

5 April 2023



KASIYA INDICATED RESOURCE INCREASED BY OVER 80%

- Kasiya Indicated Resource now stands at 1.2 Billion tonnes at 1.0% rutile and 1.5% graphite
- Updated Mineral Resource Estimate (MRE) moves over 0.5 Billion tonnes from Inferred to Indicated – an increase of 81% to the Indicated category
- Over 66% of total MRE now in the Indicated category
- Kasiya's global MRE over 1.8 Billion tonnes at 1.0% rutile and 1.4% graphite
- Kasiya remains the <u>world's largest natural rutile deposit and second largest flake graphite</u> <u>deposit</u>
 - Updated MRE to underpin the mining inventory and mine plan for the forthcoming Prefeasibility Study (PFS)

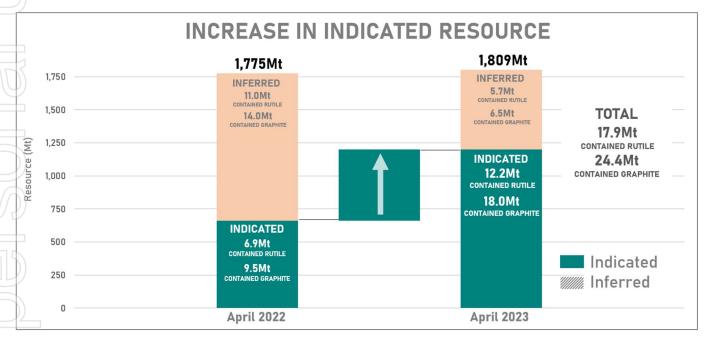


Figure 1: Increase in Kasiya's Indicated Resources compared MRE update released in April 2022

Sovereign's Managing Director Dr Julian Stephens commented: "The increase of over 80% in the Indicated component at a one-for-one conversion from Inferred is an outstanding outcome. The conversion rate confirms the very consistent geological and grade continuity and is testament to the high-quality and robustness of the deposit. Kasiya is poised to become a major long-term supplier of the critical minerals natural rutile and graphite, with both forecast to be in near-term and significant supply deficit. The PFS work program on this highly strategic and globally significant project is progressing well and approaching its final stages. The Company is looking forward to presenting the outcomes of the PFS in the coming months."

ENQUIRIES

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KASIYA - THE LARGEST RUTILE DEPOSIT IN THE WORLD

Sovereign Metals Limited (ASX:SVM; AIM:SVML) (the Company or Sovereign) is pleased to announce the updated MRE for its world-class Kasiya rutile-graphite deposit in Malawi. Kasiya is a Tier 1 deposit and a potential major source of low carbon footprint critical minerals natural rutile (TiO₂) and graphite.

Table 1: Kasiya Total Indicated + Inferred Mineral Resource Estimate at 0.7% rutile cut-off grade					
Classification	Resource (Mt)	Rutile Grade (%)	Contained Rutile (Mt)	Graphite Grade (TGC) (%)	Contained Graphite (Mt)
Indicated	1,200	1.0%	12.2	1.5%	18.0
Inferred	609	0.9%	5.7	1.1%	6.5
Total	1,809	1.0%	17.9	1.4%	24.4

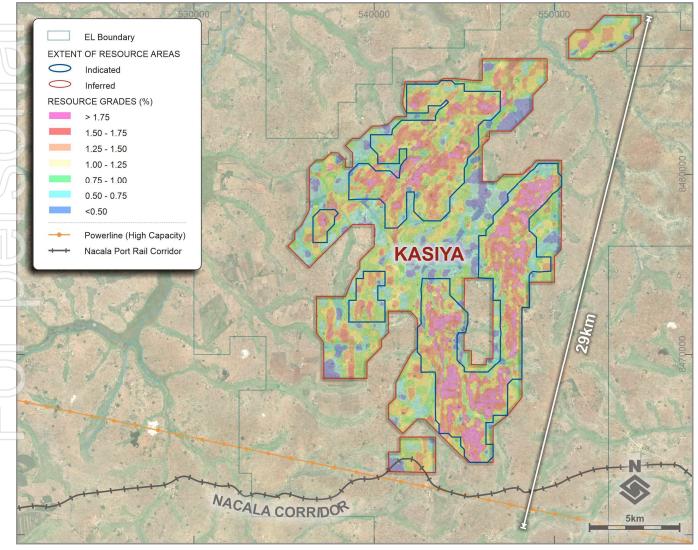


Figure 2: Kasiya map showing rutile grades of the upper blocks of the MRE block model

The updated MRE has further defined broad and contiguous zones of high-grade rutile and graphite which occur across a very large area of over 201km² (Figure 3). Rutile mineralisation is concentrated in laterally extensive, near surface, flat "blanket" style bodies in areas where the weathering profile is preserved and not significantly eroded. Graphite is depleted near surface with grades improving at depths generally >4m to the base of the saprolite zone which averages about 22m.

Sovereign's 2022 drill program at Kasiya used push tube (PT) core holes to in-fill and convert Inferred mineralisation into the Indicated category. The consistency and robustness of the geology allowed for an efficient conversion of this previously Inferred material on a near-identical one-for-one basis to the Indicated category.

A total of 66% of the MRE now reports to the Indicated category @ 1.0% rutile and 1.5% TGC - up from 33% previously. Overall, the new Indicated components show coherent, broad bodies of mineralisation that have coalesced very well with the additional infill drilling results.

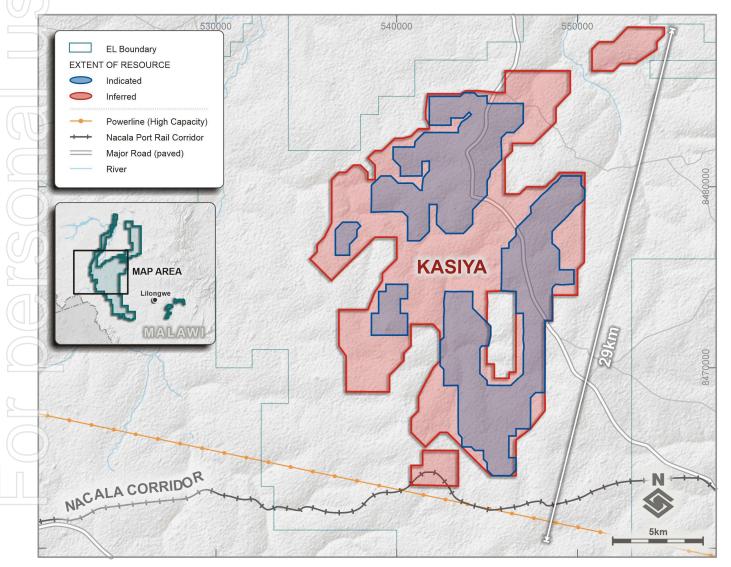


Figure 3: Kasiya MRE footprint showing the Indicated and Inferred zones.

Further advancement in this MRE update was the application of air-core (AC) drilling to define the depth of mineralisation in a number of selected higher-grade areas. As expected, this drilling shows that high-grade rutile and graphite mineralisation extends to the base of the soft saprolite unit terminating on the saprock basement averaging about 22m depth. This AC drilling targeted early-scheduled mining pits mainly in the southern areas of the MRE footprint.

A number of higher-grade graphite zones at depth were identified which are generally associated with higher grade rutile at surface. Some of these zones have graphite grades at depths >6m in the 4% to 8%. TGC range and appear to represent significant contained coarse flake graphite tonnages (see Figure 4).

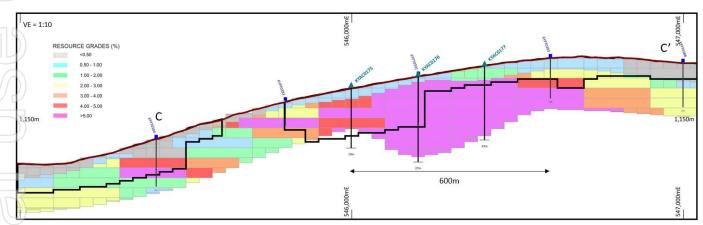


Figure 4: C-C' cross-section from the southern part of the MRE block model in a higher-grade graphite zone showing colouring by graphite grade (TGC) with previous ESS pit shapes also shown. Refer Figure 5.

The highlighted cut-off of 0.7% rutile presents 1.8 billion tonnes at a rutile grade of 1.0%. (Table 2). The overall recovered rutile equivalent grade for the MRE at the global 0.7% cut-off is 1.65% RutEq*.

Table 2: Kasiya To	Table 2: Kasiya Total Indicated + Inferred Mineral Resource Estimate at various rutile cut-off grades					
Cut-off (rutile)	Resource (Mt)	Rutile Grade (%)	Contained Rutile (Mt)	Graphite Grade (%)	Contained Graphite (Mt)	
0.40%	3,215	0.80%	25.7	1.30%	41.9	
0.50%	2,779	0.85%	23.8	1.35%	37.4	
0.60%	2,304	0.92%	21.1	1.37%	31.7	
0.70%	1,809	0.99%	17.9	1.35%	24.4	
0.80%	1,335	1.08%	14.4	1.25%	16.6	
0.90%	934	1.17%	11.0	1.06%	9.9	
1.00%	643	1.28%	8.2	0.84%	5.4	
1.10%	449	1.38%	6.2	0.65%	2.9	
1.20%	324	1.47%	4.7	0.53%	1.7	
1.30%	230	1.56%	3.6	0.48%	1.1	
1.40%	163	1.64%	2.7	0.45%	0.7	

^{*} RutEq. Formula: Rutile Grade x Recovery (98%) x Rutile Price (US\$1,308/t) + Graphite Grade x Recovery (62%) x Graphite Price (US\$1,085/t) / Rutile Price (US\$1,308/t). All assumptions are taken from the Expanded Scoping Study (ESS) released in June 2022.



KASIYA MRE TECHNICAL DETAILS

The Kasiya MRE has been prepared by independent consultants, Placer Consulting Pty Ltd (**Placer**) and is reported in accordance with the JORC Code (2012 Edition).

Rutile mineralisation lies in laterally extensive, near surface, flat "blanket" style bodies in areas where the weathering profile is preserved and not significantly eroded. The high-grade zones are relatively geologically consistent with limited variability along and across strike. The mineralisation style is illustrated best in Figures 5 & 6 below.

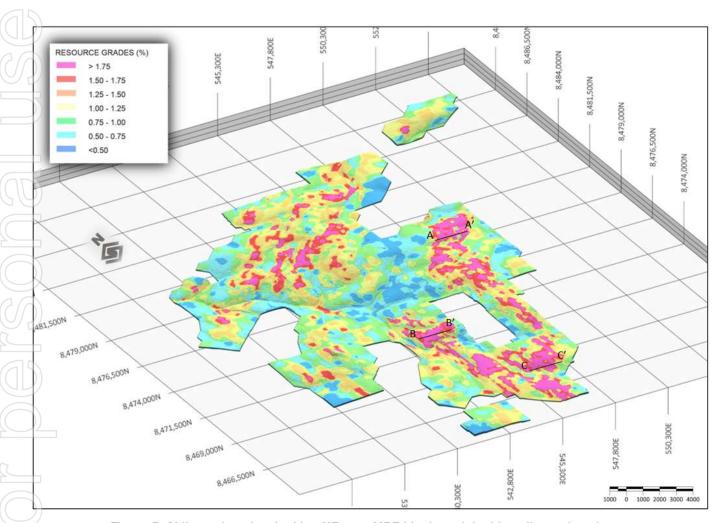


Figure 5: Oblique plan view looking NE over MRE block model with rutile grades shown.



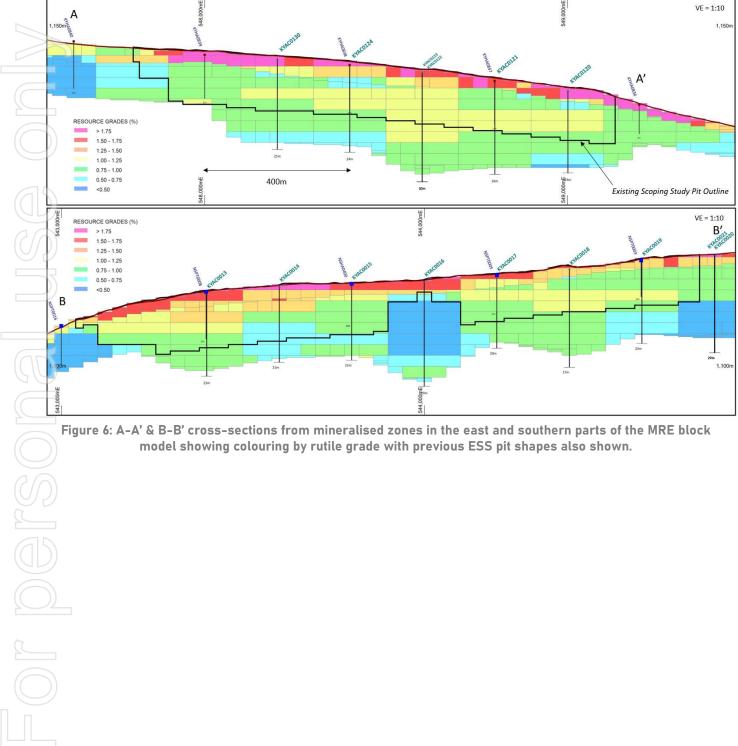


Figure 6: A-A' & B-B' cross-sections from mineralised zones in the east and southern parts of the MRE block model showing colouring by rutile grade with previous ESS pit shapes also shown.



SUMMARY OF RESOURCE ESTIMATE REPORTING CRITERA

As per ASX Listing Rule 5.8 and the 2012 JORC reporting guidelines, a summary of the material information used to estimate the MRE is detailed below.

Geology

Regional Geology

The greater part of Malawi is underlain by crystalline Precambrian to lower Palaeozoic rocks referred to as the Malawi Basement Complex. In some parts these rocks have been overlain unconformably by sedimentary and volcanic rocks ranging in age from Permo-Triassic to Quaternary. The Basement complex has undergone a prolonged structural and metamorphic history dominated by uplift and faulting resulting in the formation of the Malawi Rift Valley.

Kasiya is located on the Lilongwe Plain which is underlain by the Basement Complex paragneisses and orthogneisses which are part of the Mozambique Belt. The bulk of the gneisses are semi-pelitic but there are bands of psammitic and calcareous rocks that have been metamorphosed under high pressure and temperature conditions to granulite facies. Interspersed within the paragneiss units are lesser orthogneisses, often cropping out as conspicuous tors, as well as amphibolites, pegmatites and minor mafic to ultramafic intrusions. Foliation and banding in the gneisses have a broad north-south strike over the general area. Thick residual soils and pedolith with some alluvium overlie the gneisses and include sandy, lateritic and dambo types.



Figure 7: Drone photo above the Kasiya Deposit showing the open, flat terrain



Project Geology

Sovereign's tenure covers 1,386km² over an area to the north, west and south of Malawi's capital city covering the Lilongwe Plain. The topography is generally flat to gently undulating and the underlying geology is dominated by paragneiss with pelitic, psammitic and calcareous units.

A particular paragneiss unit is rich in rutile and graphite and is the primary source of both of these minerals in the area. This area was deeply weathered during the Tertiary and rutile concentrated in the upper part of the weathering profile forming residual placers, such as the Kasiya Deposit. Once this material is incised and eroded, it is transported and deposited into wide, regional braided river systems forming alluvial heavy mineral placers such as the Bua Channel.

Kasiya Deposit Geology

The high-grade rutile deposit at Kasiya is best described as a residual placer, or otherwise known as eluvial heavy mineral deposit. It is formed by weathering of the primary host rock and concentration in place of heavy minerals, as opposed to the high-energy transport and concentration of heavy minerals in a traditional placer.

The presence of abundant kyanite and graphite in the host material suggest a meta-sedimentary protolith. The protolith likely started with a 0.5-1.5Ga basin that also experienced consistent influx of titanium minerals.

These sedimentary rocks were subject to granulite facies metamorphism under reduced conditions in the Pan-African Orogeny. The metamorphic facies, reduced environment, relatively high titanium content and low iron content resulted in rutile being the most stable titanium mineral under these conditions. Slow exhumation and cooling then resulted in re-crystallisation as paragneisses containing coarse rutile and graphite.

The final and most important stage of rutile enrichment came as tropical weathering during the Tertiary depleted the top ~8m of physically and chemically mobile minerals. This caused significant volume loss and concurrent concentration of heavy resistate minerals including rutile and kyanite.

Rutile mineralisation therefore lies in laterally extensive, near surface, flat "blanket" style bodies in areas where the weathering profile is preserved. The Kasiya deposit shows widespread, high-grade mineralisation commonly grading 1.2% to 2.0% rutile in the top 3-5m from surface. Moderate grade mineralisation generally grading 0.5% to 1.2% rutile commonly extends from 5m to the base of the soft saprolite unit to generally 20-30m depth where it terminates on the hard saprock basement.

Graphite generally occurs in broad association with rutile. However, it is depleted in the top 3-5m and therefore can often show an inverse grade relationship with rutile in the near-surface zones. At depths generally greater than 5m, graphite is not depleted, and rutile is not particularly enriched, so a more consistent grade relationship exists.



Drilling Techniques

Spiral hand-auger (HA) drilling and Push-tube core (PT) drilling has been used extensively at the Kasiya Deposit by Sovereign to define mineralisation and to obtain quantitative rutile and graphite (TGC) assay information. For the MRE update, Aircore (AC) drilling has been applied in some high-grade areas to determine rutile and graphite grade potential at depth and to establish basement elevation and composition. Additional HA and PT drilling has been applied to extend, infill and upgrade resource confidence in more prospective regions.

A further 152 HA holes for 1,253m were drilled to extend the Kasiya Rutile Deposit and to obtain samples for quantitative determination of recoverable rutile and TGC. The total HA dataset incorporated in the MRE update is now 1,357 holes for 12,643m.

HA drilling was executed by Sovereign field teams using a manually operated enclosed-flight Spiral Auger (SP / SOS) system produced by Dormer Engineering in Queensland, Australia. The HA bits are 62mm and 75mm in diameter with 1m long steel rods. Each 1m of drill advance is withdrawn and the contents of the auger flight removed into bags and set aside. An additional 1m steel rod is attached and the open hole is re-entered to drill the next metre. This is repeated until the drill hole is terminated often due to the water table being reached, and more rarely due to bit refusal (2% of the resource HA drill database). The auger bits and flights are cleaned between each metre of sampling to avoid contamination.

The HA collars are nominally spaced at a 400m-by-400m spaced array with the PT holes similarly spaced at an offset, infill grid. This results in a 200m by 200m drill spacing (to the strike orientation of the deposit).

PT drilling is undertaken using a drop hammer Dando Terrier MK1 and a drop hammer DL650 by Geoconsult and Thompsons Drilling. A total of 488 holes for 4,669m contribute to the MRE. The drilling generated 1m runs of 83mm PQ core in the first 2m and then transition to 72mm core for the remainder of the hole. Core drilling is oriented vertically by spirit level.



Figure 8: Air-core (AC) drilling at Kasiya in May 2022.



A total of 182 AC holes for 4,404m were completed in six locations across the MRE deemed likely to fall into mining pit areas.

AC drilling was completed by Thompson Drilling utilising a Smith Capital 10R3H compact track-mounted drill. The drilling is vertical and generates 1m samples with care taken in the top metres to ensure good recoveries of the high-grade surface material. To achieve this the bit is initially pushed down ~200mm then air is slowly introduced with slow rotation rpm, once sample begins flowing freely air and rpm is increased to full volume as the hole deepens. Whilst sample size was reduced in surface samples, there was insignificant bias attributed to the AC method when compared with results from a dedicated programme of twin PT holes.

The AC sample is collected by the on-board cyclone into heavy-duty RC sample bags. Drilling continues until bit refusal onto basement ~20-30m. Sample bags are immediately transported back to Sovereign's field laydown yard where they are processed.

AC drilling is on a nominal 200m by 200m pattern. The drill spacing is deemed to adequately define the mineralisation in the MRE. There is no apparent bias arising from the orientation of the drill holes contributing to the MRE, with respect to the orientation of the deposit.

The drilling programs to date show a mineralised envelope, defined nominally by 0.7% rutile cut-off, of approximately 201km² with numerous areas of high-grade rutile and graphite defined.

The PT and AC twin and density sample holes are selectively placed throughout the deposit to ensure a broad geographical and lithological coverage for the analysis.

Placer has reviewed Standard Operating Procedures (SOPs) for HA, PT and AC drilling and found them to be fit for purpose and support the resource classifications as applied to the MRE.



Figure 9: Core drilling (push tube) in action at Kasiya



Sampling Techniques

HA samples are obtained at 1m intervals generating on average approximately 2.5kg of drill sample. HA samples are manually removed from the auger bit and sample recovery is visually assessed in the field. As samples become wet at the water table and recovery per metre declines, the drill hole is terminated.

Each 1m sample is sun dried, logged and weighed. HA samples are composited based on regolith weathering boundaries defined by expert logging. Each 1m of sample is dried, lightly pressed to remove soft aggregates and riffle-split to generate a total sample weight of 3kg for analysis, generally at 2 - 5m intervals (average 2.8m for the total resource drill database). This primary sample is then riffle split again to provide a 1.5kg sample each for rutile and graphite analyses.

PT samples are predominantly from HQ sized core (63.5mm diameter). Half core 1m samples are sun dried, logged and weighed. Samples are then lightly pressed and composited over 2m intervals. An equal mass is taken from each contributing metre to generate a 1.5kg composite sample. Individual recoveries of core samples are recorded on a quantitative basis. Core recovery is very good overall at >95%.

AC samples are collected in 1m increments. AC samples are dried, riffle split, lightly pressed and composited. Samples are collected and homogenised prior to splitting to ensure sample representivity. 1.5kg composite samples defined by the regolith boundaries are processed. An equivalent mass is taken from each primary sample to make up the composite.

This sampling and compositing method is considered appropriate and reliable based on accepted industry practice. Placer completed an on-site audit of sampling and sample processing and deemed the processes fit for purpose. Minor suggested sampling and processing adjustments were implemented.

Sample analysis methodology

All samples arrive at Sovereign's Malawi laboratory where they are sorted and checked in. Graphite samples are identified and prepared for export, while the equivalent rutile samples begin the sample workflow prior to export to Perth, Western Australia. Audit of the laboratory premises, staff, sample analysis and QA procedures were highly commended during the audit by Placer Consulting in 2022.

Rutile

Samples are dried in a commercial oven for 1 hour at 105°C and a dry raw samples mass is recorded.

Samples are soaked in 1% TSPP solution overnight and then lightly agitated prior to wet screening.

Wet screening occurs at 5mm, $600\mu m$ and $45\mu m$ to remove oversize and slimes (-45 μm) material. Each +45 μm retained fraction is dried, logged and weighed.

The resulting SAND fraction +45 μ m -600mm is oven dried for 1 hour at 105°C after which its dry weight is recorded.

The SAND fraction is then passed over a Gemeni wet shaking table at a constant feed rate to generate a heavy mineral concentrate (HMC).



Heavy Liquid Separation (**HLS**) at Diamantina Laboratories in Perth was initially trialled as a preferred separation method but was quickly superseded (supported by QA analysis) by wet-table separation on account of substantial near-density gangue material reporting to the HM sink for the HLS technique. The HLS analyses represent 11% of the MRE assay dataset.

The wet-tabled HMC is then subject to magnetic separation @ 16,800G (2.9Amps) producing a magnetic (M) and non-magnetic (NM) fraction. The separation is performed using a Mineral Technologies Reading Pilot IRM (Induced Roll Magnetic) purchased by Sovereign and located at the Company's laboratory in Malawi. Pre-2022 this step was completed by Allied Mineral Laboratories Perth (AML) in Perth, Western Australia.

The Malawi onsite laboratory sample preparation methods are considered quantitative to the point where the NM concentrate (containing the rutile) is produced.

The routine NM fractions are air freighted to ALS Metallurgy Perth for quantitative XRF analysis. The samples receive the XRF_MS sample suite which includes TiO_2 and common impurities. Check QAQC samples are sent to Intertek Perth where they receive and equivalent standard mineral sands suite FB1/XRF72.

Several generations of QEMSCAN analysis of the NM and MAG fractions performed at ALS Metallurgy show dominantly clean and liberated rutile grains and confirm rutile is the only titanium species in the NM fraction.

Recovered rutile is defined and reported here as: TiO₂ recovered in the SAND +45 to -600um range to the NM concentrate fraction as a % of the total primary, dry, raw sample mass divided by 95% (to represent an approximation of final product specifications). i.e recoverable rutile within the whole sample. Raw rutile results are also available.

Graphite

Once secured samples arrive at Intertek Johannesburg, South Africa, a split of each raw sample is dissolved in dilute hydrochloric acid to liberate carbonate carbon. The solution is filtered using a filter paper and the collected residue is then dried to 425°C in a muffle oven to drive off organic carbon. The dried sample is transported to Perth, Australia where it is then combusted in an Eltra CS-800 induction furnace infra-red CS analyser to yield total graphitic or elemental carbon (TGC).

QAQC

Accuracy monitoring is achieved through submission of certified reference materials (**CRM's**). Sovereign uses internal and externally sourced wet screening reference material inserted into samples batches at a rate of 1 in 20. The externally sourced, certified standard reference material for HM and Slimes assessment is provided by Placer Consulting.

ALS and Intertek both use internal CRMs and duplicates on XRF and TGC analyses. Sovereign also inserts its customised CRMs into all sample batches at a rate of 1 in 20.

Analysis of sample duplicates is undertaken by standard geostatistical methodologies (Scatter, Pair Difference and QQ Plots) to test for bias and to ensure that sample splitting is representative. Standards determine assay accuracy performance, monitored on control charts, where failure (beyond 2SD from the mean) initiates investigation and may trigger re-processing of the affected batch.



Precision and accuracy assessment has been completed on all alternate workflow methodologies and a consistent method has been decided, in consultation with Placer Resource Geologists. Examination of the QA/QC sample data indicates satisfactory performance of field sampling protocols and assay laboratories providing acceptable levels of precision and accuracy. Rutile determination by alternate methods showed no observable bias.

Acceptable levels of accuracy and precision are displayed in geostatistical analyses to support the resource classifications as applied to the estimate.

Classification

A nominal 200m-by-200m-by-2m drill sample array is deemed to adequately define the Indicated mineralisation for the MRE, with a predictable grade distribution and consistent host stratigraphy.

The PT twin and density sample holes are selectively placed throughout the deposit to ensure a broad geographical and lithological spread of material types for the analysis.

Renewed kriging neighbourhood analysis, completed using Supervisor software, has confirmed the drill and sample spacing applied to the MRE update. Variography has also confirmed the optimal search distances and orientations. Based on these results and the experience of the Competent Person, the data spacing, and distribution is considered adequate for the definition of mineralisation classification and adequate for the MRE.

The HA and PT drilling methods applied to define the Kasiya Deposit (HA and PT) are not able to retrieve reliable samples once the bit is 3 to 5m below the water table and each terminate at an average depth of about 9.5m in the resource dataset. Application of AC drilling has confirmed the continuation of material rutile and graphite grade to depth and defined the basement horizon at the saprock interface. Elsewhere, mineralisation remains open at depth and substantial additional tonnages could be anticipated.

High grade sample results are constrained adequately by the search parameters and interpolation method applied to the MRE. High-grade results are confirmed by an audit analysis program.

Regolith stratigraphy is uniform and rutile and graphite mineralisation is predictable across the Kasiya Deposit. Open-hole drilling and infill PT/AC drilling techniques have been expertly applied and data collection procedures, density assessments, QA protocols and interpretations conform to industry best practice.

Assay, mineralogical determinations and metallurgical test work conform to industry best practice and demonstrate a rigorous assessment of product and procedure. These and the development of a conventional processing flowsheet and marketability studies support the classification of the Kasiya Resource.

Estimation Methodology

Datamine Studio RM and Supervisor software are used for the data analysis, variography, geological interpretation and resource estimation. Key fields are interpolated into the volume model using a range of parameters and interpolation methods to establish best fit for the deposit. For the Kasiya MRE update, the Inverse Distance weighting (power 4) method was seen to perform a superior interpolation of informing data and replication of the high-value and thin, surface (SOIL/FERP) grade distribution. This was assisted by the application of a Dynamic Anisotropy search, informed by the results of variography. Suitable limitations on the number of samples and the impact of those samples, was maintained.



Interpolation was constrained by hard boundary domains that result from the geological interpretation. The construction of an upper soil ("SOIL" 0-1m) and ferruginous pedolith ("FERP", 1-4m) domain referred to as the Soil/Ferp domain reduces the dilution of resource grade from the underlying, less mineralised mottled ("MOTT", 4-7m), pallid saprolite ("PSAP", 7-9m) and saprolite ("SAPL", 9-25m) or collectively the Mott/Sapl domain.

A Topsoil horizon has been defined at 0.3m thickness throughout the Indicated Resource area to support anticipated ore reserve calculation and mining studies. Topsoil is disclosed separately but remains in the MRE in recognition of advanced investigations by SVM on synthetic topsoil generation for rehabilitation.

The average parent cell size used is equivalent to the average drill hole spacing within the Indicated Resource (200m*200m). Cell size in the Z-axis was established to cater for the composite sample spacing and definition of the Topsoil domain. This resulted in a parent cell size of 200m x 200m x 3m for the volume model with 5 sub-cell splits available in the X and Y axes and 10 in the Z axis to smooth topographical and lithological transitions.

Both parent and sub-cell interpolations were completed and reconciled spatially against each other. The parent cell and sub cell interpolations produced near identical global tonnages and grades. The sub-cell interpolation was seen to provide a better graduation of informing drill hole data through intermediate model cells and to conform more sympathetically to the geological interpretation. Whilst both are available, in this instance and as a geological resource, the sub-cell interpolation was applied to the MRE.

The resource model has been constrained by the drill array plus one drill interval. This applies a buffer of 200*200*2.7m in X, Y and Z axes. Only those areas drilled by AC allow the accurate generation of a basement horizon, elsewhere the base of the MRE hovers within the saprolite and reflects only the depth of effective drilling by HA and PT methods where they terminate due to excess water ingress. Substantial additional mineralisation is anticipated below this depth in these areas, as demonstrated by the limited AC drilling to date.

Extreme grade values were not identified by statistical analysis, nor were they anticipated in this style of deposit. No top cut is applied to rutile or graphite in the resource estimation.

Validation of each interpolation method and of the reported grade interpolation was done visually in Datamine by loading model and drill hole files and annotating, colouring and using filtering to check for the appropriateness of drill data interpolation.

Statistical distributions were prepared for model zones from both the drill hole file and the model to assess how well the interpolation represents informing data. Model-drilling reconciliation was also performed by generating swath plots to measure drilling support against interpolation performance in all three primary orientations. Where data population is adequate, the resource model has effectively averaged informing drill hole data and is considered suitable to support the resource classifications as applied to the estimate.

Density is determined on a 10cm segment of complete core through a simple cylinder volume calculation on both wet in-situ weight and an oven dry weight. The in-situ state of the core is carefully preserved prior to selection. After the segment is chosen, it undergoes measurement and weighing. Subsequently, it is subjected to oven-drying for a specific duration, and its weight is once again determined. This method is applied to samples that represent different weathering domains found in various drill holes throughout the project site.

This methodology delivers an accurate density result that is interpolated in the MRE for each host material type.



Density data are applied to the resource estimate by weathering domain. Minor adjustments were made for the MRE update on the receipt of additional density data. Averaged density results of 1.39 t/m³ for the soil (SOIL) domain, 1.58 t/m³ for the ferruginous pedolith (FERP) domain, 1.66 t/m³ for the mottled (MOTT) domain, 1.69 t/m³ for the pallid saprolite (PSAP) domain, 1.97 t/m³ for the saprolite (SAPL) domain and 1.95 t/m³ for the laterite (LAT) domain were calculated. Density data are interpolated into the resource estimate by the nearest neighbour method.

Cut-off Grades

All results reported are of a length-weighted average of in-situ grades. The resource is reported at a range of bottom cut-off grades in recognition that optimisation and financial assessment is in process.

A nominal bottom cut of 0.7% rutile is offered, based on preliminary assessment of resource product value and anticipated cost of operations. As a by-product of a rutile operation, graphite is not considered for top or bottom cuts.

Mining and Metallurgy Factors

Hydro-mining has been determined as the optimal method of mining for the Kasiya Rutile deposit. The material is loose, soft, fine and friable with no cemented sand or dense clay layers rendering it amenable to hydro-mining. It is considered that the strip ratio would be zero or near zero.

Dilution is considered to be minimal as mineralisation commonly occurs from surface and mineralisation is generally gradational with few sharp boundaries.

Recovery parameters have not been factored into the estimate. However, the valuable minerals are readily separable due to their SG differential and are expected to have a high recovery through the proposed conventional wet concentration plant, as demonstrated by metallurgical test work.

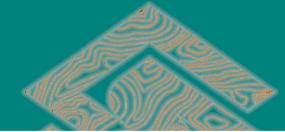
Sovereign has announced three sets of metallurgical results to the market (24 June 2019, 9 September 2020 and 7 December 2021), relating to the Company's ability to produce a high-grade rutile product with a high recovery via simple conventional processing methods. Sovereign engaged AML to conduct the metallurgical test work and develop a flowsheet for plant design considerations. The work has shown a premium quality rutile product ranging from 95.0% to 97.2% TiO_2 with low impurities could be produced with recoveries of about 94% to 100% and with favourable product sizing at d50 of 118 μ m (Kasiya North) and 128 μ m (Kasiya South).

Gravity separation was effective at concentrating graphite to a "light mineral pre-concentrate" due to its low specific gravity (~2.2 t/m³) providing an upgrade of graphite grade to the flotation circuit to about three times the run of mine grade.

A program at SGS Lakefield in Canada was undertaken in order to confirm that the graphite gravity preconcentrate can be upgraded into a coarse flake graphite by-product via a conventional graphite flotation flowsheet.

The test-work was extremely successful, and a very coarse-flake graphite concentrate at 96.3% TGC was produced. Greater than 60% of the graphite concentrate is in the large to super-jumbo fractions, suggesting a high combined basket value. The overall graphite recovery from the raw sample to product was 62%.

Further graphite flotation testwork to define the PFS flowsheet has been undertaken at ALS in Perth, Western Australia. Test work results are being finalised, however as with all other Kasiya metallurgical test work to date, minimal variation is expected from previous results.



MRE TABLES

Table 5: Indicated MRE at various rutile cut-offs					
Cut-off (rutile)	Resource (Mt)	Rutile Grade (%)	Contained Rutile (Mt)	Graphite Grade (%)	Contained Graphite (Mt)
0.40%	1,840	0.86	15.8	1.48	27.3
0.50%	1,673	0.90	15.0	1.51	25.2
0.60%	1,463	0.95	13.9	1.53	22.3
0.70%	1,200	1.01	12.2	1.50	18.0
0.80%	906	1.10	10.0	1.37	12.4
0.90%	645	1.20	7.7	1.15	7.4
1.00%	452	1.31	5.9	0.88	4.0
1.10%	327	1.41	4.6	0.65	2.1
1.20%	246	1.50	3.7	0.52	1.3
1.30%	185	1.58	2.9	0.47	0.9
1.40%	139	1.66	2.3	0.44	0.6

Cut-off (rutile)	Resource (Mt)	Rutile Grade (%)	Contained Rutile (Mt)	Graphite Grade (%)	Contained Graphite (Mt)
0.40%	1,840	0.86	15.8	1.48	27.3
0.50%	1,673	0.90	15.0	1.51	25.2
0.60%	1,463	0.95	13.9	1.53	22.3
0.70%	1,200	1.01	12.2	1.50	18.0
0.80%	906	1.10	10.0	1.37	12.4
0.90%	645	1.20	7.7	1.15	7.4
1.00%	452	1.31	5.9	0.88	4.0
1.10%	327	1.41	4.6	0.65	2.1
1.20%	246	1.50	3.7	0.52	1.3
1.30%	185	1.58	2.9	0.47	0.9
1.40% Table 6: Inferred M	139 IRE at various rut	1.66 ile cut-offs	2.3	0.44	0.6
			2.3 Contained Rutile (Mt)	0.44 Graphite Grade (%)	Contained
Table 6: Inferred M	IRE at various rut Resource	ile cut-offs Rutile Grade	Contained Rutile	Graphite Grade	Contained Graphite
Table 6: Inferred M	IRE at various rut Resource (Mt)	ile cut-offs Rutile Grade (%)	Contained Rutile (Mt)	Graphite Grade (%)	Contained Graphite (Mt)
Table 6: Inferred M Cut-off (rutile) 0.40%	IRE at various rut Resource (Mt) 1,375	ile cut-offs Rutile Grade (%) 0.72	Contained Rutile (Mt) 9.9	Graphite Grade (%) 1.06	Contained Graphite (Mt) 14.6
Table 6: Inferred M Cut-off (rutile) 0.40% 0.50%	IRE at various rut Resource (Mt) 1,375 1,106	ile cut-offs Rutile Grade (%) 0.72 0.79	Contained Rutile (Mt) 9.9 8.7	Graphite Grade (%) 1.06 1.10	Contained Graphite (Mt) 14.6 12.2
Table 6: Inferred M Cut-off (rutile) 0.40% 0.50% 0.60%	Resource (Mt) 1,375 1,106	ile cut-offs Rutile Grade (%) 0.72 0.79 0.86	Contained Rutile (Mt) 9.9 8.7 7.3	Graphite Grade (%) 1.06 1.10 1.11	Contained Graphite (Mt) 14.6 12.2 9.4
Table 6: Inferred M Cut-off (rutile) 0.40% 0.50% 0.60% 0.70%	Resource (Mt) 1,375 1,106 841 609	ile cut-offs Rutile Grade (%) 0.72 0.79 0.86 0.94	Contained Rutile (Mt) 9.9 8.7 7.3 5.7	Graphite Grade (%) 1.06 1.10 1.11 1.06	Contained Graphite (Mt) 14.6 12.2 9.4 6.5
Table 6: Inferred M Cut-off (rutile) 0.40% 0.50% 0.60% 0.70% 0.80%	Resource (Mt) 1,375 1,106 841 609 429	ile cut-offs Rutile Grade (%) 0.72 0.79 0.86 0.94 1.03	Contained Rutile (Mt) 9.9 8.7 7.3 5.7 4.4	Graphite Grade (%) 1.06 1.10 1.11 1.06 0.98	Contained Graphite (Mt) 14.6 12.2 9.4 6.5
Table 6: Inferred M Cut-off (rutile) 0.40% 0.50% 0.60% 0.70% 0.80% 0.90%	Resource (Mt) 1,375 1,106 841 609 429 290	ile cut-offs Rutile Grade (%) 0.72 0.79 0.86 0.94 1.03 1.11	Contained Rutile (Mt) 9.9 8.7 7.3 5.7 4.4 3.2	Graphite Grade (%) 1.06 1.10 1.11 1.06 0.98 0.86	Contained Graphite (Mt) 14.6 12.2 9.4 6.5 4.2 2.5
Table 6: Inferred M Cut-off (rutile) 0.40% 0.50% 0.60% 0.70% 0.80% 0.90% 1.00%	Resource (Mt) 1,375 1,106 841 609 429 290 190	ile cut-offs Rutile Grade (%) 0.72 0.79 0.86 0.94 1.03 1.11 1.20	Contained Rutile (Mt) 9.9 8.7 7.3 5.7 4.4 3.2 2.3	Graphite Grade (%) 1.06 1.10 1.11 1.06 0.98 0.86 0.74	Contained Graphite (Mt) 14.6 12.2 9.4 6.5 4.2 2.5 1.4
Table 6: Inferred M Cut-off (rutile) 0.40% 0.50% 0.60% 0.70% 0.80% 0.90% 1.00% 1.10%	Resource (Mt) 1,375 1,106 841 609 429 290 190 122	ile cut-offs Rutile Grade (%) 0.72 0.79 0.86 0.94 1.03 1.11 1.20 1.29	Contained Rutile (Mt) 9.9 8.7 7.3 5.7 4.4 3.2 2.3 1.6	Graphite Grade (%) 1.06 1.10 1.11 1.06 0.98 0.86 0.74 0.64	Contained Graphite (Mt) 14.6 12.2 9.4 6.5 4.2 2.5 1.4 0.8



Table 7: Inferred	Table 7: Inferred & Indicated MRE at various rutile cut-offs						
Cut-off (rutile)	Resource (Mt)	Rutile Grade (%)	Contained Rutile (Mt)	Graphite Grade (%)	Contained Graphite (Mt)		
0.40%	3,215	0.80	25.7	1.30	41.9		
0.50%	2,779	0.85	23.8	1.35	37.4		
0.60%	2,304	0.92	21.1	1.37	31.7		
0.70%	1,809	0.99	17.9	1.35	24.4		
0.80%	1,335	1.08	14.4	1.25	16.6		
0.90%	934	1.17	11.0	1.06	9.9		
1.00%	643	1.28	8.2	0.84	5.4		
1.10%	449	1.38	6.2	0.65	2.9		
1.20%	324	1.47	4.7	0.53	1.7		
1.30%	230	1.56	3.6	0.48	1.1		
1.40%	163	1.64	2.7	0.45	0.7		

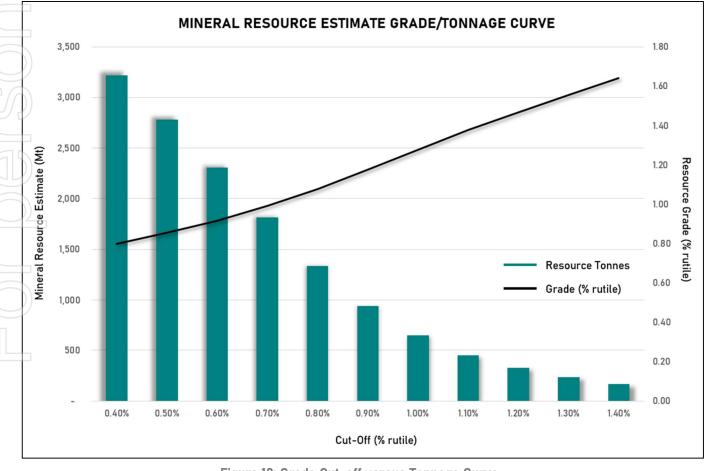


Figure 10: Grade Cut-off versus Tonnage Curve.



Forward Looking Statement

This release may include forward-looking statements, which may be identified by words such as "expects", "anticipates", "believes", "projects", "plans", and similar expressions. These forward-looking statements are based on Sovereign's expectations and beliefs concerning future events. Forward looking statements are necessarily subject to risks, uncertainties and other factors, many of which are outside the control of Sovereign, which could cause actual results to differ materially from such statements. There can be no assurance that forward-looking statements will prove to be correct. Sovereign makes no undertaking to subsequently update or revise the forward-looking statements made in this release, to reflect the circumstances or events after the date of that release.

Competent Persons Statement

The information in this announcement that relates to Mineral Resources is based on, and fairly represents, information compiled by Mr Richard Stockwell, a Competent Person, who is a fellow of the Australian Institute of Geoscientists (AIG). Mr Stockwell is a principal of Placer Consulting Pty Ltd, an independent consulting company. Mr Stockwell has sufficient experience, which is relevant to the style of mineralisation and type of deposit under consideration, and to the activity he is undertaking, to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Stockwell consents to the inclusion of the matters based on his information in the form and context in which it appears.

The information in this announcement that relates to Exploration Results is based on, and fairly represents, information compiled by Mr Samuel Moyle, a Competent Person who is a member of The Australasian Institute of Mining and Metallurgy (AusIMM). Mr Moyle is the Exploration Manager of Sovereign Metals Limited and a holder of ordinary shares, unlisted options and performance rights in Sovereign. Mr Moyle has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken, to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Moyle consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

The information in this announcement that relates to Metallurgical test-work Results - Rutile & Graphite is extracted from the announcement dated 24 June 2019, 9 September 2020 and 7 December 2021. The announcement is available to view on www.sovereignmetals.com.au. Sovereign confirms that a) it is not aware of any new information or data that materially affects the information included in the announcement; b) all material assumptions included in the announcement continue to apply and have not materially changed; and c) the form and context in which the relevant Competent Persons' findings are presented in this report have not been materially changed from the announcement.

This ASX Announcement has been approved and authorised for release by the Company's Managing Director, Dr Julian Stephens.



APPENDIX 1 – JORC CODE, 2012 EDITION – TABLE 1

SECTION 1 - SAMPLING TECHNIQUES AND DATA

Criteria	JORC Code explanation	Commentary
Sampling Techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.	Hand Auger (HA) samples are composited based on regolith boundaries and sample chemistry generated by hand-held XRF (pXRF). Each 1m of sample is dried and riffle-split to generate a total sample weight of 3kg for analysis, generally at 2 - 5m intervals. This primary sample is then split again to create a 3kg composite to provide a 1.5kg sample for both rutile and graphite analyses. Infill Push-Tube (PT) core drilling is sampled routinely at 2m intervals by compositing dried and riffle-split half core. A consistent, 1.5kg sample is generated for both the rutile and graphite determination.
		Air-Core (AC) samples are composited based on expertly logged regolith boundaries. Each 1m of sample is dried and riffle-split to generate a total sample weight of 3kg for analysis, generally at 2m intervals. This primary sample is ther split again to provide a 1.5kg sample for both rutile and graphite analyses.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or	Drilling and sampling activities are supervised by a suitably qualified company geologist who is present at all times. All drill samples are geologically logged by the geologist at the drill site/core yard.
1	systems used.	Each sample is sun dried and homogenised. Sub-samples are carefully riffle split to ensure representivity. The 1.5kg composite samples are then processed.
		An equivalent mass is taken from each sample to make up the composite. A calibration schedule is in place for laboratory scales, sieves and field XRF equipment.
		Placer Consulting Pty Ltd (Placer) Resource Geologists have reviewed Standard Operating Procedures (SOPs) for the collection and processing of dril samples and found them to be fit for purpose and support the resource classifications as applied to the Mineral Resource Estimate (MRE). The primary composite sample is considered representative for this style of rutile mineralisation.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	Logged mineralogy percentages, lithology/regolith information and TiO ₂ % obtained from pXRF are used to assist in determining compositing intervals. Car is taken to ensure that only samples with similar geological characteristics ar composited together.
Drilling Techniques	Drill type (e.g. core, reverse circulation, open- hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face- sampling bit or other type, whether core is	A total of 1,357 HA holes for 12,643m have been drilled to date at the Kasiy Rutile Deposit to obtain samples for quantitative determination of recoverabl rutile and Total Graphitic Carbon (TGC). A PT infill drilling programme, designed to support this resource estimat upgrade, was completed. An additional 234 core holes for 2,368.5m were
	oriented and if so, by what method, etc).	included in the updated MRE. The total PT holes contributing to the updated MRI are 488 for 4,669m.
		A total of 182 AC holes for 4,404m were completed in six locations across th Kasiya deposit deemed likely to fall into mining pit areas. The results are include in this updated MRE.
		Placer has reviewed SOPs for HA, PT and AC drilling and found them to be fit for purpose and support the resource classifications as applied to the MRE. Sampl handling and preparation techniques are consistent for PT and coring samples.
		Two similar designs of HA drilling equipment are employed. HA drilling with 75mr diameter enclosed spiral bits (SOS) with 1m long steel rods and with 62mr diameter open spiral bits (SP) with 1m long steel rods. Drilling is oriente vertically by eye.



Criteria	JORC Code explanation	Commentary
		Each 1m of drill sample is collected into separate sample bags and set asid The auger bits and flights are cleaned between each metre of sampling to avo contamination.
		Core-drilling is undertaken using a drop hammer, Dando Terrier MK1. The drilling generated 1m runs of 83mm PQ core in the first 2m and then transitioned 72mm core for the remainder of the hole. Core drilling is oriented vertically the spirit level.
		AC drilling was completed by Thompson Drilling utilising a Smith Capital 10R3 compact track-mounted drill. The drilling is vertical and generates 1m sample with care taken in the top metres to ensure good recoveries of the high-grad surface material. Each 1m sample bag is immediately transported back Sovereign's field laydown yard where they await processing.
Drill Sample Recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	Samples are assessed visually for recoveries. The configuration of drilling an nature of materials encountered results in negligible sample loss contamination.
		HA and PT drilling is ceased when recoveries become poor once the water table has been reached. Water table and recovery information is included in lithologic logs.
		Core drilling samples are actively assessed by the driller and geologist onsite recoveries and contamination.
		AC drilling recovery in the top few metres are moderate to good. Extra care taken to ensure sample is recovered best as possible in these metres. Recoveri are recorded on the rig at the time of drilling by the geologist. Drilling is ceas when recoveries become poor or once Saprock or refusal has been reached.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	The Company's trained geologists supervise drilling on a 1 team 1 geologist ba and are responsible for monitoring all aspects of the drilling and sampli process.
		For PT drilling, core is extruded into core trays; slough is actively removed by the driller at the drilling rig and core recovery and quality is recorded by the geolog
		AC samples are recovered in large plastic bags. The bags are clearly labell and delivered back to sovereign's laydown yard at the end of shift for processing
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential	No relationship is believed to exist between grade and sample recovery. The hi percentage of silt and absence of hydraulic inflow from groundwater at tl deposit results in a sample size that is well within the expected size range.
	loss/gain of fine/coarse material.	No bias related to preferential loss or gain of different materials is observed.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a	Geologically, data is collected in detail, sufficient to aid in Mineral Resource estimation.
	level of detail to support appropriate Mineral Resource estimation mining studies and metallurgical studies.	All individual 1m HA intervals are geologically logged, recording relevant data a set log-chief template using company codes. A small representative sample collected for each 1m interval and placed in appropriately labelled chip trays for future reference.
		All individual 1m PT core intervals are geologically logged, recording relevant data to a set log-chief template using company codes.
		Half core remains in the trays and is securely stored in the company warehous
		All individual AC 1-metre intervals are geologically logged, recording relevant. data to a set log-chief template using company codes. A small representat sample is collected for each 1-metre interval and placed in appropriately label chip trays for future reference.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.	All logging includes lithological features and estimates of basic mineralog Logging is generally qualitative.
		The PT core is photographed dry, after logging and sampling is completed.
	The total length and percentage of the relevant intersection logged	100% of samples are geologically logged.
Sub-	If core, whether cut or sawn and whether	Due to the soft nature of the material, core samples are carefully cut in half by hand tools.



Criteria	JORC Code explanation	Commentary
techniques and sample preparation	If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.	HA, PT and AC hole samples are dried, riffle split and composited. Samples are collected and homogenised prior to splitting to ensure sample representivity. ~1.5kg composite samples are processed.
		An equivalent mass is taken from each primary sample to make up the composite.
		The primary composite sample is considered representative for this style of mineralisation and is consistent with industry standard practice.
	For all sample types, the nature, quality and appropriateness of the sample preparation	Techniques for sample preparation are detailed on SOP documents verified by Placer Resource Geologists.
	technique.	Sample preparation is recorded on a standard flow sheet and detailed QA/QC undertaken on all samples. Sample preparation techniques and QA/QC protocols are appropriate for mineral determination and support the resource classifications as stated.
	Quality control procedures adopted for all sub-	The sampling equipment is cleaned after each sub-sample is taken.
	sampling stages to maximise representivity of samples.	Field duplicate, laboratory replicate and standard sample geostatistical analysis employed to manage sample precision and analysis accuracy.
	Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.	Sample size analysis is completed to verify sampling accuracy. Field duplicat are collected for precision analysis of riffle splitting. SOPs consider samp representivity. Results indicate a sufficient level of precision for the resour classification.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	The sample size is considered appropriate for the material sampled.
Quality of assay data and	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or	Rutile The Malawi onsite laboratory sample preparation methods are considered quantitative to the point where a heavy mineral concentrate (HMC) is generate
laboratory tests	total.	Final results generated are for recovered rutile i.e, the % mass of the sample that is rutile that can be recovered to the non-magnetic component of a HMC.
		Heavy liquid separation (HLS) of the HM is no longer required and a HM result is not reported in the updated MRE. The HMC prepared via wet-table, gravity separation at the Lilongwe Laboratory provides an ideal sample for subsequen magnetic separation and XRF.
		All 8,855 samples (not incl. QA) included in the MRE update received the following workflow undertaken on-site in Malawi;
		Dry sample in oven for 1 hour at 105℃
		Soak in water and lightly agitate
		Wet screen at 5mm, 600µm and 45µm to remove oversize and slimes material Dry 45µm 600mm (cond fraction) in even for 1 hour at 10500.
		 Dry +45µm -600mm (sand fraction) in oven for 1 hour at 105°C 7,904 of the 8,855 samples received the following workflow undertaken on-site
		in Malawi ■ Pass +45µm -600mm (sand fraction) across wet table to generate a
		HMC.
		 Dry HMC in oven for 30 minutes at 105°C Bag HMC fraction and send to Perth, Australia for quantitative chemical and
		mineralogical determination.
		951 of the 8,855 samples received the following workflow undertaken at Perth based Laboratories (superseded).
		 Split ~150g of sand fraction for HLS using Tetrabromoethane (TBE SG 2.96g/cc) as the liquid heavy media to generate HMC. Work undertaken at Diamantina Laboratories.
		4,738 of the 8,855 samples received magnetic separation undertaken at Allied Mineral Laboratories in Perth, Western Australia.



Criteria	JORC Code explanation	Commentary
		Magnetic separation of the HMC by Carpco magnet @ 16,800G (2.9Amps) into a magnetic (M) and non-magnetic (NM) fraction.
		4,117 of the 8,855 samples received magnetic separation undertaken on-site in Malawi.
		 Magnetic separation of the HMC by Mineral Technologies Reading Pilot IRM (Induced Roll Magnetic) @ 16,800G (2.9Amps) into a magnetic (M) and non-magnetic (NM) fraction.
		All 8,855 routine samples received the following chemical analysis in Perth, Western Australia.
		 The routine NM fractions are sent to ALS Metallurgy Perth for quantitative XRF analysis. Samples receive XRF_MS and are analysed for: TiO₂, Al₂O₃, CaO, Cr₂O₃, Fe₂O₃, K₂O, MgO, MnO, SiO₂, V₂O₅, ZrO₂, HfO₂.
		Graphite 8,078 graphite samples are processed at Intertek-Genalysis Johannesburg and Perth via method C72/CSA.
1) T		A portion of each test sample is dissolved in dilute hydrochloric acid to liberate carbonate carbon. The solution is filtered using a filter paper and the collected residue is the dried to 425°C in a muffle oven to drive off organic carbon. The dried sample is then combusted in a Carbon/ Sulphur analyser to yield total graphitic or TGC.
5		An Eltra CS-800 induction furnace infra-red CS analyser is then used to determine the remaining carbon which is reported as TGC as a percentage.
	For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	Acceptable levels of accuracy and precision have been established. No pXRF methods are used for quantitative determination.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicate, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and	Sovereign uses internal and externally sourced wet screening reference material inserted into samples batches at a rate of 1 in 20. The externally sourced, certified standard reference material for HM and Slimes assessment is provided by Placer Consulting.
	precision have been established.	An external laboratory raw sample duplicate is sent to laboratories in Perth, Australia as an external check of the full workflow. These duplicates are produced at a rate of 1 in 20.
		Accuracy monitoring is achieved through submission of certified reference materials (CRM 's). ALS and Intertek both use internal CRMs and duplicates on XRF analyses.
/2		Sovereign also inserts CRMs into the sample batches at a rate of 1 in 20. Three Rutile CRMs are used by Sovereign and range from 35% - 95% TiO ₂ . Three Graphite CRMs are used by Sovereign and range from 3% – 25% TGC.
		Analysis of sample duplicates is undertaken by standard geostatistical methodologies (Scatter, Pair Difference and QQ Plots) to test for bias and to ensure that sample splitting is representative. Standards determine assay accuracy performance, monitored on control charts, where failure (beyond 3SD from the mean) may trigger re-assay of the affected batch.
		Examination of the QA/QC sample data indicates satisfactory performance of field sampling protocols and assay laboratories providing acceptable levels of precision and accuracy.
		Acceptable levels of accuracy and precision are displayed in geostatistical analyses to support the resource classifications as applied to the estimate.
Verification of sampling & assaying	The verification of significant intersections by either independent or alternative company personnel.	Results are reviewed in cross-section using Datamine Studio RM software and any spurious results are investigated. The deposit type and consistency of mineralisation leaves little room for unexplained variance. Extreme high grades are not encountered.
	The use of twinned holes.	Twinned holes are drilled across a geographically dispersed area to determine short-range geological and assay field variability for the resource estimation. Twin drilling is applied at a rate of 1 in 20 routine holes. Twin paired data in all drill methods represent ~4% of the database included in the updated MRE.



Criteria	JORC Code explanation	Commentary
		Substantial comparative data between different drilling types and test pit results are also available but not referenced in the MRE.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	All data are collected electronically using coded templates and logging software. This data is then imported to a cloud hosted Database and validated automatically and manually.
	Discuss any adjustment to assay data.	A transition to electronic field and laboratory data capture has been achieved. Assay data adjustments are made to convert laboratory collected weights to assay field percentages and to account for moisture.
		QEMSCAN of the NM fraction shows dominantly clean and liberated rutile grains and confirms rutile is the only titanium species in the NM fraction.
		Recovered rutile is defined and reported here as: TiO ₂ recovered in the +45 to -600um range to the NM concentrate fraction as a % of the total primary, dry, raw sample mass divided by 95% (to represent an approximation of final product specifications). i.e recoverable rutile within the whole sample.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations	A Trimble R2 Differential GPS is used to pick up the collars. Daily capture at a registered reference marker ensures equipment remains in calibration.
	used in Mineral Resource estimation.	No downhole surveying of any holes is completed. Given the vertical nature and shallow depths of the holes, drill hole deviation is not considered to significantly affect the downhole location of samples.
	Specification of the grid system used.	WGS84 UTM Zone 36 South.
	Quality and adequacy of topographic control.	The digital terrane model (DTM) was generated by wireframing a 20m-by-20m lidar drone survey point array, commissioned by SVM in March 2022. Major cultural features were removed from the survey points file prior to generating the topographical wireframe for resource model construction. The ultra-high resolution 3D drone aerial survey was executed utilising a RTK GPS equipped Zenith aircraft with accuracy of <10cm ground sampling distance (GSD). Post-processing includes the removal of cultural features that do not reflect material movements (pits, mounds, etc)
		The DTM is suitable for the classification of the resources as stated.
Data spacing & distribution	Data spacing for reporting of Exploration Results.	The HA collars are spaced at nominally 400m along the 400m spaced drill-lines with the PT holes similarly spaced at an offset, infill grid. The resultant 200m-by-200m drill spacing (to the strike orientation of the deposit) is deemed to adequately define the mineralisation in the MRE.
		The AC collars are spaced on a 200m x 200m grid which is deemed to adequately define the mineralisation.
		The PT twin and density sample holes are selectively placed throughout the deposit to ensure a broad geographical and lithological spread for the analysis.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the	The drill spacing and distribution is considered to be sufficient to establish a degree of geological and grade continuity appropriate for the Mineral Resource estimation.
	Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Kriging neighbourhood analysis completed using Supervisor software informs the optimal drill and sample spacing for the MRE. Based on these results and the experience of the Competent Person, the data spacing and distribution is considered adequate for the definition of mineralisation and adequate for mineral resource estimation.
	Whether sample compositing has been applied.	Individual 1m auger intervals have been composited, based on lithology, at 2 – 5m sample intervals for the 1,357 HA holes. 488 PT core holes have been sampled at a regular 2m interval to provide greater control on mineralisation for the Indicated Resource.
		Individual 1m intervals have been composited, based on lithology, at a max 2m sample interval for the 182 AC holes.
		The DH Compositing tool was utilised in Supervisor software to define the optimal sample compositing length. A 2m interval is applied to the MRE.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known considering the deposit type	Sample orientation is vertical and approximately perpendicular to the orientation of the mineralisation, which results in true thickness estimates, limited by the sampling interval as applied. Drilling and sampling are carried out on a regular square grid. There is no apparent bias arising from the orientation of the drill holes with respect to the orientation of the deposit.



Criteria	JORC Code explanation	Commentary
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	There is no apparent bias arising from the orientation of the drill holes with respect to the orientation of the deposit.
Sample security	The measures taken to ensure sample security	Samples are stored in secure storage from the time of drilling, through gathering, compositing and analysis. The samples are sealed as soon as site preparation is complete. A reputable international transport company with shipment tracking enables a chain of custody to be maintained while the samples move from Malawi to Australia. Samples are again securely stored once they arrive and are processed at Australian laboratories. A reputable domestic courier company manages the movement of samples within Perth, Australia. At each point of the sample workflow the samples are inspected by a company representative to monitor sample condition. Each laboratory confirms the integrity of the samples upon receipt.
Audits or reviews	The results of any audits or reviews of sampling techniques and data	The CP Richard Stockwell has reviewed and advised on all stages of data collection, sample processing, QA protocol and mineral resource estimation. Methods employed are considered industry best-practice. Perth Laboratory visits have been completed by Mr Stockwell. Field and incountry lab visits have been completed by Mr Stockwell in May 2022. A high standard of operation, procedure and personnel was observed and reported. Sovereign Metals Managing Director Julian Stephens and Exploration Manager Samuel Moyle have been onsite in Malawi numerous times since the discovery of the Kasiya Deposit.

SECTION 2 - REPORTING OF EXPLORATION RESULTS

Criteria	Explanation	Commentary
Mineral tenement & land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites,	The Company owns 100% of the following Exploration Licences (ELs) and Licence Applications (APLs) under the Mines and Minerals Act 2019, held in the Company's wholly-owned, Malawi-registered subsidiaries: EL0561, EL0492, EL0609, EL0582, EL0545, EL0528, EL0657 and APL0404.
5)	wilderness or national park and environment settings.	A 5% royalty is payable to the government upon mining and a 2% of net profit royalty is payable to the original project vendor.
		No significant native vegetation or reserves exist in the area. The region is intensively cultivated for agricultural crops.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	The tenements are in good standing and no known impediments to exploration or mining exist.
Exploration done by other parties	Acknowledgement and appraisal of exploration by other parties.	Sovereign Metals Ltd is a first-mover in the discovery and definition of residual rutile and graphite resources in Malawi. No other parties are, or have been, involved in exploration.
Geology	Deposit type, geological setting and style of mineralisation	The rutile deposit type is considered a residual placer formed by the intense weathering of rutile-rich basement paragneisses and variable enrichment by elluvial processes.
		Rutile occurs in a mostly topographically flat area west of Malawi's capital, known as the Lilongwe Plain, where a deep tropical weathering profile is preserved. A typical profile from top to base is generally soil ("SOIL" 0-1m) ferruginous pedolith ("FERP", 1-4m), mottled zone ("MOTT", 4-7m), pallid saprolite ("PSAP", 7-9m), saprolite ("SAPL", 9-25m), saprock ("SAPR", 25-35m) and fresh rock ("FRESH" >35m).
		The low-grade graphite mineralisation occurs as multiple bands of graphite gneisses, hosted within a broader Proterozoic paragneiss package. In the Kasiya areas specifically, the preserved weathering profile hosts significant vertical thicknesses, from near surface, of graphite mineralisation.



	Criteria	Explanation	Commentary
	Drill hole information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: easting and northings of the drill hole collar; elevation or RL (Reduced Level-elevation above sea level in metres of the drill hole collar); dip and azimuth of the hole; down hole length and interception depth; and hole length	All intercepts relating to the Kasiya Deposit have been included in public releases during each phase of exploration and in this report. Releases included all collar and composite data and these can be viewed on the Company website. There are no further drill hole results that are considered material to the understanding of the exploration results. Identification of the broad zone of mineralisation is made via multiple intersections of drill holes and to list them all would not give the reader any further clarification of the distribution of mineralisation throughout the deposit.
		If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case	No information has been excluded.
	Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high-grades) and cut-off grades are usually Material and should be stated.	All results reported are of a length-weighted average of in-situ grades. The resource is reported at a range of bottom cut-off grades in recognition that optimisation and financial assessment is outstanding. A nominal bottom cut of 0.7% rutile is offered, based on preliminary assessment of resource product value and anticipated cost of operations.
N		Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	No data aggregation was required.
		The assumptions used for any reporting of metal equivalent values should be clearly stated.	Rutile Equivalent (RutEq) Formula: Rutile Grade x Recovery (97%) x Rutile Price (US\$1,346/t) + Graphite Grade x Recovery (62%) x Graphite Price (US\$1,085/t) / Rutile Price (US\$1,346/t). Commodity Prices:
			Rutile price: US\$1,308/t Graphite price: US\$1,085/t Metallurgical Recovery: Rutile Recovery: 98% Graphite Recovery: 62% All assumptions taken from the Company's 2022 Expanded Scoping Study
			released 16 June 2022. The Modifying Factors included in the JORC Code were assessed as part of the Scoping Study, including mining, processing, infrastructure, economic, marketing, legal, environmental, social and government factors. The Company has received advice from appropriate experts when assessing each Modifying Factor.
			Following an assessment of the results of the Scoping Study, the Company has formed the view that the next stage of feasibility studies is justified for Kasiya. Feasibility Studies will provide the Company with far more comprehensive assessment of a range of options for the technical and economic viability of Kasiya which by international standards should be sufficient detail for project development financers to base an investment decision.
	Relationship between mineralisation widths & intercept lengths	These relationships are particularly important in the reporting of Exploration Results.	The mineralisation has been released by weathering of the underlying, layered gneissic bedrock that broadly trends NE-SW at Kasiya North and N-S at Kasiya South. It lies in a laterally extensive superficial blanket with high-grade zones reflecting the broad bedrock strike orientation of ~045° in the North of Kasiya and 360° in the South of Kasiya.
		If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	The mineralisation is laterally extensive where the entire weathering profile is preserved and not significantly eroded. Minor removal of the mineralised profile has occurred in alluvial channels. These areas are adequately defined by the drilling pattern and topographical control for the resource estimate.
		If it is not known and only the down hole lengths are reported, there should be a clear	Downhole widths approximate true widths limited to the sample intervals applied. Mineralisation remains open at depth and in areas coincident with high-rutile grade lithologies in basement rocks, is increasing with depth. Graphite results are



Criteria	Explanation	Commentary
	statement to this effect (e.g. 'down hole length, true width not known'.	approximate true width as defined by the sample interval and typically increase witl depth.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of the drill collar locations and appropriate sectional views.	Refer to figures in this report and in previous releases. These are accessible on th Company's webpage.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high-grades and/or widths should be practiced to avoid misleading reporting of exploration results.	All results are included in this report and in previous releases. These are accessible on the Company's webpage.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to: geological observations; geophysical survey results; geochemical	Limited lateritic duricrust has been variably developed at Kasiya, as is customal in tropical highland areas subjected to seasonal wet/dry cycles. Lithological log record drilling refusal in just under 2% of the HA/PT drill database, No drilling refusal was recorded above the saprock interface by AC drilling.
	survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating	Slimes (-45 um) averages 46wt% in the Indicated Resource at a 0.7% rutile bottor cut. Separation test work conducted at AML demonstrates the success in applyin a contemporary mineral sands flowsheet in treating this material and achievin excellent rutile recovery.
7	substances.	Sample quality (representivity) is established by geostatistical analysis comparable sample intervals.
		Several generations of QEMSCAN analysis of the NM performed at ALS Metallurg fraction shows dominantly clean and liberated rutile grains and confirms rutile is the only titanium species in the NM fraction.
Further work	The nature and scale of planned further work (e.g. test for lateral extensions or depth extensions or large-scale step-out drilling).	Further AC drilling will allow the definition of a more extensive saprock-interfact basement and should continue to deliver additional resources below the HA/P ⁻¹ drilled regions.
		A greater understanding of the lithological character and extent of those basemed units, where high-grade (>1%) rutile persists at the saprock interface, may assist focussing further resource definition and exploration targeting.
		Further metallurgical assessment is suggested to characterise rutile quality ar establish whether any chemical variability is inherent across the deposit.
		Trialling drill definition at a 100m spacing is suggested for Measured Resource assessment.
	Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	Refer to diagrams in the body of this report and in previous releases. These at accessible on the Company's webpage.

SECTION 3 - ESTIMATION AND REPORTING OF MINERAL RESOURCES

Criteria	JORC Code explanation	Commentary
Database integrity	Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.	Data are manually entered into database tables according to SOP's and conforming to company field names and classifications. These are then migrated to Datashed5 cloud-hosted database managed internally by the Company with validation and quarantine capability. Relevant tables from the database are exported to csv format and forwarded to Placer for independent review.
	Data validation procedures used.	Validation of the primary data include checks for overlapping intervals, missing survey data, missing assay data, missing lithological data, missing and mismatched (to Lithology) collars.



Criteria	JORC Code explanation	Commentary
		Statistical, out-of-range, distribution, error and missing data validation is completed by Placer on data sets before being compiled into a de-surveyed drill hole file and interrogated in 3D using Datamine Studio RM software.
		All questions relating to the input data are forwarded to the client for review and resolution prior to resource estimation.
Site visits	Comment on any site visits undertaken by the Competent Person and the outcome of those visits.	Perth Laboratory visits have been completed by the Competent Person, Mr Richard Stockwell. Field and in-country lab visits were complete over a 1-week period in May 2022. A high standard of operation, procedure and personnel was observed and reported.
	If no site visits have been undertaken indicate why this is the case.	From the discovery of Kasiya in late 2019 through to early 2022, the Australian and Western Australian Governments restricted unnecessary international travel due to the global Covid19 pandemic.
		During this time the company endeavoured to increase its site photography and drone footage library to satisfy the competent person that best practice procedures are being employed in country.
Geological interpretation	Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.	There is a high degree of repeatability and uniformity in the geological character of the Kasiya Deposit demonstrated by lithological logging of AC, PT core and HA samples. Satellite imagery and airborne geophysical data provided guidance for interpreting the strike continuity of the deposit.
		Drill hole intercept logging and assay results (AC, PT and HA), stratigraphic interpretations from drill core and geological logs of drill data have formed the basis for the geological interpretation. The drilling exclusively targeted the SOIL, FERP, MOTT and SAPL weathering horizons, with no sampling of the SAPR and below the upper level of the fresh rock (FRESH) domain.
Ŧ	Nature of the data used and of any assumptions made.	No assumptions were made.
	The effect, if any, of alternative interpretations on Mineral Resource estimation.	No alternative interpretations on mineral resource estimation are offered.
	The use of geology in guiding and controlling Mineral Resource estimation.	The mineral resource is constrained by the drill array plus one interval in each of the X, Y and Z axes.
		The topographical DTM constrains the vertical extent of the resource. Rutile, enriched at surface by deflation and elluvial processes, is constrained internally by a hard boundary at the base of the SOIL and FERP horizons that overly the (generally less-mineralised) MOTT and SAPL horizons. In this way, continuity of rutile, observed in surface drilling results, is honoured between drill lines rather than being diluted by averaging with underlying, lower-grade material.
		The base to mineralisation is arbitrarily designated at effective drill depth plus one (average sample width) interval in the Z orientation in HA/PT drilling. The effective drill depth is where HA drilling intersects the static water table, rather than being a true depth to un-mineralised basement. Deeper drilling using the AC method has shown rutile enrichment persists to bedrock and a material resource increase is anticipated upon application of this method to a broader area.
		A base to mineralisation of BOH plus 2.7m (-2.7 RL) is retained for this estimate, where drilled by HA/PT methods. This basement horizon is interpreted on 200m north sections and accounts for artifacts of ineffective drilling terminating in soil or ferp horizons. It is applied consistently to both Indicated and Inferred resource areas.
		AC drilling has accurately defined depth to basement at the saprock interface, which has been modelled where intersected in the updated MRE.
	The factors affecting continuity both of grade and geology.	Rutile grade is generally concentrated in surface regolith horizons. Deposit stratigraphy and weathering is consistent along and across strike. Rutile grade is oriented at 45 degrees at Kasiya North and 360 degrees at Kasiya South, which mimics the underlying basement source rocks and residual topography. Rutile varies across strike as a result of the layering of mineralised and non-mineralised basement rocks.
Dimensions	The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below	The Kasiya mineralised footprint strikes NE – SW and currently occupies an area of about 201km².
	surface to the upper and lower limits of the Mineral Resource.	Depth to basement is described previously.



Criteria	JORC Code explanation	Commentary
Estimation and modelling techniques	The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.	Datamine Studio RM and Supervisor software are used for the data analysis, variography, geological interpretation and resource estimation. Key fields are interpolated into the volume model using a range of parameters and interpolation methods to establish best fit for the deposit. For the Kasiya MRE update, the Inverse Distance weighting (power 4) method was seen to perform a superior interpolation of informing data and replication of the high-value and thin, surface (SOIL/FERP) grade distribution. This was assisted by the (customary) application of a Dynamic Anisotropy search, informed by the results of variography, Suitable limitations on the number of samples and the impact of those samples, was maintained. Extreme grade values were not identified by statistical analysis, nor were they
		anticipated in this style of deposit. No top cut is applied to the resource estimation. Interpolation was constrained by hard boundaries (domains) that result from the geological interpretation.
	The availability of check estimates, previous	This is the fourth MRE for the Kasiya Deposit.
	estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.	Pilot plant-scale test work has been completed and results support the view of th Competent Person that an economic deposit of readily separable, high-quality rutile is anticipated from the Kasiya Deposit. The recovery of a coarse-flake graphite by-product was achieved by the test work.
	The assumptions made regarding recovery of by-products.	A graphite by-product was modelled as recoverable TGC.
	Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).	No significant deleterious elements are identified. A selection of assay, magnetic separation and XRF results are modelled and are reported.
	In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.	The average parent cell size used is equivalent to the average drill hole spacing within the Indicated Resource (200m*200m). Cell size in the Z-axis is establishe to cater for the composite sample spacing and definition of the Topsoil domain. This resulted in a parent cell size of 200m x 200m x 3m for the volume model wi 5 sub-cell splits available in the X and Y axes and 10 in the Z axis to smooth topographical and lithological transitions. Both parent cell and sub-cell interpolations were completed and reported. The sub-cell interpolation was again applied to this MRE as it better reflected the geological interpretation and a reasonable graduation of informing data through intermediate cell areas.
		A Topsoil horizon has been defined at 0.3m thickness throughout the Indicated Resource area to support anticipated ore reserve calculation and mining studies Topsoil is disclosed separately but remains in the MRE in recognition of advance investigations by SVM on synthetic topsoil generation for rehabilitation.
	Any assumptions behind modelling of selective mining units.	No assumptions were made regarding the modelling of selective mining units. The resource is reported at an Indicated level of confidence and is suitable for optimisation and the calculation of a Probable Reserve.
	Any assumptions about correlation between variables.	No assumptions were made regarding the correlation between variables.
	Description of how the geological interpretation was used to control the resource estimates.	Interpolation was constrained by hard boundaries (domains) that result from the geological interpretation.
	Discussion of basis for using or not using grade cutting or capping.	Extreme grade values were not identified by statistical analysis, nor were they anticipated in this style of deposit. No top cut is applied to the resource estimation.
	The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.	Validation of grade interpolations was done visually In Datamine by loading mod and drill hole files and annotating, colouring and using filtering to check for the appropriateness of interpolations. Statistical distributions were prepared for model zones from both drill holes and the model to compare the effectiveness of the interpolation. Distributions of section line averages (swath plots) for drill holes and models were also prepared for each zone and orientation for comparison purposes. The resource model has effectively averaged informing drill hole data and is considered suitable to support the resource classifications as applied to the estimate.



Criteria	JORC Code explanation	Commentary
Moisture	Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.	Tonnages are estimated on a dry basis. No moisture content is factored.
Cut-off parameters	The basis of the adopted cut-off grade(s) or quality parameters applied.	The resource is reported at a range of bottom cut-off grades in recognition that optimisation and financial assessment is outstanding.
		A nominal bottom cut of 0.7% rutile is offered, based on preliminary assessment of resource value and anticipated operational cost.
Mining factors or assumptions	Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.	Hydro-mining has been determined as the optimal method of mining for the Kasiya Rutile deposit. The materials competence is loose, soft, fine and friable with no cemented sand or dense clay layers rendering it amenable to hydromining. It is considered that the strip ratio would be zero or near zero. Dilution is considered to be minimal as mineralisation commonly occurs from surface and mineralisation is generally gradational with few sharp boundaries. Recovery parameters have not been factored into the estimate. However, the valuable minerals are readily separable due to their SG differential and are expected to have a high recovery through the proposed, conventional wet concentration plant.
Metallurgical factors or assumptions	The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	Sovereign have announced three sets of metallurgical results to the market (24 June 2019, 9 September 2020 and 7 December 2021), relating to the company's ability to produce a high-grade rutile product with a high recovery via simple conventional processing methods. Sovereign engaged AML to conduct the metallurgical test work and develop a flowsheet for plant design considerations. An initial sighter metallurgical test-work program was undertaken in June 2019 o a 180kg sample of saprolite-hosted rutile from an area representative of the style of mineralisation at the Wofiira prospect. This test work focused on generating saleable product specifications and demonstrated that a high-quality commercial Rutile product can be produced using conventional mineral sands processing methods. The recovered, in-situ rutile grade was 1.16% produced in a +38µm to 250µm size fraction with a produced rutile product grade of 96.0% TiO ₂ . A follow-up test work program was then commissioned on a mineralised sample of approximately 1,000kg composited from a number of drill holes across the Kasiya deposit. The sample had a head grade of 0.96% recoverable rutile. The test-work focussed on producing a rutile product. The test work was based on the flowsheet previously developed with AML with minor improvements. The work showed a premium quality rutile product of 96.3% TiO ₂ with low impurities could again be produced with favourable product sizing a d50 of 145µm. Recoveries were about 98%. A scoping study test work program was then undertaken on a 1,600kg mineralise sample to confirm and improve on the previous bulk metallurgy program completed in late 2020. Results again confirmed premium grade rutile can be produced via a simple and conventional process flow sheet and are consistent with previous results. World-class product chemical specifications are reported a 95.0% to 97.2% TiO ₂ with low impurities and stand-out metallurgical recoveries ranging from 94% to 100%.
Environmental factors or assumptions	Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	A large portion of the Mineral Resource is confined to the SOIL, FERP and MOT weathering domains, and any sulphide minerals have been oxidised in the geological past. Therefore, acid mine-drainage is not anticipated to be a significant risk when mining from the oxidised domain. No major water courses run through the resource area. The Kasiya deposit is located within a farming area and has villages located alor the strike of the deposit. Sovereign holds regular discussions with local landholders and community groups to keep them well informed of the status and future planned directions of the project. Sovereign has benefited from maintainingood relations with landowners and enjoys strong support from the community at large.



Criteria	JORC Code explanation	Commentary
		Kasiya is in a sub-equatorial region of Malawi and is subject to heavy seasonal rainfall, with rapid growth of vegetation in season. Substantial vegetation or nature reserve is absent in the area.
Bulk density	Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.	Density was calculated from 310 full core samples taken from geographically and lithologically-diverse sites across the deposit. Density is calculated using a cylinder volume wet and dry method performed by Sovereign in Malawi and calculations verified by Placer Consulting.
		Density data was loaded into an Excel file, which was flagged against weathering horizons and mineralisation domains. These results were then averaged, by domain and applied to the MRE.
	The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vughs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.	As above.
	Discuss assumptions for bulk density estimates used in the evaluation process of	An average density of 1.65 t/m³ was determined for the total weathering profile.
5	the different materials.	This incorporates and average density of 1.39 t/m³ for the SOIL domain, 1.58 t/m for the FERP domain, 1.66 t/m³ for the MOTT domain, 1.69 t/m³ for the PSAP domain, 1.97 t/m³ for the SAPL domain, and 1.95 t/m³ for the LAT domain. Density data are interpolated into the resource estimate by the nearest neighbour method.
Classification	The basis for the classification of the Mineral Resources into varying confidence categories.	Classification of the MRE is at an Indicated and Inferred category. Minor regions of unclassified material occur in sparsely drilled, typically extraneous regions of the resource area. These are excluded from the resource inventory.
	Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).	All available data were assessed and the competent person's relative confidence in the data was used to assist in the classification of the Mineral Resource.
	Whether the result appropriately reflects the Competent Person's view of the deposit	Results appropriately reflects a reasonable and conservative view of the deposit.
Audits or reviews	The results of any audits or reviews of Mineral Resource estimates.	Independent audit of the MRE construction was contracted to Datamine Australia by Placer prior to delivery to SVM. A third party is engaged by SVM for a further verification of the MRE.
Discussion of relative accuracy/	Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or	Substantial additional resource material is expected to occur below the effective depth of drilling (water table).
confidence	procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy	A high-degree of uniformity exists in the broad and contiguous lithological and grade character of the deposit. Drilling technique have been expertly applied and data collection procedures, density assessments, QA protocols and interpretations conform to industry best practice with few exceptions.
	of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.	Assay, mineralogical determinations and metallurgical test work conform to industry best practice and demonstrate a rigorous assessment of product and procedure. The development of a conventional processing flowsheet and marketability studies support the classification of the Kasiya Resource.
	The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.	The estimate is global.
	These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	No production data are available to reconcile model results.