1 V M	GB2314	361797	6207015	47.4	10.0	3.0	2.0	1.8
	JT 1 V M	GB2325	361432	6206826	45.3	8.0	4.0	2.0	2.8
	JT 1 V M	GB2326	361446	6206746	44.4	10.0	4.0	2.0	4.0
7	JT 1 V M	GB2327	361365	6206713	44.0	10.0	4.0	2.0	1.6
	JT 1 V M	GB2329	361303	6206660	43.4	10.0	4.0	2.0	1.3
707	JT 1 V M	GB2341	361668	6206743	44.4	8.0	6.0	2.0	1.9
	JT 1 V M	GB2350	362107	6206789	44.9	10.0	5.0	4.0	5.2
6	JT 1 V M	GB2351	362063	6206719	44.1	10.0	6.0	3.0	6.7
9	JT 1 V M	GB2352	362029	6206647	43.3	10.0	7.0	2.0	4.0
	JT 1 V M	GB2353	361986	6206583	42.6	10.0	6.0	2.0	1.4
(JT 1 V M	GB2354	362091	6206519	41.8	10.0	8.0	2.0	1.2
	JT 1 V M	GB2436	362128	6206596	42.7	10.0	7.0	2.0	4.0
7	JT 1 V M	GB2437	362057	6206456	41.1	14.0	8.0	2.0	2.2
2	JT 1 V M	GB2439	362018	6206393	40.4	10.0	8.0	2.0	2.7
6	JT 1 V M	GB2440	362122	6206336	39.8	14.0	9.0	3.0	3.8
S	JT 1 V M	GB2443	362122	6206123	37.4	12.0	8.0	3.0	4.0
	JT 1 V M	GB2444	362087	6206024	36.3	14.0	10.0	2.0	3.6
	JT 1 V M	GB2445	361982	6206095	37.1	12.0	7.0	2.0	3.7
	JT 1 V M	GB2447	361910	6206012	36.1	10.0	7.0	3.0	4.0
	JT 1 V M	W00230	362189	6207061	47.9	15.0	3.0	1.0	4.3
	JT 1 V M	W00231	362220	6206854	45.6	15.0	4.0	2.0	8.5
	JT 1 V M	W00232	362219	6206807	45.1	15.0	5.0	2.0	4.9
	JT 1 V M	W00233	362219	6206756	44.5	15.0	3.0	5.0	3.8
	JT 1 V M	W00234	362220	6206707	44.0	15.0	6.0	2.0	4.5
	JT 1 V M	W00235	362221	6206656	43.4	15.0	5.0	3.0	5.7
	JT 1 V M	W00236	362222	6206608	42.8	15.0	6.0	2.0	6.1
	JT 1 V M	W00237	362224	6206545	42.1	15.0	6.0	2.0	3.2



		East	North	RL	Depth	From	Interval	ым
Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	(%)
JT 1 V M	W00238	362224	6206508	41.7	15.0	7.0	2.0	2.8
JT 1 V M	W00239	362224	6206463	41.2	15.0	7.0	2.0	1.3
JT 1 V M	W00240	362224	6206412	40.6	15.0	8.0	2.0	1.3
JT 1 V M	W00241	362225	6206363	40.1	15.0	8.0	2.0	1.4
JT 1 V M	W00243	362227	6206269	39.0	15.0	9.0	3.0	4.4
JT 2 M	GB2373	362350	6205991	36.0	12.0	8	3	5.3
JT 2 M	GB2381	362546	6206190	38.1	12.0	4	2	3.1
JT 2 M	GB2382	362549	6206115	37.3	12.0	3	3	4.6
JT 2 M	GB2383	362550	6206040	36.5	12.0	4	2	6.5
JT 2 M	GB2384	362551	6205965	36.0	12.0	5	4	5.1
JT 2 M	GB2385	362553	6205890	35.8	12.0	6	5	6.9
JT 2 M	GB2386	362553	6205815	35.7	12.0	7	3	8
JT 2 M	GB2387	362555	6205739	35.6	12.0	8	3	6.9
JT 2 M	GB2388	362555	6205740	35.6	12.0	8	3	5.7
JT 2 M	GB2389	362559	6205664	35.5	14.0	10	2	3.9
JT 2 M	GB2409	363300	6205204	34.9	14.0	8	4	5.2
JT 2 M	GB2410	363255	6205137	34.8	16.0	10	2	6.8
JT 2 M	GB2411	363407	6205251	34.9	14.0	8	3	3.6
JT 2 M	GB2420	363803	6205248	34.9	16.0	2	4	2.6
JT 2 M	GB2421	363803	6205247	34.9	14.0	2	4	2.6
JT 2 M	GB2428	363618	6205271	35.0	14.0	5	4	2.5
JT 2 M	GB2429	363635	6205198	34.9	16.0	5	4	3.3
JT 2 M	GB2430	363456	6205184	34.8	14.0	7	1	2.2
JT 2 M	GB2431	363650	6205086	34.7	16.0	6	4	3.8
JT 2 M	GB2432	363513	6205072	34.7	16.0	9	1	2.3
JT 2 M	GB2454	362709	6206084	36.9	10.0	1	4	3.5
JT 2 M	GB2455	362709	6206085	37.0	10.0	1	2	2.6
JT 2 M	GB2456	362710	6206000	36.0	12.0	5	2	3.5
JT 2 M	GB2457	362711	6205925	35.9	12.0	7	1	4.2
JT 2 M	GB2458	362712	6205828	35.8	12.0	5	3	3.9
JT 2 M	GB2459	362706	6205750	35.6	12.0	6	3	4.4
JT 2 M	GB2460	362701	6205667	35.5	12.0	8	3	5
JT 2 M	GB2461	362701	6205584	35.4	12.0	9	3	4.2
JT 2 M	GB2474	362836	6205930	35.9	12.0	2	2	2.5
JT 2 M	GB2475	362838	6205854	35.8	10.9	3	2	3.6
JT 2 M	GB2476	362837	6205762	35.7	12.0	4	3	3.9
JT 2 M	GB2529	363109	6205772	35.7	12.0	1	2	2.6
JT 2 M	GB2535	363027	6205712	35.6	14.0	3	3	2.9
JT 2 M	GB2536	363023	6205759	35.7	12.0	2	3	2.7
JT 2 M	GB2538	362833	6205700	35.6	14.0	6	2	6.7
JT 2 M	GB2539	362833	6205622	35.5	14.0	7	4	5.3
JT 2 M	GB2540	362833	6205542	35.3	14.0	8	2	8.3
JT 2 M	GB2573	363223	6205594	35.4	12.0	2	4	3.1
JT 2 M	GB2574	363165	6205536	35.3	12.0	4	4	4



			East	North	RL	Depth	Бкоро	Intowal	
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASI)	(m)	(m)	(m)	(%)
			Z50)	Z50)		(11)		(III)	(%)
2	JT 2 M	GB2575	363118	6205474	35.2	12.0	6	3	6.6
2	JT 2 M	GB2580	363533	6205390	35.1	14.0	3	3	2.7
(JT 2 M	GB2581	363479	6205328	35.0	14.0	5	4	3.2
	JT 2 M	GB2590	363355	6205471	35.2	14.0	4	2	2.7
(JT 2 M	GB2595	363661	6205342	35.1	14.0	2	2	2.2
6	JT 2 M	GB2596	363001	6205376	35.1	14.0	9	2	5
	JT 2 M	GB2597	362961	6205315	35.0	14.0	10	1	9.6
(JT 2 M	W00179	363800	6205340	35.1	18.0	1	2	2.2
	JT 2 M	W00180	363801	6205291	35.0	18.0	3	2	2.2
\overline{a}	JT 2 M	W00181	363802	6205241	34.9	18.0	2	4	3
	JT 2 M	W00182	363802	6205205	34.9	18.0	2	4	2.3
	JT 2 M	W00216	363011	6205860	35.8	15.0	1	1	2
	JT 2 M	W00217	363018	6205807	35.7	15.0	1	3	2.8
	JT 2 M	W00218	363024	6205758	35.7	15.0	2	2	3
	JT 2 M	W00219	363030	6205711	35.6	15.0	3	2	5.6
	JT 2 M	W00220	363037	6205659	35.5	15.0	3	4	4.9
F	JT 2 M	W00221	363044	6205609	35.4	15.0	4	4	3.4
9	JT 2 M	W00222	363050	6205565	35.4	15.0	5	3	6.2
6	JT 2 M	W00223	363056	6205513	35.3	15.0	6	3	5.2
7	JT 2 M	W00224	363063	6205462	35.2	15.0	7	3	7.2
/	JT 2 M	W00225	363071	6205412	35.2	15.0	8	2	8
	JT 2 M	W00229	363117	6205348	35.1	15.0	8	2	6
7	JT 3 V M	GB1150	361830	6206636	43.2	12.0	2.0	2.0	5.4
2	JT 3 V M	GB1151	361676	6206592	42.7	12.0	3.0	4.0	4.9
2	JT 3 V M	GB1152	361626	6206527	41.9	6.0	4.0	2.0	4.9
(JT 3 V M	GB1153	361561	6206466	41.2	12.0	3.0	3.0	5.8
C	ЈТ З V М	GB1154	361512	6206370	40.2	6.0	3.0	2.0	1.5
6	JT 3 V M	GB1165	361859	6206223	38.5	7.0	5.0	2.0	2.5
)T 3 V M	GB1166	361890	6206299	39.4	12.0	6.0	2.0	6.3
	JT 3 V M	GB1167	361919	6206371	40.2	12.0	6.0	2.0	5.3
7	JT 3 V M	GB1168	361938	6206457	41.1	12.0	3.0	5.0	3.7
	JT 3 V M	GB1169	361963	6206539	42.1	9.0	4.0	2.0	4.0
(JT 3 V M	GB2328	361442	6206575	42.5	10.0	3.0	2.0	2.8
l	JT 3 V M	GB2340	361566	6206693	43.8	4.1	2.1	2.0	1.9
	JT 3 V M	GB2342	361817	6206595	42.7	8.0	2.0	4.0	4.1
	JT 3 V M	GB2343	361801	6206518	41.8	8.0	4.0	3.0	5.4
	JT 3 V M	GB2344	361780	6206444	41.0	10.0	5.0	3.0	7.0
	JT 3 V M	GB2345	361717	6206383	40.3	10.0	6.0	2.0	6.1
	JT 3 V M	GB2346	361683	6206310	39.5	10.0	5.0	2.0	2.6
	JT 3 V M	GB2438	361941	6206467	41.3	10.0	6.0	3.0	2.8
	JT 3 V M	GB2441	362076	6206257	38.9	12.0	7.0	3.0	3.7
	JT 3 V M	GB2442	362002	6206207	38.3	12.0	6.0	5.0	5.2
	JT 3 V M	W00239	362224	6206463	41.2	15.0	3.0	2.0	1.2
	JT 3 V M	W00240	362224	6206412	40.6	15.0	3.0	3.0	3.1
	JT 3 V M	W00241	362225	6206363	40.1	15.0	6.0	2.0	2.6



		East	North	RL	Depth	From	Interval	НМ
Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	(%)
		Z50)	Z50)		× ź	()	()	(//)
JT 3 V M	W00242	362226	6206313	39.5	15.0	7.0	4.0	3.3
JT 3 V M	W00243	362227	6206269	39.0	15.0	6.0	3.0	3.4
JT 3 V M	W00244	362225	6206268	39.0	15.0	6.0	6.0	3.0
JT 3 V M	W00245	362228	6206220	38.5	15.0	8.0	2.0	4.5
JT 3 V M	W00246	362228	6206170	37.9	15.0	8.0	3.0	3.2
JT 3 V M	W00247	362229	6206120	37.4	15.0	8.0	3.0	5.2
JT 3 V M	W00248	362230	6206068	36.8	15.0	8.0	3.0	6.3
JT 3 V M	W00249	362231	6206018	36.2	15.0	7.0	4.0	4.7
JT 3 V M	W00250	362232	6205968	36.0	15.0	8.0	3.0	4.9
JT 3 V M	W00251	362233	6205916	35.9	15.0	8.0	3.0	3.4
JT SW N	GB1171	362127	6205578	35.4	12.0	3.0	2.0	2.6
JT SW N	GB1172	361972	6205521	35.3	12.0	5.0	4.0	3.6
JT SW N	GB1173	361852	6205404	35.1	12.0	6.0	5.0	3.6
JT SW N	GB1174	361759	6205343	35.1	12.0	6.0	3.0	2.7
JT SW N	GB1196	362230	6205120	34.7	18.0	8.0	4.0	3.3
JT SW N	GB2393	362562	6205213	34.9	18.0	6.0	5.0	3.6
JT SW N	GB2394	362857	6205062	34.7	16.0	7.0	8.0	2.6
JT SW N	GB2395	362828	6204994	34.6	16.0	6.0	5.0	3.2
JT SW N	GB2396	362788	6204933	34.5	16.0	7.0	6.0	2.6
JT SW N	GB2397	362745	6204874	34.4	14.0	5.0	7.0	2.7
JT SW N	GB2398	362708	6204818	34.3	18.0	6.0	6.0	3.3
JT SW N	GB2399	362631	6204725	34.2	18.0	8.0	6.0	3.2
JT SW N	GB2400	362702	6204664	34.1	16.0	10.0	5.0	3.1
JT SW N	GB2401	362490	6204770	35.2	20.0	14.0	5.0	3.6
JT SW N	GB2403	362236	6205051	34.6	16.0	10.0	2.0	3.4
JT SW N	GB2404	362234	6205207	34.9	12.0	6.0	4.0	2.5
JT SW N	GB2415	363004	6204927	34.5	16.0	9.0	7.0	2.7
JT SW N	GB2426	363091	6205103	34.7	16.0	11.0	4.0	5.1
JT SW N	GB2477	362536	6204829	33.3	14.0	6.0	6.0	3.0
JT SW N	GB2478	362534	6204902	34.4	14.0	4.0	9.0	2.8
JT SW N	GB2479	362533	6204981	34.5	14.0	5.0	8.0	2.6
JT SW N	GB2480	362532	6205056	34.7	14.0	5.0	9.0	2.3
JT SW N	GB2481	362529	6205127	34.8	16.5	8.0	5.0	3.4
JT SW N	GB2482	362406	6204874	34.4	16.0	10.0	4.0	2.9
JT SW N	GB2483	362404	6204950	34.5	16.0	7.0	7.0	2.6
JT SW N	GB2484	362404	6205029	34.6	16.0	10.0	4.0	2.4
JT SW N	GB2485	362403	6205117	34.2	14.0	4.0	8.0	2.8
JT SW N	GB2486	362399	6205198	34.9	14.0	10.0	3.0	2.9
JT SW N	GB2487	361872	6205730	35.6	14.0	4.2	4.0	3.6
JT SW N	GB2488	361811	6205686	35.6	8.0	4.0	3.0	3.1
JT SW N	GB2489	361708	6205740	35.6	10.0	5.0	3.0	3.6
JT SW N	GB2490	362049	6205403	35.1	8.0	5.0	3.0	2.9
JT SW N	GB2491	361942	6205486	35.3	12.0	5.0	2.0	2.6
JT SW N	GB2492	361810	6205570	35.4	8.0	4.0	2.0	2.2
JT SW N	GB2493	361693	6205644	35.5	10.0	6.0	3.0	3.2
JT SW N	GB2494	361720	6205514	35.3	8.0	4.0	4.0	3.5



			East	North	RL	Depth	From	Interval	ЦМ
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASI)	(m)	(m)	(m)	(%)
			Z50)	Z50)		(,,,,)			(70)
1	JT SW N	GB2495	361766	6205412	35.2	10.0	7.0	2.0	3.2
\geq	JT SW N	GB2496	361917	6205404	35.1	10.0	6.0	2.0	4.1
	JT SW N	GB2497	362206	6205305	35.0	10.0	5.0	4.0	2.3
$\left(\right)$	JT SW N	GB2498	362207	6205306	35.0	10.0	5.0	4.0	2.1
	JT SW N	GB2499	362148	6205245	34.9	12.0	4.0	7.0	2.4
6	JT SW N	GB2500	362083	6205192	34.8	12.0	7.0	5.0	3.1
6	JT SW N	GB2501	361945	6205257	34.9	10.0	5.0	5.0	3.5
	JT SW N	GB2502	361742	6205279	35.0	12.0	7.0	3.0	3.3
	JT SW N	GB2503	362012	6205331	35.0	12.0	6.0	4.0	3.2
	JT SW N	GB2913	362129	6205514	38.1	8.0	3.0	2.0	2.7
7	JT SW N	GB2941	362567	6205286	41.7	8.0	7.0	4.0	2.6
	JT SW N	GB2943	362866	6204807	40.0	8.0	6.0	8.0	2.2
	JT SW N	GB2945	362653	6205176	38.5	10.0	11.0	2.0	3.4
	JT SW N	GB2946	362654	6205107	37.9	10.0	9.0	7.0	2.4
	JT SW N	GB2948	362659	6204946	41.6	8.0	6.0	8.0	3.2
	JT SW N	W00228	362929	6205136	34.8	18.0	6.0	9.0	1.7
	JT SW N	W00257	362238	6205613	35.5	15.0	3.0	2.0	2.1
6	JT SW N	W00258	362238	6205562	35.4	15.0	5.0	5.0	2.3
9	JT SW N	W00259	362239	6205513	35.3	15.0	5.0	5.0	1.8
	JT SW N	W00260	362240	6205458	35.2	15.0	3.0	5.0	2.0
2	JT SW N	W00261	362242	6205410	35.2	18.0	4.0	3.0	2.4
	JT SW N	W00262	362244	6205358	35.1	18.0	4.0	4.0	2.2
(JT SW N	W00263	362244	6205309	35.0	18.0	5.0	4.0	2.3
	JT SW N	W00264	362245	6205244	34.9	18.0	6.0	5.0	2.6
7	\bigcirc								
100	JJTE	GB2949	364759	6205150	35.3	12.0	4.0	5.0	3.1
2	JT E	GB2950	364727	6205077	36.0	12.0	6.0	4.0	3.3
(JT E	GB2951	364682	6205008	35.2	12.0	6.0	4.0	3.4
	JT E	GB2952	364642	6204957	35.1	12.0	7.0	4.0	4.2
	JIE	GB2953	364856	6204984	35.3	14.0	6.0	3.0	4.4
(JIE	GB2954	364811	6204924	35.2	14.0	7.0	3.0	4.9
	JIE	GB2955	364596	6204878	35.0	14.0	8.0	4.0	4.5
	JT E	GB2956	364554	6204814	34.8	14.0	9.0	4.0	3.3
2	JT E	GB2957	364771	6204854	35.1	14.0	6.0	4.0	4.9
0	JT E	GB2958	364723	6204785	34.9	14.0	8.0	3.0	4.7
	JT E	GB2959	364680	6204726	34.8	14.0	9.0	2.0	2.4
1	JTE	GB2960	364908	6204771	35.1	14.0	10.0	2.0	3.8
	JT E	GB2961	364861	6204700	34.9	14.0	10.0	2.0	2.8
	JT E	GB2962	364637	6204657	34.7	14.0	10.0	3.0	2.5
	JT E	GB2963	364783	6204568	34.7	14.0	10.0	4.0	3.1
	JT E	GB2964	364818	6204637	34.8	14.0	10.0	3.0	2.9
	JT E	GB2965	364951	6204537	34.7	14.0	10.0	4.0	3.1
	JT E	GB2966	364917	6204482	34.6	14.0	11.0	3.0	3.5
	JT E	GB2967	364589	6204589	34.5	16.0	11.0	3.0	5.2
	JT E	GB2968	364570	6204509	34.4	16.0	12.0	2.0	4.6
	JT E	GB2969	364554	6204426	34.3	16.0	12.0	4.0	3.9
	JT E	GB2970	364504	6204359	34.1	18.0	12.0	4.0	5.7



		East	North	RL	Depth	Гиото	Intonial	
Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	нм (%)
ITE	GB2972	364736	6204498	34.5	16.0	10.0	5.0	3.6
UT E	GB2974	365038	6204668	35.0	14.0	8.0	4.0	4.2
JTE	GB2975	365083	6204732	35.1	13.0	8.0	4.0	2.7
JTE	GB2976	365120	6204794	35.3	12.0	7.0	4.0	3.4
JTE	GB2977	365121	6204795	35.3	12.0	9.0	3.0	3.8
ЛЕ	GB2978	365163	6204861	35.4	12.0	7.0	3.0	4.8
JTE	GB2979	364952	6204833	35.2	12.0	8.0	3.0	3.3
JTE	GB2980	365203	6204921	35.5	12.0	5.0	4.0	4.2
JTE	GB2981	364995	6204902	35.3	12.0	6.0	5.0	3.9
JTE	GB2982	365040	6204968	35.5	10.0	7.0	3.0	3.3
JTE	GB2983	365093	6205036	35.6	10.0	5.0	4.0	4.7
	GB2984	365157	6205052	35.7	10.0	4.0	4.0	4.1
JTE	GB2985	365085	6205144	35.8	8.0	4.0	3.0	3.8
	GB2986	364899	6205053	35.5	10.0	5.0	4.0	3.8
	GB2987	364946	6205119	35.6	8.0	5.0	3.0	5.4
ITE	GB2988	364986	6205184	35.7	8.0	4.0	2.0	3.7
ITE	GB2989	365195	6205101	35.8	10.0	4.0	2.0	2.9
	GB2990	365093	6205182	35.9	10.0	4.0	2.0	3.2
ITE	GB2991	365032	6205255	35.9	6.0	3.9	2.0	3.2
ITF	GB2992	365056	6205324	36.0	6.0	3.0	2.0	2.6
ITE	GB2993	364826	6205314	35.8	8.0	4.0	4.0	4.1
	GB2994	364907	6205352	35.0	5.9	2.0	3.9	3.8
	GB2995	364956	6205414	36.1	6.0	3.0	2.0	3.5
	GB2999	364818	6205446	36.0	6.0	3.0	3.0	<u> </u>
	GB3000	364813	6205516	35.0	6.0	1.0	3.0	33
	GB3003	364556	6205645	36.1	8.0	5.0	2.0	2.4
	GB3004	364399	6205747	36.2	6.0	3.0	2.0	3.6
ITE	GB3006	364265	6205747	36.0	8.0	3.0	3.0	2.7
ITE	GB3007	364127	6205701	35.9	8.0	2.0	5.0	2.7
ITE	GB3008	364025	6205638	35.5	8.0	6.0	2.0	<i>J</i> . <i>J</i>
	GB3009	363971	6205556	35.5	10.0	4.0	5.0	
	GB3010	363915	6205478	35.5	12.0	5.0	5.0	<u> </u>
ITF	GB3011	363861	6205381	35.4	12.0	7.0	5.0	3.7
ITF	GB3012	364013	6205143	34.9	14.0	8.0	5.0	4.1
	GB3013	364069	6205182	35.1	14.0	11.0	2.0	4.8
ITE	GB3014	364116	6205241	35.2	12.0	8.0	4.0	5.0
	000017	201110	6205241	05.2	40.0	0.0		0.0
JTE	GB3015	364167	6205310	35.3	12.0	8.0	3.0	3.2
JT E	GB3016	364221	6205387	35.5	10.0	7.0	3.0	2.8
JTE	GB3017	364123	6205042	34.9	14.0	10.0	2.0	2.3
JTE	GB3018	364175	6205098	35.0	14.0	10.0	2.0	5.1
JT E	GB3019	364216	6205161	35.1	12.0	8.0	4.0	4.5
JT E	GB3020	364268	6205240	35.3	12.0	7.0	4.0	3.9
JT E	GB3021	364324	6205321	35.5	10.0	6.0	4.0	4.4
JT É	GB3022	364293	6205024	35.0	14.0	9.0	5.0	4.9
JT E	GB3023	364344	6205089	35.1	12.0	9.0	3.0	3.6
JT E	GB3024	364385	6205153	35.2	12.0	9.0	3.0	3.6
	GB3025	364235	6204958	34 8	14.0	10.0	40	4 8



			East	North	RL	Depth	From	Intorval	
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	∩™ (%)
			Z50)	Z50)	((11)	(11)	(/0)
	JT E	GB3026	364151	6204962	34.8	14.0	11.0	3.0	4.1
\square	JT E	GB3027	364053	6204935	34.7	14.0	11.0	3.0	5.0
	JT E	GB3028	363954	6204821	34.4	16.0	12.0	3.0	3.9
(JT E	GB3031	364086	6204715	34.4	18.0	12.0	4.0	5.6
2	JT E	GB3032	364119	6204773	34.5	16.0	10.0	6.0	5.0
6	JT E	GB3033	364119	6204774	34.5	16.0	11.0	5.0	4.3
Y	JT E	GB3034	364198	6204890	34.8	16.0	10.0	4.0	3.4
	JT E	GB3036	364284	6204708	34.5	16.0	11.0	4.0	3.8
	JT E	GB3037	364267	6204855	34.7	16.0	11.0	3.0	4.2
(() JT E	GB3064	365999	6204594	35.7	8.0	4.0	3.0	2.8
A	JT E	GB3068	365659	6204741	35.6	10.0	4.0	5.0	2.6
(C	JTE	GB3076	364651	6205500	37.0	10.0	5.0	2.0	2.7
Д	JTE	GB3077	364699	6205366	35.8	10.0	5.0	3.0	4.2
Т	JT E	GB3078	364692	6205283	35.7	10.0	5.0	4.0	3.9
	JTE	GB3079	364670	6205207	35.5	10.0	6.0	4.0	2.7
	JT E	GB3080	364615	6205174	35.5	12.0	7.0	3.0	2.8
	JT E	GB3081	364616	6205174	35.5	12.0	8.0	2.0	4.9
A	JTE	GB3082	365829	6204702	35.7	8.0	5.0	2.0	2.2
Y	JT E	GB3083	365827	6204765	35.8	8.0	3.0	3.0	3.4
a	JT E	GB3088	365583	6204801	35.7	8.0	5.0	2.0	2.2
22	JT E	GB3092	365472	6204815	35.6	10.0	6.0	2.0	3.8
7	JTE	GB3095	365364	6204886	35.6	8.0	5.0	3.0	3.7
((JTE	GB3096	365378	6204960	35.7	8.0	4.0	2.0	2.6
М	JTE	GB3099	364600	6205083	35.3	12.0	7.0	4.0	3.4
(JTE	GB3100	364528	6205057	35.2	12.0	8.0	3.0	3.2
2	JIE	GB3101	364464	6205015	35.1	12.0	10.0	2.0	2.5
2	JIE	GB3102	364395	6204986	35.0	12.0	10.0	2.0	2.3
	JIE	GB3103	364316	6204974	34.9	14.0	9.0	5.0	3.8
Q	JIE	GB3104	364542	6205181	35.4	10.0	8.0	2.0	2.9
A	JIE	GB3105	364541	6205181	35.4	12.0	9.0	2.0	2.9
((JIE	GB3106	364564	6205222	36.0	10.0	8.0	2.0	3.6
۲	JIE	GB3107	364601	6205302	35.7	10.0	6.0	3.0	4.8
~	JIE	GB3108	364593	6205404	35.8	10.0	5.0	2.0	4.6
2	JIE	GB3109	364607	6205462	37.4	10.0	6.0	2.0	3.1
		083110	265265	6203520	35.9 25 5	8.U 1E 0	4.0	3.0	5.L 1 0
Q		W00290	305205	6204880	33.3 25 5	12.0	6.0	2.0	4.0
		W00297	305257	6204927	35.5	12.0	<u> </u>	2.0	3.4
		W00298	265227	6205021	25.0	12.0	5.0	2.0	2.9
		W/00299	365210	6205021	25 0	12.0	1.0	2.0	5.0
		W00300	265104	6205072	33.0 25.0	12.0	4.0	4.0	2.9
		W/00202	365202	6205110	25.0	12.0	4.0	2.0	3.2
	ITE	W/00302	365170	6205174	36.0	9.0	2.0	2.0	2.7
	JIE	000000	2021/0	0203209	30.0	9.0	2.0	2.0	5.7
	JTEU	GB2955	364596	6204878	35.0	14.0	4.0	2.0	2.3
	JT E U	GB2956	364554	6204814	34.8	14.0	4.0	5.0	2.1
	JT E U	GB2963	364783	6204568	34.7	14.0	6.0	4.0	3.2
	JT E U	GB2964	364818	6204637	34.8	14.0	5.0	3.0	2.8



			East	North	RL	Depth	Гкоро	Intonial	
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	нм (%)
	ITFU	GB2965	364951	6204537	34 7	14.0	5.0	3.0	2.5
1	HEU	GB2966	364917	6204482	34.6	14.0	6.0	5.0	3.5
ľ	JTEU	GB2967	364589	6204589	34.5	16.0	7.0	4.0	2.8
7	JTEU	GB2968	364570	6204509	34.4	16.0	9.0	3.0	2.9
4	JTEU	GB3022	364293	6205024	35.0	14.0	4.0	2.0	2.3
	JTEU	GB3025	364235	6204958	34.8	14.0	5.0	5.0	2.4
ſ	JTEU	GB3026	364151	6204962	34.8	14.0	5.0	4.0	3.3
	JTEU	GB3027	364053	6204935	34.7	14.0	6.0	5.0	5.2
1	JTEU	GB3034	364198	6204890	34.8	16.0	7.0	3.0	3.1
1	JT E U	GB3037	364267	6204855	34.7	16.0	7.0	4.0	2.4
Ľ	JTEU	GB3103	364316	6204974	34.9	14.0	3.0	3.0	3.6
2	\bigcirc								
9	JT SW E	GB1190	361602	6204841	34.3	18.0	9.0	10.0	6.0
	JT SW E	GB1191	361761	6204843	34.3	15.0	9.0	10.0	4.0
	JT SW E	GB1192	361922	6204844	34.3	18.0	9.0	10.0	6.0
	JT SW E	GB1193	362081	6204847	34.4	18.0	10.0	11.0	5.0
	JT SW E	GB1194	362235	6204851	34.4	21.0	12.0	13.0	6.0
	JT SW E	GB2399	362631	6204725	34.2	18.0	8.0	9.0	6.0
	JT SW E	GB2402	362358	6204806	34.3	18.0	13.0	14.0	3.0
	JT SW E	GB2406	362363	6204744	34.2	18.0	12.0	13.0	5.0
	JT SW E	GB2914	362363	6204581	36.0	17.0	12.0	13.0	5.0
	JT SW E	GB2915	362134	6204630	35.2	18.0	12.0	13.0	5.0
7	JT SW E	GB2916	362066	6204717	35.1	16.0	12.0	13.0	4.0
Ч	JT SW E	GB2917	362036	6204813	35.2	16.0	10.0	11.0	6.0
2	JT SW E	GB2919	361772	6204640	34.9	16.0	8.0	9.0	7.0
Y	JT SW E	GB2920	361917	6204614	34.9	16.0	11.0	12.0	5.0
7	JT SW E	GB2921	361905	6204670	35.0	16.0	9.0	10.0	7.0
7	JT SW E	GB2922	361826	6204703	34.6	16.0	9.0	10.0	7.0
(]	JT SW E	GB2923	361971	6204726	35.1	16.0	11.0	12.0	5.0
Y	JT SW E	GB2924	362088	6204651	35.1	16.0	9.0	10.0	6.0
2	JT SW E	GB2925	362266	6204540	35.9	18.0	14.0	15.0	3.0
1	JT SW E	GB2926	362075	6204588	34.9	16.0	12.0	13.0	4.0
	JT SW E	GB2931	362049	6204781	35.2	16.0	10.0	11.0	4.0
7	JT SW E	GB2932	362049	6204780	35.2	16.0	12.0	13.0	4.0
	JT SW E	GB2933	361770	6204793	34.3	16.0	7.0	8.0	8.0
	JT SW E	GB2934	361820	6204797	35.2	16.0	9.0	10.0	7.0
4	2								
	JT SW S	GB1179	361398	6204938	35.5	19.0	7.0	9.0	3.0
	JT SW S	GB1198	361220	6205104	34.7	18.0	9.0	8.0	2.8
	JT SW S	GB1199	361370	6204899	33.4	18.0	6.0	8.0	2.8
	JT SW S	GB2838	360904	6205085	29.5	12.0	7.0	5.0	2.6
	JT SW S	GB2839	361082	6205078	31.0	13.0	10.5	2.0	2.8
	JT E	W00300	365219	6205072	35.8	12.0	4.0	4.0	5.9
	JT E	W00301	365194	6205118	35.8	12.0	4.0	3.0	3.2
	JT E	W00302	365202	6205174	35.9	9.0	3.0	3.0	3.7
	JT E	W00303	365170	6205269	36.0	9.0	2.0	2.0	3.7
	JT E	GB3020	364268	6205240	35.3	12.0	7.0	4.0	3.9



			East	North	RL	Depth	From	Interval	нм
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASL)	(m)	(m)	(m)	(%)
			Z50)	Z50)		(,	()	(''')	(70)
	JT E U	GB2955	364596	6204878	35.0	14.0	4.0	5.0	2.0
20	JT E U	GB2956	364554	6204814	34.8	14.0	4.0	5.0	4.0
7	JT E U	GB2963	364783	6204568	34.7	14.0	6.0	7.0	4.0
((JT E U	GB2964	364818	6204637	34.8	14.0	5.0	6.0	3.0
V	JTEU	GB2967	364589	6204589	34.5	16.0	7.0	8.0	4.0
	JT E U	GB2968	364570	6204509	34.4	16.0	9.0	10.0	2.0
6	JT E U	GB3022	364293	6205024	35.0	14.0	4.0	5.0	2.0
Y	JT E U	GB3025	364235	6204958	34.8	14.0	5.0	6.0	4.0
0	JT E U	GB3026	364151	6204962	34.8	14.0	5.0	6.0	4.0
(\mathbf{Q})	JT E U	GB3027	364053	6204935	34.7	14.0	6.0	7.0	5.0
	JT E U	GB3034	364198	6204890	34.8	16.0	7.0	8.0	3.0
	JT E U	GB3037	364267	6204855	34.7	16.0	7.0	8.0	3.0
Ч	JT E U	GB3103	364316	6204974	34.9	14.0	3.0	4.0	3.0
	JT SW E	GB1190	361602	6204841	34.3	18.0	9.0	10.0	6.0
$\left(\right)$	JT SW E	GB1191	361761	6204843	34.3	15.0	9.0	10.0	4.0
9	JT SW E	GB1192	361922	6204844	34.3	18.0	9.0	10.0	6.0
A	JT SW E	GB1193	362081	6204847	34.4	18.0	10.0	11.0	5.0
\mathbb{Z}	JT SW E	GB1194	362235	6204851	34.4	21.0	12.0	13.0	6.0
	JT SW E	GB2399	362631	6204725	34.2	18.0	8.0	9.0	6.0
((JT SW E	GB2402	362358	6204806	34.3	18.0	13.0	14.0	3.0
A	JT SW E	GB2406	362363	6204744	34.2	18.0	12.0	13.0	5.0
(C	JT SW E	GB2914	362363	6204581	36.0	17.0	12.0	13.0	5.0
7	JT SW E	GB2915	362134	6204630	35.2	18.0	12.0	13.0	5.0
2	JT SW E	GB2916	362066	6204717	35.1	16.0	12.0	13.0	4.0
6	JT SW E	GB2917	362036	6204813	35.2	16.0	10.0	11.0	6.0
U	JT SW E	GB2919	361772	6204640	34.9	16.0	8.0	9.0	7.0
2	JT SW E	GB2920	361917	6204614	34.9	16.0	11.0	12.0	5.0
((JT SW E	GB2921	361905	6204670	35.0	16.0	9.0	10.0	7.0
	JT SW E	GB2922	361826	6204703	34.6	16.0	9.0	10.0	7.0
~	JT SW E	GB2923	361971	6204726	35.1	16.0	11.0	12.0	5.0
2	JT SW E	GB2924	362088	6204651	35.1	16.0	9.0	10.0	6.0
	JT SW E	GB2925	362266	6204540	35.9	18.0	14.0	15.0	3.0
((JT SW E	GB2926	362075	6204588	34.9	16.0	12.0	13.0	4.0
	JT SW E	GB2931	362049	6204781	35.2	16.0	10.0	11.0	4.0
	JT SW E	GB2932	362049	6204780	35.2	16.0	12.0	13.0	4.0
	JT SW E	GB2933	361770	6204793	34.3	16.0	7.0	8.0	8.0
	JT SW E	GB2934	361820	6204797	35.2	16.0	9.0	10.0	7.0
	JT SW S	GB1179	361398	6204938	35.5	19.0	7.0	9.0	3.0
	JT SW S	GB1198	361220	6205104	34.7	18.0	9.0	8.0	2.8
	JT SW S	GB1199	361370	6204899	33.4	18.0	6.0	8.0	2.8
	JT SW S	GB2838	360904	6205085	29.5	12.0	7.0	5.0	2.6
	JT SW S	GB2839	361082	6205078	31.0	13.0	10.5	2.0	2.8
	JT SW S	GB2840	361252	6205010	32.5	16.0	7.0	8.0	2.6



			East	North	RL	Depth	From	Intorval	
	Wireframe	Hole ID	(GDA94	(GDA94	(m ASI)	(m)	(m)	(m)	(%)
			Z50)	Z50)		()	(11)		(%)
	JT SW S	GB2841	361303	6204965	32.0	16.0	8.0	7.0	2.3
2	JT SW S	GB2842	361306	6204843	32.0	18.0	4.0	10.0	2.2
	JT SW S	GB2843	361179	6204967	31.0	16.0	6.0	8.0	2.5
	JT SW S	GB2844	361180	6204967	31.0	14.0	6.0	7.0	2.2
	JT SW S	GB2845	361052	6205000	30.5	13.0	4.0	2.0	3.5
1	JT SW S	GB2846	360960	6205000	29.9	14.0	5.0	2.0	4.4
Y	JT SW S	GB2847	360981	6204921	30.0	14.0	7.0	6.0	2.5
	JT SW S	GB2848	361124	6204891	29.5	14.0	5.0	8.0	2.1
	JT SW S	GB2849	361233	6204862	30.0	15.0	5.0	9.0	2.3
	JT SW S	GB2850	361089	6204834	30.0	14.0	6.0	7.0	2.4
	JT NW	GB1265	358741.7	6208394	28.0	9.0	2.92	4.0	2.0
9	JT NW	GB1266	358798.1	6208449	28.6	9.0	2.18	4.0	3.0
	JT NW	GB1267	358855.8	6208508	30.2	9.0	2	6.0	2.0
	JT NW	GB1268	358910.5	6208564	29.2	9.0	3.83	5.0	2.0
	JT NW	GB1269	358966.9	6208623	29.1	9.0	4.14	4.0	3.0
	JT NW	GB1270	359021.6	6208685	28.9	6.0	1.39	3.0	2.0
7	JT NW	GB1277	358572.1	6208901	29.0	6.0	2.39	3.0	2.0
5	JT NW	GB1278	358457.6	6208791	28.9	6.0	2.52	3.0	2.0
	JT NW	GB1279	358119	6209125	29.5	6.0	2.48	4.0	2.0
Q	JT NW	GB1301	358001.4	6209009	28.3	7.0	5.1	4.0	2.0
	JT NW	GB1302	358062.3	6209071	28.6	7.0	4.55	4.0	2.0
(JT NW	GB1303	358335.9	6208662	28.4	11.0	3.11	5.0	3.0
9	JT NW	GB1304	358287.5	6208617	27.8	8.0	2.02	4.0	3.0
2	JT NW	GB1305	358240.6	6208578	27.7	9.0	3.32	4.0	2.0
Ч	JT NW	GB1306	358186	6208508	27.4	7.0	2.85	5.0	2.0
5	JINW	GB2624	358231	6209041	28.5	6.0	0.72	3.0	2.0
	JINW	GB2625	358174	6208971	30.8	8.0	0.37	5.0	2.0
Y	JINW	GB2626	358105	6208914	29.2	7.0	1.13	4.3	2.0
A		GB2632	358192	6208730	29.0	8.0	4.86	6.0	2.0
		GB2633	358136	6208686	28.0	8.0	3.21	6.0	2.0
		GB2634	358222	6208789	31.0	9.0	1.32	7.0	2.0
-		GB2035	358297	6208856	30.0	8.0	2.03	4.0	3.0
5		GB2030	250320	6208919	29.5	6.0	2.07	3.7	2.0
		GB2037	250411	6206975	21.0	0.0	2.07	4.0	2.0
Y		GB2036	259500	6209038	21.0	0.0	1 01	5.0	2.0
		GB2039	220720	6208780	28.0	9.0	0.25	0.0	2.0
		GB2040	259402	6208785	20.9	0.0	2 / 2	5.7	2.0
		GB2041	350402	6200755	20 E	5.0	0.71	2 /	2.0
		GB2042	258522	6208645	28.3	6.0	2 21	2.4	2.0
┨		GB2045	350322	620043	20.0	7.0	0.21	2.4	2.0
		GR2645	358/12	6208447	20.0	5.0	0.31	3.0 2.7	2.0
┨		GR2643	358536	6208430	20.0	9.0 8.0	2.76	1.2	2.0
-		GP2640	350520	6200357	27.5	0.0 Q ()	2.70	4.5	2.0
┟		GB2049	358675	6208433	30.5	10.0	5 52	5.0	3.6
╞		GR2651	3586//	6208520	30.5	9.0	Δ 7Λ	5.0	2.0
ł	JT NW	GB2652	358643	6208530	30.0	9.0	2.9	5.0	3.0



		East	North	RL	Depth	E ve e	Interval	
Wireframe	Hole ID	(GDA94	(GDA94	(m ASI)	(m)	(m)	(m)	нм («)
When arrie		Z50)	Z50)		()		(III)	(%)
JT NW	GB2655	358909	6208330	29.1	8.0	3.28	5.0	2.0
JT NW	GB2656	358966	6208397	29.1	8.0	3.81	5.0	2.0
JT NW	GB2657	358964	6208266	29.5	8.0	4.28	5.0	2.0
JT NW	GB2665	359214	6208428	28.8	10.0	2.8	3.0	4.0
JT NW	GB2666	359159	6208356	28.6	10.0	3.38	5.0	2.0
JT NW	GB2667	359158	6208357	28.6	10.0	4.09	5.0	2.0
JT NW	GB2670	359072	6208504	28.8	7.0	2.25	4.0	2.0
JT NW	GB2672	359015	6208439	28.6	7.0	4.35	4.5	2.0
JT NW	GB2673	358912	6208568	29.2	8.0	3.04	5.0	2.4
JT NW	GB2674	358903	6208699	28.5	6.0	19.4	4.0	2.0
JT NW	GB2675	358879	6208751	28.5	6.0	5.34	3.8	2.0
JT NW	GB2679	358746	6208838	29.5	7.0	2.4	4.0	2.0
JT NW	GB2680	358582	6208705	29.5	7.0	2.76	4.0	2.6
JT NW	GB2681	358632	6208760	29.5	8.0	1.35	4.3	2.0
JT NW	GB2682	358508	6208852	31.0	8.0	1.38	5.7	2.0
JT W	GB1227	358626	6207596	25.8	8.0	3.0	3.0	2.9
W TL	GB1228	358571.4	6207544	25.9	12.0	4.0	3.0	4.4
W TL	GB1229	358515.4	6207486	24.7	12.0	3.0	4.0	2.9
JT W	GB1242	358856.8	6207149	24.2	9.0	4.0	3.0	3.9
JT W	GB1243	358905.7	6207201	24.2	9.0	3.0	3.0	6.1
JT W	GB1244	358967.5	6207265	24.6	7.0	3.0	3.0	3.1
JTW	GB1255	358128.1	6207772	25.4	9.0	4.0	3.0	4.1
JT W	GB1256	358169	6207831	25.6	9.0	4.0	3.0	4.1
JT W	GB1257	358230.5	6207885	25.7	9.0	4.0	3.0	2.2
W TL	GB1309	357831.7	6208161	21.5	9.0	4.0	5.0	3.3
JT W	GB1310	357780.3	6208109	20.4	8.0	5.0	3.0	3.8
JT W	GB2711	358640	6207440	24.8	8.0	4.0	3.9	3.9
JT W	GB2717	358849	6207396	23.5	6.0	3.0	2.2	3.3
JIW	GB2/18	358723	6207479	25.0	9.0	5.0	3.6	3.2
JT W	GB2720	358349	6207530	24.7	7.0	4.0	2.6	3.1
	GB2722	358401	6207595	24.9	9.0	5.5	2.0	3.4
	GB2723	358518	6207687	25.5	8.0	3.0	4.9	2.8
	GB2724	358481	6207601	27.0	10.0	6.0	3.8	4.3
	GB2728	358356	6207722	25.6	8.0	4.0	3.7	2.9
	GB2729	358312	6207733	26.1	9.0	6.0	4.0	4.8
	GB2738	358247	6207669	25.0	7.0	4.7	2.0	3.Z
	GB2739	358008	6207885	25.0	9.0	0.0	2.0	5
	GB2740	250U01	6207941	25.8 26.9	12.0	7.0	5.0	4.9
	GB2741	338133	620/994	20.8	12.0	4.0	0.U	2.8
	GB2742	25730/	6208103	25.0	0.0	3.0	5.4	3
	GD2745	357745	6200297	20.1	9.0	2.0	4.0	5 2 7
	GB2740	257093	6208242	20.0	12.0	5.0	0.5 6.0	3./
		257/38 25700C	6208012	20.7	10.0	0.0	0.0	2.0
	GB2749	257015	6207928	27.0	10.0	/.4	2.0	2.8
JIVV	062751	22/212	0207632	24.5	7.0	4./	2.0	5.9
Southeast	GB0991	356875	6208564	26.0	15.0	9.0	4.0	3.8



Wireframe	Hole ID	East (GDA94 Z50)	North (GDA94 Z50)	RL (m ASL)	Depth (m)	From (m)	Interval (m)	HM (%)
Southeast	GB0992	356933	6208616	26.2	15.0	8.0	4.0	4.3
Southeast	GB0993	356989	6208675	27.2	15.0	7.0	6.0	4.1
Southeast	GB0997	357385	6208401	26.2	14.0	7.0	5.0	3.3
Southeast	GB0998	357329	6208338	26.2	15.0	8.0	4.0	4.0